## Wide Supply Range, Rail-to-Rail Output Instrumentation Amplifier

## Data Sheet

## FEATURES

Gain set with 1 external resistor Gain range: 1 to 1000
Input voltage goes below ground
Inputs protected beyond supplies
Very wide power supply range
Single supply: 2.2 V to 36 V
Dual supplies: $\pm 1.35 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$
Bandwidth ( $\mathbf{G}=1$ ): $\mathbf{1 . 5} \mathbf{~ M H z}$
CMRR (G = 1): 90 dB minimum for BR models Input noise: $\mathbf{2 2} \mathbf{~ n V} / \sqrt{ } \mathbf{H z}$
Typical supply current: $350 \mu \mathrm{~A}$
Specified temperature: $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
8 -lead SOIC and MSOP packages
APPLICATIONS
Industrial process controls
Bridge amplifiers
Medical instrumentation
Portable data acquisition
Multichannel systems

## GENERAL DESCRIPTION

The AD8226 is a low cost, wide supply range instrumentation amplifier that requires only one external resistor to set any gain between 1 and 1000 .

The AD8226 is designed to work with a variety of signal voltages. A wide input range and rail-to-rail output allow the signal to make full use of the supply rails. Because the input range also includes the ability to go below the negative supply, small signals near ground can be amplified without requiring dual supplies. The AD8226 operates on supplies ranging from $\pm 1.35 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$ for dual supplies and 2.2 V to 36 V for single supply.

The robust AD8226 inputs are designed to connect to realworld sensors. In addition to its wide operating range, the

## PIN CONFIGURATION



Figure 1.

Table 1. Instrumentation Amplifiers by Category ${ }^{1}$

| General <br> Purpose | Zero <br> Drift | Military <br> Grade | Low <br> Power | High Speed <br> PGA |
| :--- | :--- | :--- | :--- | :--- |
| AD8220 | AD8231 | AD620 | AD627 | AD8250 |
| AD8221 | AD8290 | AD621 | AD623 | AD8251 |
| AD8222 | AD8293 | AD524 | AD8223 | AD8253 |
| AD8224 | AD8553 | AD526 | AD8226 |  |
| AD8228 | AD8556 | AD624 | AD8227 |  |
| AD8295 | AD8557 |  | AD8235/ |  |

${ }^{1}$ Visit www.analog.com for the latest instrumentation amplifiers.

AD8226 can handle voltages beyond the rails. For example, with a $\pm 5 \mathrm{~V}$ supply, the part is guaranteed to withstand $\pm 35 \mathrm{~V}$ at the input with no damage. Minimum as well as maximum input bias currents are specified to facilitate open wire detection.
The AD8226 is perfect for multichannel, space-constrained industrial applications. Unlike other low cost, low power instrumentation amplifiers, the AD8226 is designed with a minimum gain of 1 and can easily handle $\pm 10 \mathrm{~V}$ signals. With its MSOP package and $125^{\circ} \mathrm{C}$ temperature rating, the AD8226 thrives in tightly packed, zero airflow designs.

The AD8226 is available in 8-lead MSOP and SOIC packages, and is fully specified for $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ operation.

For a device with a similar package and performance as the AD8226 but with gain settable from 5 to 1000, consider using the AD8227.

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## SPECIFICATIONS

$+\mathrm{V}_{\mathrm{S}}=+15 \mathrm{~V},-\mathrm{V}_{\mathrm{S}}=-15 \mathrm{~V}, \mathrm{~V}_{\text {REF }}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{G}=1, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, specifications referred to input, unless otherwise noted.
Table 2.



[^0]$+\mathrm{V}_{\mathrm{S}}=2.7 \mathrm{~V},-\mathrm{V}_{\mathrm{S}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{REF}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{G}=1, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, specifications referred to input, unless otherwise noted.
Table 3.


${ }^{1}$ Input stage uses pnp transistors; therefore, input bias current always flows out of the part.
${ }^{2}$ The values specified for $G>1$ do not include the effects of the external gain-setting resistor, $R_{G}$.
${ }^{3}$ Input voltage range of the AD8226 input stage. The input range depends on the common-mode voltage, the differential voltage, the gain, and the reference voltage. See the Input Voltage Range section for more information.

## ABSOLUTE MAXIMUM RATINGS

Table 4.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | $\pm 18 \mathrm{~V}$ |
| Output Short-Circuit Current | Indefinite |
| Maximum Voltage at $-I N$ or $+I \mathrm{~N}$ | $-\mathrm{V}_{\mathrm{s}}+40 \mathrm{~V}$ |
| Minimum Voltage at -IN or +IN | $+\mathrm{V}_{\mathrm{s}}-40 \mathrm{~V}$ |
| REF Voltage | $\pm \mathrm{V}_{\mathrm{S}}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Specified Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Maximum Junction Temperature | $140^{\circ} \mathrm{C}$ |
| ESD |  |
| $\quad$ Human Body Model | 1.5 kV |
| $\quad$ Charge Device Model | 1.5 kV |
| $\quad$ Machine Model | 100 V |

## THERMAL RESISTANCE

$\theta_{\text {IA }}$ is specified for a device in free air.
Table 5. Thermal Resistance

| Package | $\boldsymbol{\theta}_{\text {JA }}$ | Unit |
| :--- | :--- | :--- |
| 8-Lead MSOP, 4-Layer JEDEC Board | 135 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead SOIC, 4-Layer JEDEC Board | 121 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage |
| :--- | :--- |
| may occur on devices subjected to high energy ESD. |  |
| Therefore, proper ESD precautions should be taken to |  |
| avoid performance degradation or loss of functionality. |  |

$\theta$ is

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



Table 6. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :--- | :--- | :--- |
| 1 | -IN | Negative Input. |
| 2,3 | $\mathrm{R}_{\mathrm{G}}$ | Gain-Setting Pins. Place a gain resistor between these two pins. |
| 4 | +IN | Positive Input. |
| 5 | $-\mathrm{V}_{\mathrm{S}}$ | Negative Supply. |
| 6 | REF | Reference. This pin must be driven by low impedance. |
| 7 | $\mathrm{~V}_{\text {out }}$ | Output. |
| 8 | $+\mathrm{V}_{\mathrm{S}}$ | Positive Supply. |

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{T}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, unless otherwise noted.


Figure 3. Typical Distribution of Output Offset Voltage


Figure 4. Typical Distribution of Output Offset Voltage Drift


Figure 5. Typical Distribution of Input Offset Voltage


Figure 6. Typical Distribution of Input Offset Voltage Drift, G = 100


Figure 7. Typical Distribution of Input Bias Current


Figure 8. Typical Distribution of Input Offset Current


Figure 9. Input Common-Mode Voltage vs. Output Voltage, Single Supply, $V_{S}=+2.7$ V, G = 1


Figure 10. Input Common-Mode Voltage vs. Output Voltage, Single Supply, $V_{S}=+5 V, G=1$


Figure 11. Input Common-Mode Voltage vs. Output Voltage, Dual Supplies, $V_{S}= \pm 5 \mathrm{~V}, \mathrm{G}=1$


Figure 12. Input Common-Mode Voltage vs. Output Voltage, Single Supply, $V_{s}=+2.7$ V, G = 100


Figure 13. Input Common-Mode Voltage vs. Output Voltage,
Single Supply, $V_{S}=+5 V, G=100$


Figure 14. Input Common-Mode Voltage vs. Output Voltage, Dual Supplies, $V_{S}= \pm 5 \mathrm{~V}, \mathrm{G}=100$


Figure 15. Input Common-Mode Voltage vs. Output Voltage, Dual Supplies, $V_{S}= \pm 15$ V, G $=1$


Figure 16. Input Overvoltage Performance, $G=1, V_{s}=2.7 \mathrm{~V}$


Figure 17. Input Overvoltage Performance, $G=1, V_{S}= \pm 15 \mathrm{~V}$


Figure 18. Input Common-Mode Voltage vs. Output Voltage,
Dual Supplies, V $= \pm 15$ V, G $=100$


Figure 19. Input Overvoltage Performance, $G=100, V_{S}=2.7 \mathrm{~V}$


Figure 20. Input Overvoltage Performance, $G=100, V_{s}= \pm 15 \mathrm{~V}$


Figure 21. Input Bias Current vs. Common-Mode Voltage, $V_{S}=+5 \mathrm{~V}$


Figure 22. Input Bias Current vs. Common-Mode Voltage, $V_{S}= \pm 15 \mathrm{~V}$


Figure 23. Positive PSRR vs. Frequency, RTI


Figure 24. Negative PSRR vs. Frequency


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Figure 26. Gain vs. Frequency, 2.7 V Single Supply


Figure 27. CMRR vs. Frequency, RTI


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Figure 29. Change in Input Offset Voltage vs. Warm-Up Time


Figure 30. Input Bias Current and Input Offset Current vs. Temperature


Figure 31. Gain Error vs. Temperature, G=1


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Figure 33. Input Voltage Limit vs. Supply Voltage


Figure 34. Output Voltage Swing vs. Supply Voltage, $R_{L}=10 \mathrm{k} \Omega$


Figure 35. Output Voltage Swing vs. Supply Voltage, $R_{L}=2 \mathrm{k} \Omega$


Figure 36. Output Voltage Swing vs. Load Resistance


Figure 37. Output Voltage Swing vs. Output Current, $G=1$


Figure 38. Gain Nonlinearity, $G=1, R_{L} \geq 2 k \Omega$


Figure 39. Gain Nonlinearity, $G=10, R_{L} \geq 2 \mathrm{k} \Omega$


Figure 40. Gain Nonlinearity, $G=100, R_{L} \geq 2 \mathrm{k} \Omega$


Figure 41. Gain Nonlinearity, $G=1000, R_{L} \geq 2 \mathrm{k} \Omega$


Figure 42. Voltage Noise Spectral Density vs. Frequency


Figure 43. 0.1 Hz to 10 Hz RTI Voltage Noise, $G=1, G=1000$


Figure 44. Current Noise Spectral Density vs. Frequency


Figure 45. 0.1 Hz to 10 Hz Current Noise


Figure 46. Large-Signal Frequency Response


Figure 47. Large-Signal Pulse Response and Settling Time, $G=1,10 \mathrm{VStep}, V_{s}= \pm 15 \mathrm{~V}$


Figure 48. Large-Signal Pulse Response and Settling Time, $G=10,10 \mathrm{~V}$ Step, $V_{s}= \pm 15 \mathrm{~V}$


Figure 49. Large-Signal Pulse Response and Settling Time, $G=100,10 \mathrm{~V}$ Step, $V_{S}= \pm 15 \mathrm{~V}$


Figure 50. Large-Signal Pulse Response and Settling Time, $G=1000,10 \mathrm{VStep}, V_{S}= \pm 15 \mathrm{~V}$


Figure 51. Small-Signal Response, $G=1, R_{L}=10 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$


Figure 52. Small-Signal Response, $G=10, R_{L}=10 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$


Figure 53. Small-Signal Response, $G=100, R_{L}=10 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$

Figure 54. Small-Signal Response, $G=1000, R_{L}=10 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$


Figure 55. Small-Signal Response with Various Capacitive Loads, $G=1, R_{L}=\infty$


Figure 56. Settling Time vs. Step Size, $V_{S}= \pm 15$ V Dual Supplies


Figure 57. Supply Current vs. Supply Voltage

## THEORY OF OPERATION



## ARCHITECTURE

The AD8226 is based on the classic 3-op-amp topology. This topology has two stages: a preamplifier to provide differential amplification, followed by a difference amplifier to remove the common-mode voltage. Figure 58 shows a simplified schematic of the AD8226.
The first stage works as follows: in order to maintain a constant voltage across the bias resistor $\mathrm{R}_{\mathrm{B}}, \mathrm{A} 1$ must keep Node 3 a constant diode drop above the positive input voltage. Similarly, A2 keeps Node 4 at a constant diode drop above the negative input voltage. Therefore, a replica of the differential input voltage is placed across the gain-setting resistor, $\mathrm{R}_{\mathrm{G}}$. The current that flows across this resistance must also flow through the R1 and R2 resistors, creating a gained differential signal between the A2 and A1 outputs. Note that, in addition to a gained differential signal, the original common-mode signal, shifted a diode drop up, is also still present.
The second stage is a difference amplifier, composed of A3 and four $50 \mathrm{k} \Omega$ resistors. The purpose of this stage is to remove the common-mode signal from the amplified differential signal.

The transfer function of the AD8226 is

$$
V_{\text {OUT }}=G\left(V_{I N_{+}}-V_{I N-}\right)+V_{\text {REF }}
$$

where:
$G \quad 1+=\frac{49.4 \mathrm{k} \Omega}{R_{G}}$

## GAIN SELECTION

Placing a resistor across the $\mathrm{R}_{\mathrm{G}}$ terminals sets the gain of the AD8226, which can be calculated by referring to Table 7 or by using the following gain equation:

$$
R_{G}=\frac{49.4 \mathrm{k} \Omega}{G-1}
$$

Table 7. Gains Achieved Using 1\% Resistors

| $\mathbf{1 \%}$ Standard Table Value of $\mathbf{R}_{\mathbf{G}}(\mathbf{\Omega})$ | Calculated Gain |
| :--- | :--- |
| 49.9 k | 1.990 |
| 12.4 k | 4.984 |
| 5.49 k | 9.998 |
| 2.61 k | 19.93 |
| 1.00 k | 50.40 |
| 499 | 100.0 |
| 249 | 199.4 |
| 100 | 495.0 |
| 49.9 | 991.0 |

The AD8226 defaults to $\mathrm{G}=1$ when no gain resistor is used. The tolerance and gain drift of the $\mathrm{R}_{\mathrm{G}}$ resistor should be added to the AD8226 specifications to determine the total gain accuracy of the system. When the gain resistor is not used, gain error and gain drift are minimal.
If a gain of 5 is required and minimal gain drift is important, consider using the AD8227. The AD8227 has a default gain of 5 that is set with internal resistors. Because all resistors are internal, the gain drift is extremely low ( $<5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ maximum).

## REFERENCE TERMINAL

The output voltage of the AD8226 is developed with respect to the potential on the reference terminal. This is useful when the output signal needs to be offset to a precise midsupply level. For example, a voltage source can be tied to the REF pin to levelshift the output so that the AD8226 can drive a single-supply ADC. The REF pin is protected with ESD diodes and should not exceed either $+\mathrm{V}_{\mathrm{S}}$ or $-\mathrm{V}_{\mathrm{S}}$ by more than 0.3 V .
For the best performance, source impedance to the REF terminal should be kept below $2 \Omega$. As shown in Figure 58, the reference terminal, REF, is at one end of a $50 \mathrm{k} \Omega$ resistor. Additional impedance at the REF terminal adds to this $50 \mathrm{k} \Omega$ resistor and results in amplification of the signal connected to the positive input. The amplification from the additional $R_{\text {REF }}$ can be computed by $2\left(50 \mathrm{k} \Omega+\mathrm{R}_{\text {REF }}\right) /\left(100 \mathrm{k} \Omega+\mathrm{R}_{\text {REF }}\right)$.
Only the positive signal path is amplified; the negative path is unaffected. This uneven amplification degrades CMRR.


Figure 59. Driving the Reference Pin

## INPUT VOLTAGE RANGE

Figure 9 through Figure 15 and Figure 18 show the allowable common-mode input voltage ranges for various output voltages and supply voltages. The 3-op-amp architecture of the AD8226 applies gain in the first stage before removing common-mode voltage with the difference amplifier stage. Internal nodes between the first and second stages (Node 1 and Node 2 in Figure 58) experience a combination of a gained signal, a common-mode signal, and a diode drop. This combined signal can be limited by the voltage supplies even when the individual input and output signals are not limited.

For most applications, Figure 9 through Figure 15 and Figure 18 provide sufficient information to achieve a good design. For applications where a more detailed understanding is needed, Equation 1 to Equation 3 can be used to understand how the gain (G), common-mode input voltage ( $\mathrm{V}_{\mathrm{CM}}$ ), differential input voltage ( $\mathrm{V}_{\text {DIFF }}$ ), and reference voltage ( $\mathrm{V}_{\text {REF }}$ ) interact. The values for the constants, $\mathrm{V}_{\text {-Limit }}, \mathrm{V}_{\text {+LIMIT }}$, and $\mathrm{V}_{\text {Ref_Limit }}$, are shown in Table 8. These three formulas, along with the input and output range specifications in Table 2 and Table 3, set the operating boundaries of the part.

$$
\begin{align*}
& V_{C M}-\left|\frac{\left(V_{\text {DIFF }}\right)(G)}{2}\right|>-V_{S}+V_{-L I M I T}  \tag{1}\\
& V_{C M}+\left|\frac{\left(V_{D I F F}\right)(G)}{2}\right|<+V_{S}-V_{+L I M I T}  \tag{2}\\
& \frac{\left(V_{D I F F}\right)(G)}{2}+V_{C M}+V_{R E F}  \tag{3}\\
& 2
\end{align*}+V_{S}-V_{\text {REF_L }_{-} L I M I T}
$$

Table 8. Input Voltage Range Constants for Various Temperatures

| Temperature | $\mathbf{V}_{\text {-LIMIT }}$ | $\mathbf{V}_{\text {+LIMIT }}$ | $\mathbf{V}_{\text {REF_LIMIT }}$ |
| :--- | :--- | :--- | :--- |
| $-40^{\circ} \mathrm{C}$ | -0.55 V | 0.8 V | 1.3 V |
| $+25^{\circ} \mathrm{C}$ | -0.35 V | 0.7 V | 1.15 V |
| $+85^{\circ} \mathrm{C}$ | -0.15 V | 0.65 V | 1.05 V |
| $+125^{\circ} \mathrm{C}$ | -0.05 V | 0.6 V | 0.9 V |

## Performance Across Temperature

The common-mode input range shifts upward with temperature. At cold temperatures, the part requires extra headroom from the positive supply, and operation near the negative supply has more margin. Conversely, hot temperatures require less headroom from the positive supply, but are the worst-case conditions for input voltages near the negative supply.

## Recommendation for Best Performance

A typical part functions up to the boundaries described in this section. However, for best performance, designing with a few hundred millivolts extra margin is recommended. As signals approach the boundary, internal transistors begin to saturate, which can affect frequency and linearity performance.

If the application requirements exceed the boundaries, one solution is to apply less gain with the AD8226, and then apply additional gain later in the signal chain. Another option is to use the pin-compatible AD8227.

## LAYOUT

To ensure optimum performance of the AD8226 at the PCB level, care must be taken in the design of the board layout. The AD8226 pins are arranged in a logical manner to aid in this task.


Figure 60. Pinout Diagram

## Common-Mode Rejection Ratio Over Frequency

Poor layout can cause some of the common-mode signals to be converted to differential signals before reaching the in-amp. Such conversions occur when one input path has a frequency response that is different from the other. To keep CMRR across frequency high, the input source impedance and capacitance of each path should be closely matched. Additional source resistance in the input path (for example, for input protection) should be placed close to the in-amp inputs, which minimizes their interaction with parasitic capacitance from the PCB traces.
Parasitic capacitance at the gain-setting pins can also affect CMRR over frequency. If the board design has a component at the gain-setting pins (for example, a switch or jumper), the part should be chosen so that the parasitic capacitance is as small as possible.

## Power Supplies

A stable dc voltage should be used to power the instrumentation amplifier. Note that noise on the supply pins can adversely affect performance. For more information, see the PSRR performance curves in Figure 23 and Figure 24.
A $0.1 \mu \mathrm{~F}$ capacitor should be placed as close as possible to each supply pin. As shown in Figure 61, a $10 \mu \mathrm{~F}$ tantalum capacitor can be used farther away from the part. In most cases, it can be shared by other precision integrated circuits.


Figure 61. Supply Decoupling, REF, and Output Referred to Local Ground

## References

The output voltage of the AD8226 is developed with respect to the potential on the reference terminal. Care should be taken to tie REF to the appropriate local ground.

## INPUT BIAS CURRENT RETURN PATH

The input bias current of the AD8226 must have a return path to ground. When the source, such as a thermocouple, cannot provide a return current path, one should be created, as shown in Figure 62.


Figure 62. Creating an $I_{B A A}$ Path

## INPUT PROTECTION

The AD8226 has very robust inputs and typically does not need additional input protection. Input voltages can be up to 40 V from the opposite supply rail. For example, with a +5 V positive supply and a -8 V negative supply, the part can safely withstand voltages from -35 V to 32 V . Unlike some other instrumentation amplifiers, the part can handle large differential input voltages even when the part is in high gain. Figure 16, Figure 17, Figure 19, and Figure 20 show the behavior of the part under overvoltage conditions.
The rest of the AD8226 terminals should be kept within the supplies. All terminals of the AD8226 are protected against ESD.
For applications where the AD8226 encounters voltages beyond the allowed limits, external current-limiting resistors and lowleakage diode clamps such as the BAV199L, the FJH1100s, or the SP720 should be used.

## RADIO FREQUENCY INTERFERENCE (RFI)

RF rectification is often a problem when amplifiers are used in applications having strong RF signals. The disturbance can appear as a small dc offset voltage. High frequency signals can be filtered with a low-pass RC network placed at the input of the instrumentation amplifier, as shown in Figure 63. The filter limits the input signal bandwidth according to the following relationship:

$$
\begin{aligned}
& \text { FilterFrequency }_{\text {DIFF }}=\frac{1}{2 \pi R\left(2 C_{D}+C_{C}\right)} \\
& \text { FilterFrequency }_{C M}=\frac{1}{2 \pi R C_{C}}
\end{aligned}
$$

where $C_{D} \geq 10 \mathrm{C}$.


Figure 63. RFI Suppression
$C_{D}$ affects the difference signal and $C_{C}$ affects the common-mode signal. Values of R and $\mathrm{C}_{\mathrm{c}}$ should be chosen to minimize RFI. Mismatch between the $\mathrm{R} \times \mathrm{C}_{\mathrm{C}}$ at the positive input and the $\mathrm{R} \times \mathrm{C}_{\mathrm{C}}$ at the negative input degrades the CMRR of the AD8226. By using a value of $C_{D}$ that is one magnitude larger than $C_{C}$, the effect of the mismatch is reduced and performance is improved.

## APPLICATIONS INFORMATION

## DIFFERENTIAL DRIVE



RECOMMENDED OP AMPS: AD8515, AD8641, AD820. RECOMMENDED R VALUES: $5 \mathrm{k} \Omega$ to $20 \mathrm{k} \Omega$.

Figure 64. Differential Output Using an Op Amp
Figure 64 shows how to configure the AD8226 for differential output.
The differential output is set by the following equation:

$$
V_{\text {DIFF_OUT }}=V_{\text {OUT+ }+}-V_{\text {OUT- }}=\operatorname{Gain} \times\left(V_{\text {IN+ }+}-V_{\text {IN- }}\right)
$$

The common-mode output is set by the following equation:

$$
V_{\text {CM_OUT }}=\left(V_{\text {OUT+ }}-V_{\text {OUT-- }}\right) / 2=V_{\text {BIAS }}
$$

The advantage of this circuit is that the dc differential accuracy depends on the AD8226, not on the op amp or the resistors. In addition, this circuit takes advantage of the precise control that the AD8226 has of its output voltage relative to the reference voltage. Although the dc performance and resistor matching of the op amp affect the dc common-mode output accuracy, such errors are likely to be rejected by the next device in the signal chain and therefore typically have little effect on overall system accuracy.

## Tips for Best Differential Output Performance

For best ac performance, an op amp with at least a 2 MHz gain bandwidth and a $1 \mathrm{~V} / \mu \mathrm{s}$ slew rate is recommended. Good choices for op amps are the AD8641, AD8515, and AD820.

Keep trace lengths from the resistors to the inverting terminal of the op amp as short as possible. Excessive capacitance at this node can cause the circuit to be unstable. If capacitance cannot be avoided, use lower value resistors.
For best linearity and ac performance, a minimum positive supply voltage $\left(+V_{s}\right)$ is required. Table 9 shows the minimum supply voltage required for optimum performance. In this mode, $\mathrm{V}_{\mathrm{CM} \text { _MAX }}$ indicates the maximum common-mode voltage expected at the input of the AD8226.

Table 9. Minimum Positive Supply Voltage

| Temperature | Equation |
| :--- | :--- |
| Less than $-10^{\circ} \mathrm{C}$ | $+\mathrm{V}_{\mathrm{S}}>\left(\mathrm{V}_{\text {CM_MAX }}+\mathrm{V}_{\text {BAA }}\right) / 2+1.4 \mathrm{~V}$ |
| $-10^{\circ} \mathrm{C}$ to $25^{\circ} \mathrm{C}$ | $+\mathrm{V}_{\mathrm{S}}>\left(\mathrm{V}_{\text {CM_MAX }}+\mathrm{V}_{\text {BIAS }}\right) / 2+1.25 \mathrm{~V}$ |
| More than $25^{\circ} \mathrm{C}$ | $+\mathrm{V}_{\mathrm{S}}>\left(\mathrm{V}_{\text {CM_MAX }}+\mathrm{V}_{\text {BIAS }}\right) / 2+1.1 \mathrm{~V}$ |

## PRECISION STRAIN GAGE

The low offset and high CMRR over frequency of the AD8226 make it an excellent candidate for performing bridge measurements. The bridge can be connected directly to the inputs of the amplifier (see Figure 65).


Figure 65. Precision Strain Gage

## DRIVING AN ADC

Figure 66 shows several methods for driving an ADC. The ADuC7026 microcontroller was chosen for this example because it contains ADCs with an unbuffered, charge-sampling architecture that is typical of most modern ADCs. This type of architecture typically requires an RC buffer stage between the ADC and amplifier to work correctly.

Option 1 shows the minimum configuration required to drive a charge-sampling ADC. The capacitor provides charge to the ADC sampling capacitor while the resistor shields the AD8226 from the capacitance. To keep the AD8226 stable, the RC time constant of the resistor and capacitor needs to stay above $5 \mu \mathrm{~s}$. This circuit is mainly useful for lower frequency signals.
Option 2 shows a circuit for driving higher speed signals. It uses a precision op amp (AD8616) with relatively high bandwidth and output drive. This amplifier can drive a resistor and capacitor with a much higher time constant and is therefore suited for higher frequency applications.
Option 3 is useful for applications where the AD8226 needs to run off a large voltage supply but drive a single-supply ADC. In normal operation, the AD8226 output stays within the ADC range, and the AD8616 simply buffers it. However, in a fault condition, the output of the AD8226 may go outside the supply range of both the AD8616 and the ADC. This is not an issue in the circuit, however, because the $10 \mathrm{k} \Omega$ resistor between the two amplifiers limits the current into the AD8616 to a safe level.


Figure 66. Driving an $A D C$

## OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MO-187-AA
Figure 67. 8-Lead Mini Small Outline Package [MSOP] (RM-8)
Dimensions shown in millimeters


COMPLIANT TO JEDEC STANDARDS MS-012-AA
CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 68. 8-Lead Standard Small Outline Package [SOIC_N]
Narrow Body
(R-8)
Dimensions shown in millimeters and (inches)

## ORDERING GUIDE

| Model ${ }^{1}$ | Temperature Range | Package Description | Package Option | Branding |
| :---: | :---: | :---: | :---: | :---: |
| AD8226ARMZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | Y18 |
| AD8226ARMZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP, 13" Tape and Reel | RM-8 | Y18 |
| AD8226ARMZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP, 7" Tape and Reel | RM-8 | Y18 |
| AD8226ARZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8226ARZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N, 13" Tape and Reel | R-8 |  |
| AD8226ARZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N, 7" Tape and Reel | R-8 |  |
| AD8226BRMZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | Y19 |
| AD8226BRMZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP, 13" Tape and Reel | RM-8 | Y19 |
| AD8226BRMZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP, 7" Tape and Reel | RM-8 | Y19 |
| AD8226BRZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8226BRZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N, 13" Tape and Reel | R-8 |  |
| AD8226BRZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N, 7" Tape and Reel | R-8 |  |

[^1]NOTES
$\square$
NOTES

## NOTES


[^0]:    ${ }^{1}$ The input stage uses pnp transistors; therefore, input bias current always flows out of the part.
    ${ }^{2}$ The values specified for $G>1$ do not include the effects of the external gain-setting resistor, $R_{G}$.
    ${ }^{3}$ Input voltage range of the AD8226 input stage. The input range depends on the common-mode voltage, the differential voltage, the gain, and the reference voltage. See the Input Voltage Range section for more information.

[^1]:    ${ }^{1} Z=$ RoHS Compliant Part.

