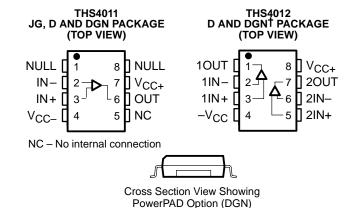
- Very High Speed
 - 290 MHz Bandwidth (G = 1, -3 dB)
 - 310 V/µs Slew Rate
 - 37 ns Settling Time (0.1%)
- **Very Low Distortion**
 - THD = -80 dBc (f = 1 MHz, R_1 = 150 Ω)
- 110 mA Output Current Drive (Typical)
- 7.5 nV/√Hz Voltage Noise
- **Excellent Video Performance**
 - 70 MHz Bandwidth (0.1 dB, G = 1)
 - 0.006% Differential Gain Error
 - 0.01° Differential Phase Error
- ±5 V to ±15 V Supply Voltage
- Available in Standard SOIC, MSOP PowerPAD, JG, or FK Packages
- **Evaluation Module Available**

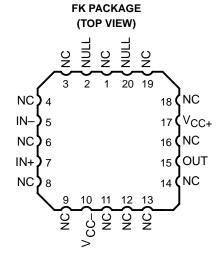
description

The THS4011 and THS4012 are very high speed, single/dual, voltage feedback amplifiers ideal for a wide range of applications. The devices offer very good ac performance with 290-MHz bandwidth, 310-V/µs slew rate, and 37-ns settling time (0.1%). These amplifiers have a high output drive capability of 110 mA and draw only 7.8-mA supply current per channel. For applications requiring low distortion, the THS4011/12 operate with a total harmonic distortion (THD) of -80 dBc at f = 1 MHz. For video applications, the THS4011/12 offer 0.1 dB gain flatness to 70-MHz, 0.006% differential gain error, and 0.01° differential phase error.



† This device is in the Product Preview stage of development. Please contact your local TI sales office for availability.

THS4011



	RELATED DEVICES			
DEVICE DESCRIPTION				
THS4011/2	290-MHz Low Distortion High-Speed Amplifiers			
THS4031/2	100-MHz Low Noise High Speed-Amplifiers			
THS4061/2	180-MHz High-Speed Amplifiers			

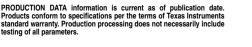


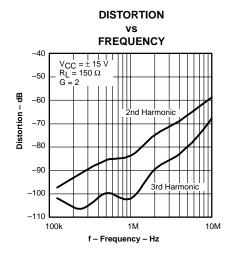
CAUTION: THE THS4011 AND THS4012 provide ESD protection circuitry. However, permanent damage can still occur if this device is subjected to high-energy electrostatic discharges. Proper ESD precautions are recommended to avoid any performance degradation or loss of functionality.



testing of all parameters.

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.





AVAILABLE OPTIONS

		PACKAGE	D DEVICES		PACKAGE	DEVICES	
TA	NUMBER OF CHANNELS	PLASTIC SMALL OUTLINE [†] (D)	PLASTIC MSOP† (DGN)	MSOP SYMBOL	CERAMIC DIP (JG)	CHIP CARRIER (FK)	EVALUATION MODULE
0°C to	1	THS4011CD	THS4011CDGN	TIACI	_	_	THS4011EVM
70°C	2	THS4012CD	THS4012CDGN [‡]	TIABY	_	_	THS4012EVM
–40°C to	1	THS4011ID	THS4011IDGN	TIACJ	_	_	_
85°C	2	THS4012ID	THS4012IDGN [‡]	TIABZ	_	_	_
–55°C to 125°C	1	_	_	_	THS4011MJG	THS4011MFK	_

[†] The D and DGN packages are available taped and reeled. Add an R suffix to the device type (i.e., THS4011CDGNR).



[‡] This device is in the Product Preview stage of development. Please contact your local TI sales office for availability.

functional block diagram

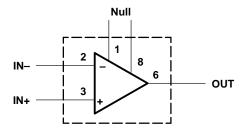


Figure 1. THS4011 – Single Channel

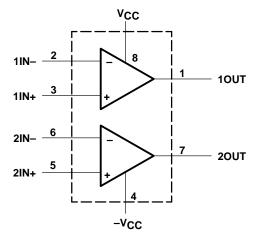


Figure 2. THS4012 - Dual Channel

THS4011, THS4012 290-MHz LOW-DISTORTION HIGH-SPEED AMPLIFIERS

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absolute maximum ratings over operating free-air temperature range (unless otherwise noted)†

Supply voltage, V _{CC}	±16.5 V
Input voltage, V _I	±V _{CC}
Output current, I _O	175 mA
Differential input voltage, V _{ID}	±4 V
Continuous total power dissipation	See Dissipation Rating Table
Maximum junction temperature, T _J	150°C
Operating free-air temperature, T _A , THS401xC	0°C to 70°C
THS401xl	–40°C to 85°C
THS4011M	–55°C to 125°C
Storage temperature, T _{stg}	–65°C to 150°C
Lead temperature, 1,6 mm (1/16 inch) from case for 10 seconds, D, DGN package	age 300°C
Lead temperature, 1,6 mm (1/16 inch) from case for 60 seconds, JG package	300°C
Case temperature for 60 seconds, FK package	260°C

[†] Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

DISSIPATION RATING TABLE

PACKAGE	θ JA (°C/W)	θ JC (°C/W)	T _A = 25°C POWER RATING
D	167†	38.3	740 mW
DGN [‡]	58.4	4.7	2.14 W
JG	119	28	1050 mW
FK	87.7	20	1375 mW

[†] This data was taken using the JEDEC standard Low-K test PCB. For the JEDEC Proposed High-K test PCB, the θ_{JA} is 95°C/W with a power rating at $T_A = 25$ °C of 1.32 W.

recommended operating conditions

			NOM MAX	UNIT
Supply voltage, VCC	Split supply	±4.5	±16	V
	Single supply	9	32	V
	C suffix	0	70	
Operating free-air temperature, T _A	I suffix	-40	85	°C
	M suffix	-55	125	



 $[\]ddagger$ This data was taken using 2 oz. trace and copper pad that is soldered directly to a 3 in. \times 3 in. PC. For further information, refer to Application Information section of this data sheet.

electrical characteristics, V_{CC} = ± 15 V, R_L = 150 Ω , T_A = 25°C, (unless otherwise noted)

dynamic performance

	PARAMETER	TEST CONDITION	TEST CONDITIONS†		THS4011C/I, THS4012C/I				
				MIN	TYP	MAX			
	Unity-gain bandwidth (–3 dB)	Gain = 1	$V_{CC} = \pm 15 \text{ V}$		290		MHz		
	Offity-gain bandwidth (=3 dB)	Gaill = 1	$V_{CC} = \pm 5 \text{ V}$		270		IVII IZ		
BW	Bandwidth for 0.1 dB flatness	Gain = 1	$V_{CC} = \pm 15 \text{ V}$		70	MHz			
Bvv	Dandwidth for 0.1 dB flattless	Galli = 1	$V_{CC} = \pm 5 \text{ V}$		35		IVIMZ		
	Full power bandwidth (see Note 2)	$V_{CC} = \pm 15 \text{ V}, R_L = 150 \Omega$	V _{O(PP)} = 20 V,		4.9		MHz		
	Full power baridwidth (see Note 2)	$V_{CC} = \pm 5 \text{ V}, R_L = 150 \Omega,$	V _{O(PP)} = 5 V,		16		IVITIZ		
SR	Slew rate	Gain = -1 , $R_{I} = 150 Ω$	$V_{CC} = \pm 15 \text{ V}$		310		V/μs		
SK .	Siew fate	Gairi = -1, KL = 150 52	$V_{CC} = \pm 5 \text{ V}$		260		V/μS		
	Settling time to 0.1%	$V_1 = -2.5 \text{ V to } 2.5 \text{ V}, \text{ Gain } = -1$	$V_{CC} = \pm 15 \text{ V}$		37		ns		
I.	Setting time to 0.1%	V = -2.5 V to 2.5 V, Gain = -1	$V_{CC} = \pm 5 \text{ V}$		35		110		
t _S	Sattling time to 0.019/	$V_{CC} = \pm 15$			90		no		
	Settling time to 0.01%	$V_I = -2.5 \text{ V to } 2.5 \text{ V}, \text{ Gain} = -1$	V _{CC} = ±5 V		70		ns		

[†] Full range = 0° C to 70° C for the C suffix and -40° C to 85° C for the I suffix.

noise/distortion performance

PARAMETER		TEST CONDITIONS [†]		TH:	UNIT		
				MIN	TYP	MAX	
THD	Total harmonic distortion	$V_{CC} = \pm 15 \text{ V},$ $V_{O(PP)} = 2 \text{ V}$	$f_C = 1 MHz,$		-80		dBc
Vn	Input voltage noise	$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V},$	f = 10 kHz		7.5		nV/√ Hz
In	Input current noise	$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V},$	f = 10 kHz		1		pA/√ Hz
	Differential gain error	Gain = 2,	$V_{CC} = \pm 15 \text{ V}$		0.01%		
	Dillerential gain endi	$R_L = 150 \Omega$, NTSC	V _{CC} = ±5 V		0.01%		
		Gain = 2,	V _{CC} = ±15 V		0.01°		
	Differential phase error	$R_L = 150 \Omega$, NTSC	V _{CC} = ±5 V		0.001°		

[†] Full range = 0° C to 70° C for the C suffix and -40° C to 85° C for the I suffix.

THS4011, THS4012 290-MHz LOW-DISTORTION HIGH-SPEED AMPLIFIERS

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electrical characteristics at T_A = 25°C, V_{CC} = \pm 15 V, R_L = 150 Ω (unless otherwise noted) (continued) dc performance

PARAMETER		TEST CONDIT	TEST CONDITIONS†		THS4011C/I, THS4012C/I		
				MIN	TYP	MAX	
	$V_{CC} = \pm 15 \text{ V},$	T _A = 25°C	10	25		\//m\/	
	Open loop gain	$V_O = \pm 10 \text{ V},$ $R_L = 1 \text{ k}\Omega$	T _A = full range	8			V/mV
Open loop gain	$V_{CC} = \pm 5 \text{ V},$	T _A = 25°C	7	12		\//==\/	
		$V_O = \pm 2.5 \text{ V},$ $R_L = 250 \Omega$	T _A = full range	5			V/mV
V	lanut affact valtage	Var. JEV an IAEV	T _A = 25°C		1	6	mV
۷IO	Input offset voltage	$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V}$	T _A = full range			8	IIIV
	Input offset voltage drift					15	μV/°C
1	Innut bigg gurrant	Van JEV or J4EV	T _A = 25°C		2	6	
ΙΒ	Input bias current	$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V}$	T _A = full range			8	μΑ
l land official command	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	T _A = 25°C		25	250	nA	
10	Input offset current VCC	$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V}$	T _A = full range			400	I IIA
	Offset current drift	V _{CC} = ±5 V or ±15 V			0.3		nA/°C

[†] Full range = 0°C to 70°C for the C suffix and -40°C to 85°C for the I suffix.

input characteristics

PARAMETER		TEST CONDITIONS [†]		THS4011C/I, THS4012C/I			UNIT
				MIN	TYP	MAX	
\/	Common mode input voltage range	V _{CC} = ±15 V		±13	±14.1		V
VICR	Common-mode input voltage range	$V_{CC} = \pm 5 \text{ V}$		±3.8	±4.3		V
		$V_{CC} = \pm 15 \text{ V},$ $V_{IC} = \pm 12 \text{ V}$	T _A = 25°C	82	110		dB
CMRR			T _A = full range	77			dB
CIVIRR	Common-mode rejection ratio	$V_{CC} = \pm 5 \text{ V},$	T _A = 25°C	90	95		dB
		$V_{CC} = \pm 5 \text{ V},$ $V_{IC} = \pm 2.5 \text{ V}$ $T_A = 25^{\circ}C$ $T_A = \text{full range}$		83			uБ
R _l	Input resistance				2		МΩ
Cl	Input capacitance				1.2		pF

[†] Full range = 0° C to 70° C for the C suffix and -40° C to 85° C for the I suffix.

output characteristics

PARAMETER		TEST	TEST CONDITIONS [†]			THS4011C/I, THS4012C/I		
				MIN	TYP	MAX		
	$V_{CC} = \pm 15 \text{ V}$		±13	±13.5				
\ _{\\} _	Vo Output voltage ewing	$V_{CC} = \pm 5 \text{ V}$	$R_L = 1 k\Omega$	±3.4	±3.7		V	
۷o	Output voltage swing	$V_{CC} = \pm 15 \text{ V}$	$R_L = 250 \Omega$	±12	±12 ±13		V	
		$V_{CC} = \pm 5 \text{ V}$	$R_L = 150 \Omega$	±3	±3.4			
1.0	Output oursent	D. 20.0	$V_{CC} = \pm 15 \text{ V}$	70	110		mA	
Ю	Output current	$R_L = 20 \Omega$	V _{CC} = ±5 V	50	75		MA	
los	Short-circuit output current	$V_{CC} = \pm 15 \text{ V}$			150		mA	
RO	Output resistance	Open loop			12		Ω	

[†] Full range = 0° C to 70° C for the C suffix and -40° C to 85° C for the I suffix.



THS4011, THS4012 290-MHz LOW-DISTORTION HIGH-SPEED AMPLIFIERS

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electrical characteristics at T_A = 25°C, V_{CC} = \pm 15 V, R_L = 150 Ω (unless otherwise noted) (continued) power supply

	PARAMETER	TEST CONDITIONS [†]		THS4011C/I, THS4012C/I			UNIT
				MIN	TYP	MAX	
Vaa	Supply voltage	Dual supply		±4.5		±16.5	V
Vcc	Supply voltage	Single supply		9		33	V
		V _{CC} = ±15 V	T _A = 25°C		7.8	9.5	
	Supply ourrent (analy amplifier)		T _A = full range			11	mΑ
Icc	Supply current (each amplifier)	V+5 V	T _A = 25°C		6.9	8.5	IIIA
		$V_{CC} = \pm 5 \text{ V}$	T _A = full range			10	
PSRR	Dower cumply rejection ratio	\\\ \o \- \+\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	T _A = 25°C	75	83		dB
FORK	Power supply rejection ratio	$V_{CC} = \pm 5 \text{ V to } \pm 15 \text{ V}$	T _A = full range	68			ub

[†] Full range = 0°C to 70°C for the C suffix and -40°C to 85°C for the I suffix.

THS4011, THS4012 290-MHz LOW-DISTORTION HIGH-SPEED AMPLIFIERS

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electrical characteristics, V_{CC} = ± 15 V, R_L = 150 Ω , T_A = 25°C, (unless otherwise noted)

dynamic performance

	PARAMETER		o.t	T⊦	IS4011N	1	UNIT	
	PARAMETER	TEST CONDITION	SI	MIN	TYP	MAX	UNII	
	Unity-gain bandwidth	Closed loop, $R_L = 1 \text{ k}\Omega$	V _{CC} = ±15 V	*160	200		MHz	
BW			$V_{CC} = \pm 15 \text{ V}$	70				
	Bandwidth for 0.1 dB flatness	Gain = 1	$V_{CC} = \pm 5 V$		35		MHz	
			$V_{CC} = \pm 2.5 \text{ V}$		30			
	Full power bandwidth (ass Note 1)	$V_{CC} = \pm 15 \text{ V}, R_L = 150 \ \Omega,$	V _{O(PP)} = 20 V		2.5		MHz	
	Full power bandwidth (see Note 1)	$V_{CC} = \pm 5 \text{ V}, R_L = 150 \Omega,$	V _{O(PP)} = 20 V		8		IVITZ	
SR	Slew rate	$V_{CC} = \pm 15 \text{ V}, R_L = 1 \text{ k}\Omega$		*300	400		V/μs	
	Sottling time to 0.19/	$V_1 = -2.5 \text{ V to } 2.5 \text{ V}, \text{ Gain } = -1$	$V_{CC} = \pm 15 \text{ V}$		37		20	
I .	Settling time to 0.1%	V = -2.5 V to 2.5 V, Gain = -1	$V_{CC} = \pm 5 \text{ V}$		35		ns	
t _S	Sottling time to 0.019/	V ₁ = 2.5 V to 2.5 V Coin = 1	V _{CC} = ±15 V		90		ns	
	Settling time to 0.01%	$V_1 = -2.5 \text{ V to } 2.5 \text{ V}, \text{Gain} = -1$	$V_{CC} = \pm 5 \text{ V}$		70			

[†] Full range = -55° C to 125° C for the M suffix.

NOTE 1: Full pwer bandwidth = slew rate/ $2\pi V_{(PP)}$.

noise/distortion performance

PARAMETER TEST CONDITIONS [†]						THS4011M		
	PARAWETER	IEST	MIN	TYP	MAX	UNIT		
THD	Total harmonic distortion	V _{CC} = ±15 V, V _{O(PP)} = 1 V	f _C = 1 MHz,			-80		dBc
٧n	Input voltage noise	$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V},$	f = 10 kHz			7.5		nV/√Hz
In	Input current noise	$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V},$	f = 10 kHz			1		pA/√ Hz
Differential gain erro	Differential gain arror	Gain = 2,		$V_{CC} = \pm 15 \text{ V}$		0.006		%
	Dillererillar gairr error	R_L = 150 Ω, NTSC		$V_{CC} = \pm 5 \text{ V}$		0.001		/0
	D''' a man t'al mhanananan	Gain = 2, R _L = 150 Ω ,		$V_{CC} = \pm 15 \text{ V}$		0.01°		
	Differential phase error	NTSC		V _C C = ±5 V	(0.002°		

[†] Full range = -55°C to 125°C for the M suffix.



^{*}This parameter is not tested.

electrical characteristics at T_A = full range, V_{CC} = ± 15 V, R_L = 1 k Ω (unless otherwise noted) (continued)

dc performance

	DADAMETER	TEST CONDITIONS†	THS4011M				
	PARAMETER	TEST CONDITIONS!	MIN	TYP	MAX	UNIT	
	Open loop gain	$V_{CC} = \pm 15 \text{ V},$ $V_{O} = \pm 10 \text{ V},$ $R_{L} = 1 \text{ k}\Omega$	T _A = full range	6	14		V/mV
	Орен юор даш	$V_{CC} = \pm 5 \text{ V},$ $V_{O} = \pm 2.5 \text{ V},$ $R_{L} = 1 \text{ k}\Omega$	T _A = full range	5	10		V/mV
V Innut effect value		V _{CC} = ±5 V or ±15 V	T _A = 25°C		2	6	mV
VIO	Input offset voltage	AGC = ∓2 A QI ∓12 A	T _A = full range		2	8	IIIV
	Input offset voltage drift	$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V}$			15		μV/°C
	lanut higa gurrant	V-0 15 V 07 145 V	T _A = 25°C		2	6	
I _{IB} Input bias current		$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V}$	T _A = full range		4	8	μΑ
ΙΙΟ	Input offset current	V _{CC} = ±5 V or ±15 V			25	250	nA
	Offset current drift	V _{CC} = ±5 V or ±15 V	T _A = 25°C		0.3		nA/°C

[†] Full range = –55°C to 125°C for the M suffix.

input characteristics

PARAMETER				THS4011M		
		TEST CONDITIONS [†]	MIN	TYP	MAX	UNIT
Vice Common mode input veltage range		$V_{CC} = \pm 15 \text{ V}$	±13	±14.1		V
VICR	Common-mode input voltage range	V _{CC} = ±5 V	±3.8	±4.3		v
CMRR	Common-mode rejection ratio	$V_{CC} = \pm 15 \text{ V}, \qquad V_{IC} = \pm 12 \text{ V}$	75	90		dB
		$V_{CC} = \pm 5 \text{ V}, \qquad V_{IC} = \pm 2.5 \text{ V}$	84	95		uБ
R _I	Input resistance			2		ΜΩ
Cl	Input capacitance			1.2		pF

[†] Full range = -55° C to 125°C for the M suffix.

output characteristics

	PARAMETER		THS4011M			UNIT	
FARAWETER		TEST CO	MIN	TYP	MAX	ONIT	
		V _{CC} = ±15 V	P 1 kO	±13	±13.5		
1,,,	Output voltage swing		±3.7		V		
Vo	Output voltage swing	$V_{CC} = \pm 15 \text{ V}$	$R_L = 250 \Omega$	±12	±13		V
		$V_{CC} = \pm 5 \text{ V}$	$R_L = 150 \Omega$	±3	±3.4		
la	Output current	V _{CC} = ±15 V	R _L = 20 Ω	70	115		mA
0 0	Output current	$V_{CC} = \pm 5 \text{ V}$		50	75		111/4
los	Short-circuit output current	V _{CC} = ±15 V	T _A = 25°C		150		mA
RO	Output resistance	Open loop			12		Ω

[†] Full range = -55° C to 125°C for the M suffix.



electrical characteristics at T_A = full range, V_{CC} = ± 15 V, R_L = 1 k Ω (unless otherwise noted) (continued)

power supply

	PARAMETER	TEST CO	THS4011M			UNIT		
PARAMETER		TEST CO	MIN	TYP	MAX	UNII		
V00	Supply voltage	Dual supply		±4.5		±16.5	V	
VCC Supply voltage		Single supply		9		33	V	
		V 145.V	T _A = 25°C		7.8	9.5		
	Quiescent current	V _{CC} = ±15 V	T _A = full range		11	A		
ICC	Quiescent current	V 15 V	T _A = 25°C		6.9	8.5	mA mA	
		V _{CC} = ±5 V	T _A = full range			10		
PSRR	Dower gunnly rejection ratio	V _{CC} = ±5 V to ±15 V	$T_A = 25^{\circ}C$	80	86		dB	
	Power supply rejection ratio	ACC = 72 A 10 ±12 A	T _A = full range	78	83	, and the second	ub	

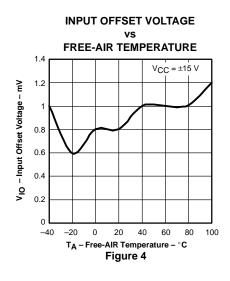
[†] Full range = -55° C to 125°C for the M suffix.

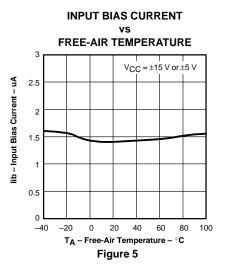
PARAMETER MEASUREMENT INFORMATION

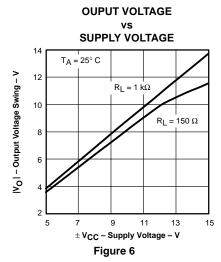


Figure 3. THS4012 Crosstalk Test Circuit

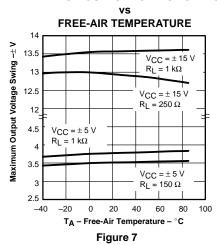
TYPICAL CHARACTERISTICS

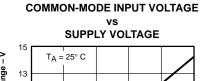


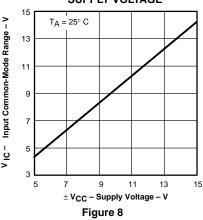




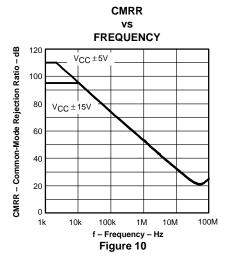


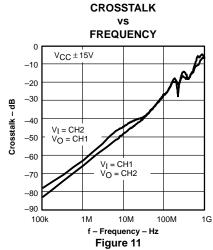


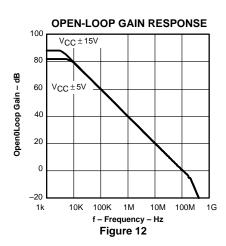




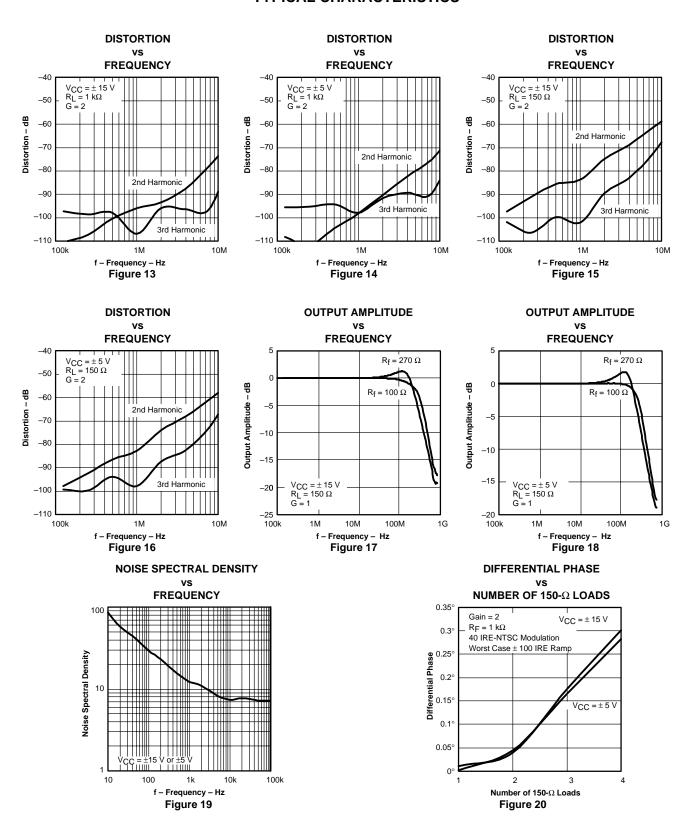
PSRR vs **FREQUENCY** 100 V_{CC} = ±15 V or ±5 V 90 PSRR - Power-Supply Rejection Ratio 80 70 60 50 40 20 10 0 10k 100k 1M 10M 100M 1k f - Frequency - Hz Figure 9





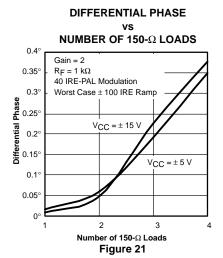


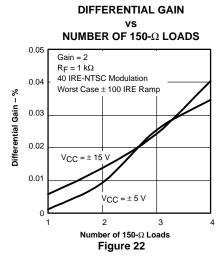
TYPICAL CHARACTERISTICS

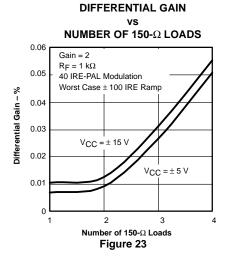




TYPICAL CHARACTERISTICS







theory of operation

The THS401x is a high-speed, operational amplifier configured in a voltage feedback architecture. It is built using a 30-V, dielectrically isolated, complementary bipolar process with NPN and PNP transistors possessing f_{TS} of several GHz. This results in an exceptionally high performance amplifier that has a wide bandwidth, high slew rate, fast settling time, and low distortion. A simplified schematic is shown in Figure 24.

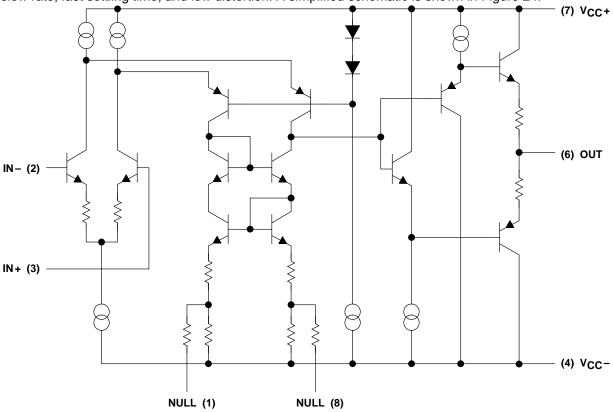


Figure 24. THS4011 Simplified Schematic

noise calculations and noise figure

Noise can cause errors on very small signals. This is especially true when amplifying small signals. The noise model for the THS401x is shown in Figure 25. This model includes all of the noise sources as follows:

- $e_n = \text{Amplifier internal voltage noise } (nV/\sqrt{Hz})$
- IN+ = Noninverting current noise (pA/√Hz)
- IN- = Inverting current noise (pA/ \sqrt{Hz})
- e_{Rx} = Thermal voltage noise associated with each resistor (e_{Rx} = 4 kTR_x)



noise calculations and noise figure (continued)

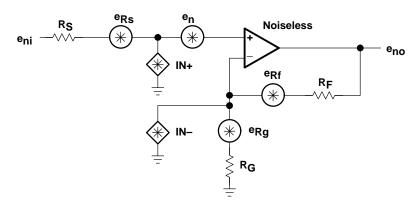


Figure 25. Noise Model

The total equivalent input noise density (eni) is calculated by using the following equation:

$$\mathbf{e}_{ni} = \sqrt{\left(\mathbf{e}_{n}\right)^{2} + \left(\mathsf{IN} + \times \mathsf{R}_{S}\right)^{2} + \left(\mathsf{IN} - \times \left(\mathsf{R}_{F} \, \| \, \mathsf{R}_{G}\right)\right)^{2} + 4 \, \, \mathsf{kTR}_{S} + 4 \, \, \mathsf{kT}\left(\mathsf{R}_{F} \, \| \, \mathsf{R}_{G}\right)}}$$

Where:

 $k = Boltzmann's constant = 1.380658 \times 10^{-23}$

T = Temperature in degrees Kelvin (273 $+^{\circ}$ C)

 $R_F \parallel R_G = Parallel resistance of R_F and R_G$

To get the equivalent output noise of the amplifier, just multiply the equivalent input noise density (e_{ni}) by the overall amplifier gain (A_V).

$$e_{no} = e_{ni} A_V = e_{ni} \left(1 + \frac{R_F}{R_G} \right)$$
 (noninverting case)

As the previous equations show, to keep noise at a minimum, small value resistors should be used. As the closed-loop gain is increased (by reducing R_G), the input noise is reduced considerably because of the parallel resistance term. This leads to the general conclusion that the most dominant noise sources are the source resistor (R_S) and the internal amplifier noise voltage (e_n). Because noise is summed in a root-mean-squares method, noise sources smaller than 25% of the largest noise source can be effectively ignored. This can greatly simplify the formula and make noise calculations much easier to calculate.

For more information on noise analysis, please refer to the *Noise Analysis* section in *Operational Amplifier Circuits Applications Report* (literature number SLVA043).

noise calculations and noise figure (continued)

This brings up another noise measurement usually preferred in RF applications, the noise figure (NF). Noise figure is a measure of noise degradation caused by the amplifier. The value of the source resistance must be defined and is typically 50Ω in RF applications.

$$NF = 10log \left[\frac{e_{ni}^2}{\left(e_{Rs}\right)^2} \right]$$

Because the dominant noise components are generally the source resistance and the internal amplifier noise voltage, we can approximate noise figure as:

$$NF = 10log \left[1 + \frac{\left(\left(e_n \right)^2 + \left(IN + \times R_S \right)^2 \right)}{4 \text{ kTR}_S} \right]$$

Figure 26 shows the noise figure graph for the THS401x.

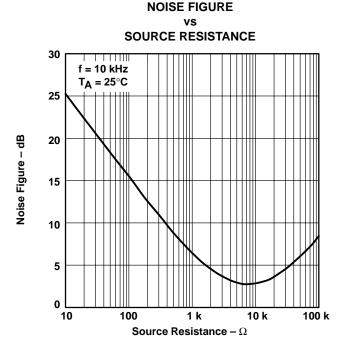


Figure 26. Noise Figure vs Source Resistance



driving a capacitive load

Driving capacitive loads with high performance amplifiers is not a problem as long as certain precautions are taken. The first is to realize that the THS401x has been internally compensated to maximize its bandwidth and slew rate performance. When the amplifier is compensated in this manner, capacitive loading directly on the output will decrease the device's phase margin leading to high frequency ringing or oscillations. Therefore, for capacitive loads of greater than 10 pF, it is recommended that a resistor be placed in series with the output of the amplifier, as shown in Figure 27. A minimum value of 20 Ω should work well for most applications. For example, in 75- Ω transmission systems, setting the series resistor value to 75 Ω both isolates any capacitance loading and provides the proper line impedance matching at the source end.

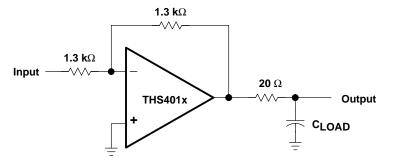


Figure 27. Driving a Capacitive Load

offset nulling

The THS401x has very low input offset voltage for a high-speed amplifier. However, if additional correction is required, an offset nulling function has been provided on the THS4011. The input offset can be adjusted by placing a potentiometer between terminals 1 and 8 of the device and tying the wiper to the negative supply. This is shown in Figure 28.

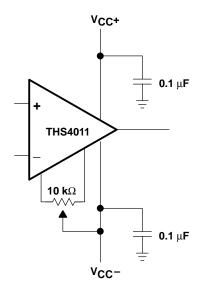


Figure 28. Offset Nulling Schematic

offset voltage

The output offset voltage, (V_{OO}) is the sum of the input offset voltage (V_{IO}) and both input bias currents (I_{IB}) times the corresponding gains. The following schematic and formula can be used to calculate the output offset voltage:

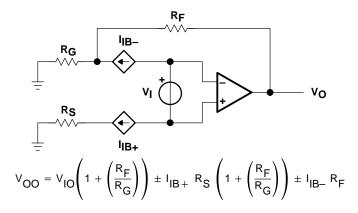


Figure 29. Output Offset Voltage Model

optimizing unity gain response

Internal frequency compensation of the THS401x was selected to provide very wideband performance yet still maintain stability when operated in a noninverting unity gain configuration. When amplifiers are compensated in this manner there is usually peaking in the closed loop response and some ringing in the step response for very fast input edges, depending upon the application. This is because a minimum phase margin is maintained for the G=+1 configuration. For optimum settling time and minimum ringing, a feedback resistor of $100\,\Omega$ should be used as shown in Figure 30. Additional capacitance can also be used in parallel with the feedback resistance if even finer optimization is required.

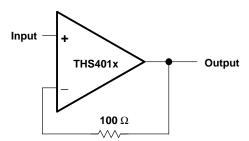


Figure 30. Noninverting, Unity Gain Schematic

general configurations

When receiving low-level signals, limiting the bandwidth of the incoming signals into the system is often required. The simplest way to accomplish this is to place an RC filter at the noninverting terminal of the amplifer (see Figure 31).

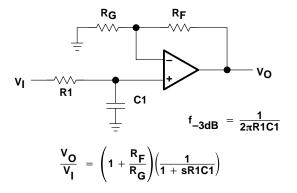


Figure 31. Single-Pole Low-Pass Filter

If even more attenuation is needed, a multiple pole filter is required. The Sallen-Key filter can be used for this task. For best results, the amplifier should have a bandwidth that is 8 to 10 times the filter frequency bandwidth. Failure to do this can result in phase shift of the amplifier.

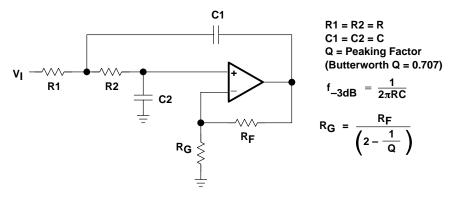


Figure 32. 2-Pole Low-Pass Sallen-Key Filter

circuit layout considerations

To achieve the levels of high frequency performance of the THS401x, follow proper printed-circuit board high frequency design techniques. A general set of guidelines is given below. In addition, a THS401x evaluation board is available to use as a guide for layout or for evaluating the device performance.

- Ground planes It is highly recommended that a ground plane be used on the board to provide all
 components with a low inductive ground connection. However, in the areas of the amplifier inputs and
 output, the ground plane can be removed to minimize the stray capacitance.
- Proper power supply decoupling Use a 6.8-μF tantalum capacitor in parallel with a 0.1-μF ceramic capacitor on each supply terminal. It may be possible to share the tantalum among several amplifiers depending on the application, but a 0.1-μF ceramic capacitor should always be used on the supply terminal of every amplifier. In addition, the 0.1-μF capacitor should be placed as close as possible to the supply terminal. As this distance increases, the inductance in the connecting trace makes the capacitor less effective. The designer should strive for distances of less than 0.1 inches between the device power terminals and the ceramic capacitors.
- Sockets Sockets are not recommended for high-speed operational amplifiers. The additional lead inductance in the socket pins will often lead to stability problems. Surface-mount packages soldered directly to the printed-circuit board is the best implementation.
- Short trace runs/compact part placements Optimum high frequency performance is achieved when stray series inductance has been minimized. To realize this, the circuit layout should be made as compact as possible, thereby minimizing the length of all trace runs. Particular attention should be paid to the inverting input of the amplifier. Its length should be kept as short as possible. This will help to minimize stray capacitance at the input of the amplifier.
- Surface-mount passive components Using surface-mount passive components is recommended for high
 frequency amplifier circuits for several reasons. First, because of the extremely low lead inductance of
 surface-mount components, the problem with stray series inductance is greatly reduced. Second, the small
 size of surface-mount components naturally leads to a more compact layout thereby minimizing both stray
 inductance and capacitance. If leaded components are used, it is recommended that the lead lengths be
 kept as short as possible.

general PowerPAD design considerations

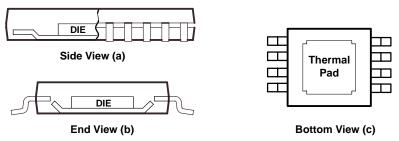
The THS401x is available packaged in a thermally-enhanced DGN package, which is a member of the PowerPAD family of packages. This package is constructed using a downset leadframe upon which the die is mounted [see Figure 33(a) and Figure 33(b)]. This arrangement results in the lead frame being exposed as a thermal pad on the underside of the package [see Figure 33(c)]. Because this thermal pad has direct thermal contact with the die, excellent thermal performance can be achieved by providing a good thermal path away from the thermal pad.

The PowerPAD package allows for both assembly and thermal management in one manufacturing operation. During the surface-mount solder operation (when the leads are being soldered), the thermal pad can also be soldered to a copper area underneath the package. Through the use of thermal paths within this copper area, heat can be conducted away from the package into either a ground plane or other heat dissipating device.

The PowerPAD package represents a breakthrough in combining the small area and ease of assembly of surface mount with the, heretofore, awkward mechanical methods of heatsinking.



general PowerPAD design considerations (continued)



NOTE A: The thermal pad is electrically isolated from all terminals in the package.

Figure 33. Views of Thermally Enhanced DGN Package

Although there are many ways to properly heatsink this device, the following steps illustrate the recommended approach.

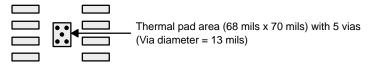


Figure 34. PowerPAD PCB Etch and Via Pattern

- 1. Prepare the PCB with a top side etch pattern as shown in Figure 34. There should be etch for the leads as well as etch for the thermal pad.
- 2. Place five holes in the area of the thermal pad. These holes should be 13 mils in diameter. Keep them small so that solder wicking through the holes is not a problem during reflow.
- 3. Additional vias may be placed anywhere along the thermal plane outside of the thermal pad area. This helps dissipate the heat generated by the THS401xDGN IC. These additional vias may be larger than the 13-mil diameter vias directly under the thermal pad. They can be larger because they are not in the thermal pad area to be soldered so that wicking is not a problem.
- 4. Connect all holes to the internal ground plane.
- 5. When connecting these holes to the ground plane, **do not** use the typical web or spoke via connection methodology. Web connections have a high thermal resistance connection that is useful for slowing the heat transfer during soldering operations. This makes the soldering of vias that have plane connections easier. In this application, however, low thermal resistance is desired for the most efficient heat transfer. Therefore, the holes under the THS401xDGN package should make their connection to the internal ground plane with a complete connection around the entire circumference of the plated-through hole.
- 6. The top-side solder mask should leave the terminals of the package and the thermal pad area with its five holes exposed. The bottom-side solder mask should cover the five holes of the thermal pad area. This prevents solder from being pulled away from the thermal pad area during the reflow process.
- 7. Apply solder paste to the exposed thermal pad area and all of the IC terminals.
- 8. With these preparatory steps in place, the THS401xDGN IC is simply placed in position and run through the solder reflow operation as any standard surface-mount component. This results in a part that is properly installed.



general PowerPAD design considerations (continued)

The actual thermal performance achieved with the THS401xDGN in its PowerPAD package depends on the application. In the example above, if the size of the internal ground plane is approximately 3 inches \times 3 inches, then the expected thermal coefficient, θ_{JA} , is about 58.4°C/W. For comparison, the non-PowerPAD version of the THS401x IC (SOIC) is shown. For a given θ_{JA} , the maximum power dissipation is shown in Figure 35 and is calculated by the following formula:

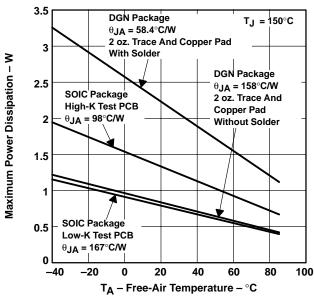
$$\begin{split} P_D &= \left(\frac{T_{MA} x^{-T} A}{\theta_{JA}}\right) \\ \text{Where:} &\qquad P_D &= \text{Maximum power dissipation of THS401x IC (watts)} \\ T_{MAX} &= \text{Absolute maximum junction temperature (150°C)} \\ T_A &= \text{Free-ambient air temperature (°C)} \end{split}$$

 $\theta_{JA} = \theta_{JC} + \theta_{CA}$

 θ_{JC} = Thermal coefficient from junction to case

 θ_{CA} = Thermal coefficient from case to ambient air (°C/W)

MAXIMUM POWER DISSIPATION vs FREE-AIR TEMPERATURE



NOTE A: Results are with no air flow and PCB size = $3"\times 3"$

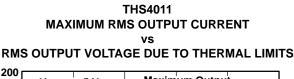
Figure 35. Maximum Power Dissipation vs Free-Air Temperature

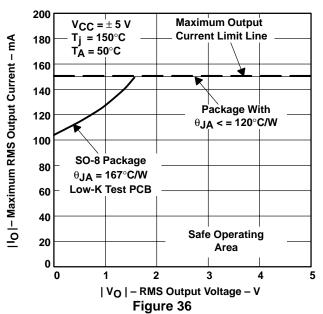
More complete details of the PowerPAD installation process and thermal management techniques can be found in the Texas Instruments Technical Brief, *PowerPAD Thermally Enhanced Package*. This document can be found at the TI web site (www.ti.com) by searching on the key word PowerPAD. The document can also be ordered through your local TI sales office. Refer to literature number SLMA002 when ordering.



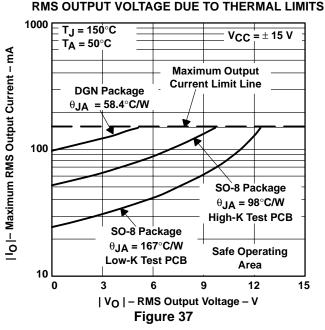
general PowerPAD design considerations (continued)

The next consideration is the package constraints. The two sources of heat within an amplifier are quiescent power and output power. The designer should never forget about the quiescent heat generated within the device, especially muti-amplifier devices. Because these devices have linear output stages (Class A-B), most of the heat dissipation is at low output voltages with high output currents. Figure 36 to Figure 39 show this effect, along with the quiescent heat, with an ambient air temperature of 50°C. When using $V_{CC} = \pm 5$ V, there is generally not a heat problem, even with SOIC packages. But, when using $V_{CC} = \pm 15$ V, the SOIC package is severely limited in the amount of heat it can dissipate. The other key factor when looking at these graphs is how the devices are mounted on the PCB. The PowerPAD devices are extremely useful for heat dissipation. But, the device should always be soldered to a copper plane to fully use the heat dissipation properties of the PowerPAD. The SOIC package, on the other hand, is highly dependent on how it is mounted on the PCB. As more trace and copper area is placed around the device, θ_{JA} decreases and the heat dissipation capability increases. The currents and voltages shown in these graphs are for the total package. For the dual amplifier package (THS4012), the sum of the RMS output currents and voltages should be used to choose the proper package.



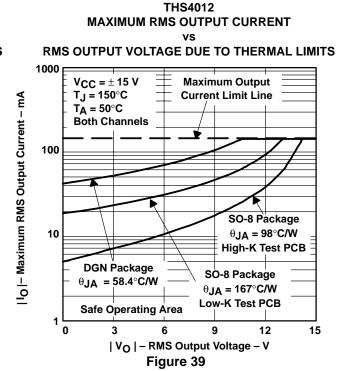


THS4011 MAXIMUM RMS OUTPUT CURRENT vs



general PowerPAD design considerations (continued)

THS4012 **MAXIMUM RMS OUTPUT CURRENT** vs RMS OUTPUT VOLTAGE DUE TO THERMAL LIMITS **Maximum Output** Package With $\theta_{JA} \le 60^{\circ} \text{C/W}$ **Current Limit Line** |IO|- Maximum RMS Output Current - mA 180 160 140 120 100 SO-8 Package $\theta_{JA} = 167^{\circ}\text{C/W}$ 80 Low-K Test PCB 60 Safe Operating Area $V_{CC} = \pm 5 V$ 40 SO-8 Package T_J = 150°C $\theta_{\text{J}}\Delta = 98^{\circ}\text{C/W}$ $T_A = 50^{\circ}C$ 20 **High-K Test PCB Both Channels** 0 3 0 5 | V_O | – RMS Output Voltage – V Figure 38



evaluation board

An evaluation board is available for the THS4011 (literature number SLOP128) and THS4012 (literature number SLOP230). This board has been configured for very low parasitic capacitance in order to realize the full performance of the amplifier. A schematic of the THS4011 evaluation board is shown in Figure 40. The circuitry has been designed so that the amplifier may be used in either an inverting or noninverting configuration. For more information, please refer to the THS4011 EVM User's Guide (literature number SLOU028) or the THS4012 EVM User's Guide (literature number SLOU041) To order the evaluation board contact your local TI sales office or distributor.

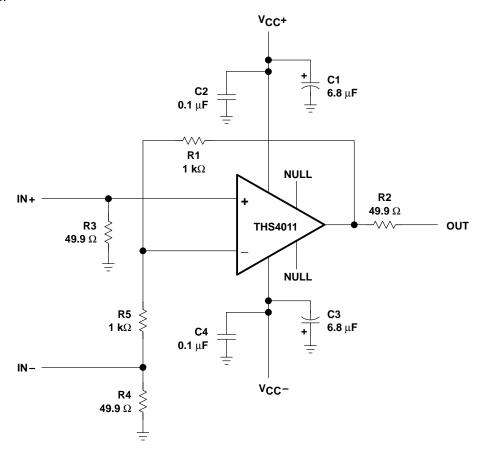


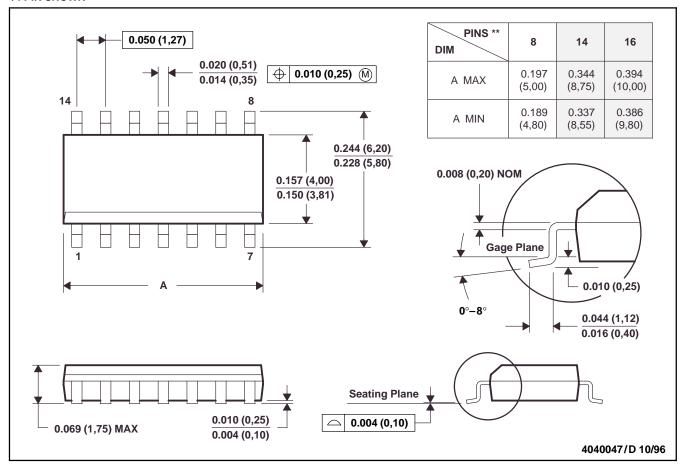
Figure 40. THS4011 Evaluation Board

MECHANICAL INFORMATION

D (R-PDSO-G**)

PLASTIC SMALL-OUTLINE PACKAGE

14 PIN SHOWN



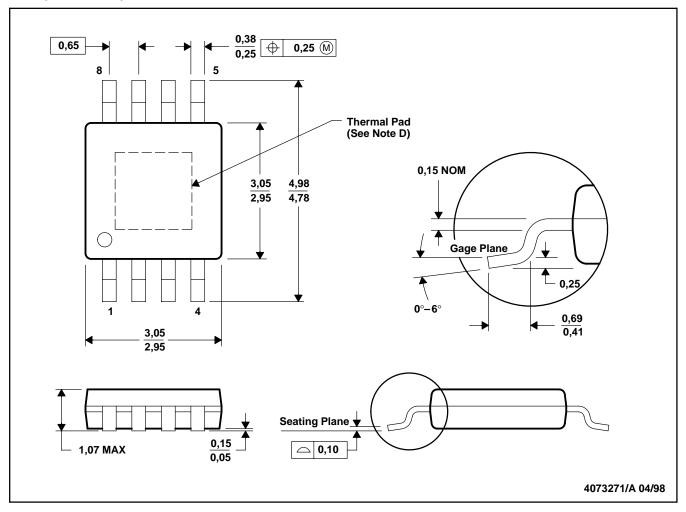
NOTES: A. All linear dimensions are in inches (millimeters).

- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion, not to exceed 0.006 (0,15).
- D. Falls within JEDEC MS-012

MECHANICAL INFORMATION

DGN (S-PDSO-G8)

PowerPAD™ PLASTIC SMALL-OUTLINE PACKAGE



NOTES: A. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. Body dimensions include mold flash or protrusions.
- D. The package thermal performance may be enhanced by attaching an external heat sink to the thermal pad. This pad is electrically and thermally connected to the backside of the die and possibly selected leads.
- E. Falls within JEDEC MO-187

PowerPAD is a trademark of Texas Instruments Incorporated.

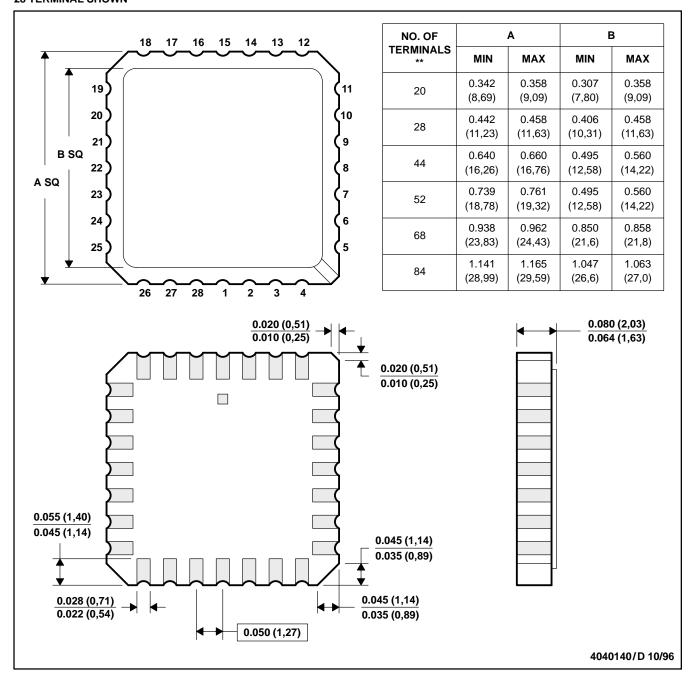


MECHANICAL INFORMATION

FK (S-CQCC-N**)

LEADLESS CERAMIC CHIP CARRIER

28 TERMINAL SHOWN



NOTES: A. All linear dimensions are in inches (millimeters).

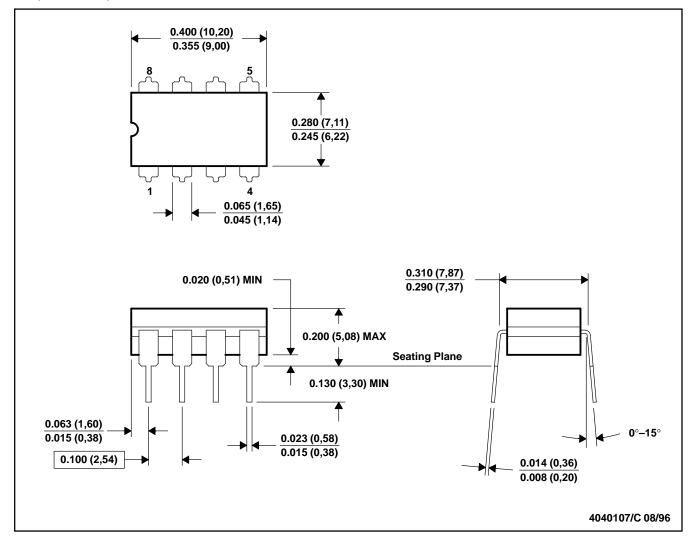
- This drawing is subject to change without notice.
- This package can be hermetically sealed with a metal lid.
- D. The terminals are gold plated.
- E. Falls within JEDEC MS-004



MECHANICAL INFORMATION

JG (R-GDIP-T8)

CERAMIC DUAL-IN-LINE PACKAGE



NOTES: A. All linear dimensions are in inches (millimeters).

- B. This drawing is subject to change without notice.
- C. This package can be hermetically sealed with a ceramic lid using glass frit.
- D. Index point is provided on cap for terminal identification only on press ceramic glass frit seal only.
- E. Falls within MIL-STD-1835 GDIP1-T8



PACKAGING INFORMATION

Orderable Device	Status ⁽¹⁾	Package Type	Package Drawing	Pins	Package Qty	e Eco Plan ⁽²⁾	Lead/Ball Finish	MSL Peak Temp ⁽³⁾
5962-9959301Q2A	ACTIVE	LCCC	FK	20	1	None	POST-PLATE	Level-NC-NC-NC
5962-9959301QPA	ACTIVE	CDIP	JG	8	1	None	A42 SNPB	Level-NC-NC-NC
THS4011CD	ACTIVE	SOIC	D	8	75	Pb-Free (RoHS)	CU NIPDAU	Level-2-260C-1YEAR/ Level-1-220C-UNLIM
THS4011CDGN	ACTIVE	MSOP- Power PAD	DGN	8	80	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4011CDGNG4	ACTIVE	MSOP- Power PAD	DGN	8	80	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4011CDGNR	ACTIVE	MSOP- Power PAD	DGN	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4011CDR	ACTIVE	SOIC	D	8	2500	Pb-Free (RoHS)	CU NIPDAU	Level-2-260C-1YEAR/ Level-1-220C-UNLIM
THS4011ID	ACTIVE	SOIC	D	8	75	Pb-Free (RoHS)	CU NIPDAU	Level-2-260C-1YEAR/ Level-1-220C-UNLIM
THS4011IDGN	ACTIVE	MSOP- Power PAD	DGN	8	80	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4011IDGNR	ACTIVE	MSOP- Power PAD	DGN	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4011IDGNRG4	ACTIVE	MSOP- Power PAD	DGN	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4011IDR	ACTIVE	SOIC	D	8	2500	Pb-Free (RoHS)	CU NIPDAU	Level-2-260C-1YEAR/ Level-1-220C-UNLIM
THS4011MFKB	ACTIVE	LCCC	FK	20	1	None	POST-PLATE	Level-NC-NC-NC
THS4011MJG	ACTIVE	CDIP	JG	8	1	None	A42 SNPB	Level-NC-NC-NC
THS4011MJGB	ACTIVE	CDIP	JG	8	1	None	A42 SNPB	Level-NC-NC-NC
THS4012CD	ACTIVE	SOIC	D	8	75	Pb-Free (RoHS)	CU NIPDAU	Level-2-260C-1YEAR/ Level-1-220C-UNLIM
THS4012CDGN	ACTIVE	MSOP- Power PAD	DGN	8	80	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4012CDGNR	ACTIVE	MSOP- Power PAD	DGN	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4012CDGNRG4	ACTIVE	MSOP- Power PAD	DGN	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4012CDR	ACTIVE	SOIC	D	8	2500	Pb-Free (RoHS)	CU NIPDAU	Level-2-260C-1YEAR/ Level-1-220C-UNLIM
THS4012ID	ACTIVE	SOIC	D	8	75	Pb-Free (RoHS)	CU NIPDAU	Level-2-260C-1YEAR/ Level-1-220C-UNLIM
THS4012IDGN	ACTIVE	MSOP- Power PAD	DGN	8	80	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4012IDGNR	ACTIVE	MSOP-	DGN	8	2500	Green (RoHS &	CU NIPDAU	Level-1-260C-UNLIM



PACKAGE OPTION ADDENDUM

22-Feb-2005

Orderable Device	Status ⁽¹⁾	Package Type	Package Drawing	Pins Pa	ackage Qty	e Eco Plan ⁽²⁾	Lead/Ball Finish	MSL Peak Temp ⁽³⁾
		Power PAD				no Sb/Br)		
THS4012IDGNRG4	ACTIVE	MSOP- Power PAD	DGN	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
THS4012IDR	ACTIVE	SOIC	D	8	2500	Pb-Free (RoHS)	CU NIPDAU	Level-2-260C-1YEAR/ Level-1-220C-UNLIM

⁽¹⁾ The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - May not be currently available - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

None: Not yet available Lead (Pb-Free).

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Green (RoHS & no Sb/Br): TI defines "Green" to mean "Pb-Free" and in addition, uses package materials that do not contain halogens, including bromine (Br) or antimony (Sb) above 0.1% of total product weight.

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDECindustry standard classifications, and peak solder temperature.

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