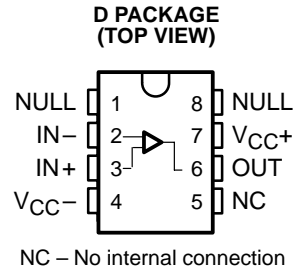


THS4001 270-MHz HIGH-SPEED AMPLIFIER

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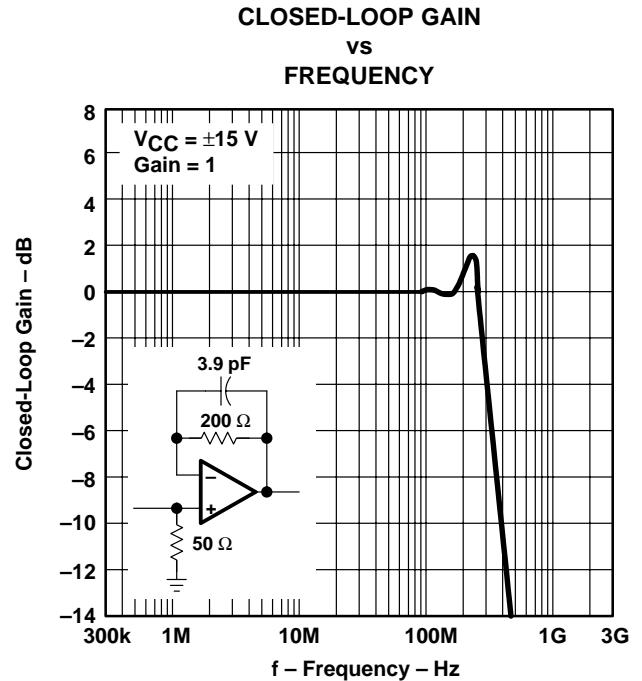
- **Very High Speed**
 - 270 MHz Bandwidth (Gain = 1, –3 dB)
 - 400 V/ μ sec Slew Rate
 - 40-ns Settling Time (0.1%)
- **High Output Drive, $I_O = 100$ mA**
- **Excellent Video Performance**
 - 60 MHz Bandwidth (0.1 dB, G = 1)
 - 0.04% Differential Gain
 - 0.15° Differential Phase
- **Very Low Distortion**
 - THD = –72 dBc at $f = 1$ MHz
- **Wide Range of Power Supplies**
 $V_{CC} = \pm 2.5$ V to ± 15 V,
 $I_{CC} = 7.5$ mA
- **Evaluation Module Available**



description

The THS4001 is a very high-performance, voltage-feedback operational amplifier especially suited for a wide range of video applications. The device is specified to operate over a wide range of supply voltages from ± 15 V to ± 2.5 V. With a bandwidth of 270 MHz, a slew rate of over 400 V/ μ s, and settling times of less than 30 ns, the THS4001 offers the unique combination of high performance in an easy to use voltage feedback configuration over a wide range of power supply voltages.

The THS4001 is stable at all gains for both inverting and noninverting configurations. It has a high output drive capability of 100 mA and draws only 7.5 mA of quiescent current. Excellent professional video results can be obtained with the differential gain/phase performance of 0.04%/0.15° and 0.1 dB gain flatness to 60 MHz. For applications requiring low distortion, the THS4001 is ideally suited with total harmonic distortion of –72 dBc at $f = 1$ MHz.



HIGH-SPEED AMPLIFIER FAMILY

| DEVICE | ARCH. | | SUPPLY VOLTAGE | | | BW (MHz) | SR (V/ μ s) | THD $f = 1$ MHz (dB) | t_s 0.1% (ns) | DIFF. GAIN | DIFF. PHASE | V_n (nV/ $\sqrt{\text{Hz}}$) |
|------------|-------|-----|----------------|-----------|------------|----------|-----------------|----------------------|-----------------|------------|-------------|---------------------------------|
| | VFB | CFB | 5 V | ± 5 V | ± 15 V | | | | | | | |
| THS3001 | | • | | • | • | 420 | 6500 | –96 | 40 | 0.01% | 0.02° | 1.6 |
| THS4001 | • | | • | • | • | 270 | 400 | –72 | 40 | 0.04% | 0.15° | 12.5 |
| THS4031/32 | • | | | • | • | 100 | 100 | –72 | 60 | 0.02% | 0.03° | 1.6 |
| THS4061/62 | • | | | • | • | 180 | 400 | –72 | 40 | 0.02% | 0.02° | 14.5 |



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

PRODUCTION DATA information is current as of publication date. Products conform to specifications per the terms of Texas Instruments standard warranty. Production processing does not necessarily include testing of all parameters.

**TEXAS
INSTRUMENTS**

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THS4001 270-MHz HIGH-SPEED AMPLIFIER

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recommended operating conditions

| | | MIN | TYP | MAX | UNIT |
|---------------------------------------|------------------------|-----------|-----|----------|--------------|
| Supply voltage, V_{CC} | Dual supply | ± 2.5 | | ± 16 | V |
| | Single supply | 5 | | 32 | |
| Quiescent current, I_{CC} | ± 15 V | | 7.8 | 9.5 | mA |
| | ± 5 V, ± 2.5 V | | 6.7 | 8 | |
| Operating free-air temperature, T_A | C suffix | | 0 | 70 | $^{\circ}$ C |
| | I suffix | | -40 | 85 | |

electrical characteristics, $V_{CC} = \pm 15$ V, $R_L = 150 \Omega$, $T_A = 25^{\circ}$ C (unless otherwise noted)

| PARAMETER | TEST CONDITIONS | V_{CC} | MIN | TYP | MAX | UNIT |
|---|--|---------------------------|-------------------|-------------------|-----|------------|
| Differential gain error | Gain = 2, $R_L = 150 \Omega$, $f = 3.58$ MHz | ± 15 V | | 0.04% | | |
| | | ± 5 V | | 0.01% | | |
| Differential phase error | | ± 15 V | | 0.15 $^{\circ}$ | | |
| | | ± 5 V | | 0.08 $^{\circ}$ | | |
| V_{IO} Input offset voltage | $T_A = 25^{\circ}$ C | ± 15 V, | | 2 | 8 | mV |
| | $T_A = \text{full range}$ | ± 5 V | | | 10 | |
| I_{IB} Input bias current | $T_A = 25^{\circ}$ C | ± 15 V, | | 2.6 | 5 | μ A |
| | $T_A = \text{full range}$ | ± 5 V | | | 6 | |
| I_{OS} Input offset current | $T_A = 25^{\circ}$ C | ± 15 V, | | 35 | 200 | nA |
| | $T_A = \text{full range}$ | ± 5 V | | | 500 | |
| Open-loop gain | $V_O = \pm 10$ V, $R_L = 1$ k Ω | $T_A = 25^{\circ}$ C | ± 15 V | 5 | 10 | V/mV |
| | | $T_A = \text{full range}$ | | 3 | | |
| | $V_O = \pm 2.5$ V, $R_L = 500 \Omega$ | $T_A = 25^{\circ}$ C | ± 5 V | 3 | 6 | |
| | | $T_A = \text{full range}$ | | 2 | | |
| CMRR Common-mode rejection ratio | $V_{(CM)} = \pm 12$ V | $T_A = 25^{\circ}$ C | ± 15 V | 85 | 100 | dB |
| | | $T_A = \text{full range}$ | | 75 | | |
| PSRR Power supply rejection ratio | $T_A = 25^{\circ}$ C | ± 15 V, | | 75 | 85 | dB |
| | $T_A = \text{full range}$ | ± 5 V | | 70 | | |
| V_{ICR} Common-mode input voltage range | | ± 15 V | 13.5 to -13 | 14.8 to -14 | | V |
| | | ± 5 V | 3.6 to -2.7 | 4.4 to -3.6 | | |
| V_O Output voltage swing | $R_L = 500 \Omega$ | ± 15 V | ± 13 | ± 13.5 | | V |
| | | ± 5 V | ± 3.3 | ± 3.8 | | |
| | | ± 2.5 V | ± 0.8 | ± 1.3 | | |
| I_O Output current | Gain = 2, $R_L = 20 \Omega$ | ± 15 V | 50 | 100 | | mA |
| | | ± 5 V | 50 | 100 | | |
| | | ± 2.5 V | 50 | 100 | | |
| THD Total harmonic distortion | $V_I = 1$ V _(PP) , $f = 1$ MHz | ± 15 V | | -72 | | dBc |
| R_I Input resistance | | | | 10 | | M Ω |
| C_I Input capacitance | | | | 1.5 | | pF |
| R_O Output resistance | Open loop | | | 10 | | Ω |



THS4001

270-MHz HIGH-SPEED AMPLIFIER

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operating characteristics, $V_{CC} = \pm 15\text{ V}$, $R_L = 150\ \Omega$, $T_A = 25^\circ\text{C}$ (unless otherwise noted)

| PARAMETER | TEST CONDITIONS | V_{CC} | MIN | TYP | MAX | UNIT |
|-------------------------------|----------------------------------|---------------------|---|------|-----|------------------------------|
| Slew rate | Gain = -1 | $\pm 15\text{ V}$ | | 400 | | $\text{V}/\mu\text{s}$ |
| | | $\pm 5\text{ V}$ | | 400 | | |
| | | $\pm 2.5\text{ V}$ | | 350 | | |
| Settling time to 0.1% | 10 V step (0 to 10 V), Gain = -1 | $\pm 15\text{ V}$ | | 40 | | ns |
| | -2.5 V to 2.5 V step, Gain = -1 | $\pm 5\text{ V}$ | | 30 | | |
| -3 dB Bandwidth | Gain = +1, $R_f = 150\ \Omega$ | $\pm 15\text{ V}$ | | 270 | | MHz |
| | | $\pm 5\text{ V}$ | | 220 | | |
| | | $\pm 2.5\text{ V}$ | | 180 | | |
| | Gain = -1, $R_f = 150\ \Omega$ | $\pm 15\text{ V}$ | | 80 | | MHz |
| | | $\pm 5\text{ V}$ | | 75 | | |
| | | $\pm 2.5\text{ V}$ | | 70 | | |
| Bandwidth for 0.1 dB flatness | Gain = +1 | $\pm 15\text{ V}$ | | 60 | | MHz |
| | | $\pm 5\text{ V}$ | | 50 | | |
| | | $\pm 2.5\text{ V}$ | | 40 | | |
| V_n | Equivalent input noise voltage | $f = 10\text{ kHz}$ | $\pm 15\text{ V}$, $\pm 5\text{ V}$ | 12.5 | | $\text{nV}/\sqrt{\text{Hz}}$ |
| I_n | Equivalent input noise current | $f = 10\text{ kHz}$ | $\pm 15\text{ V}$, $\pm 5\text{ V}$ | 1.5 | | $\text{pA}/\sqrt{\text{Hz}}$ |

TYPICAL CHARACTERISTICS

Table of Graphs

| | | FIGURE | |
|-------------|------------------------------|-------------------------|--------|
| I_{IB} | Input bias current | vs Free-air temperature | 1 |
| V_{IO} | Input offset voltage | vs Free-air temperature | 2 |
| | Open-loop gain | vs Frequency | 3 |
| | Phase | vs Frequency | 3 |
| | Differential gain | vs DC voltage | 4, 5 |
| | Differential phase | vs DC voltage | 4, 5 |
| | Closed-loop gain | vs Frequency | 6, 7 |
| CMRR | Common-mode rejection ratio | vs Frequency | 8 |
| PSRR | Power-supply rejection ratio | vs Frequency | 9 |
| | | vs Free-air temperature | 10 |
| $V_{O(PP)}$ | Output voltage swing | vs Supply voltage | 11 |
| | | vs Load resistance | 12 |
| | Bandwidth (-3 dB) | vs Feedback resistance | 13, 14 |
| I_{CC} | Supply current | vs Supply voltage | 15 |
| | | vs Free-air temperature | 16 |
| E_{nv} | Noise spectral density | vs Frequency | 17 |
| THD | Total harmonic distortion | vs Frequency | 18 |

TYPICAL CHARACTERISTICS

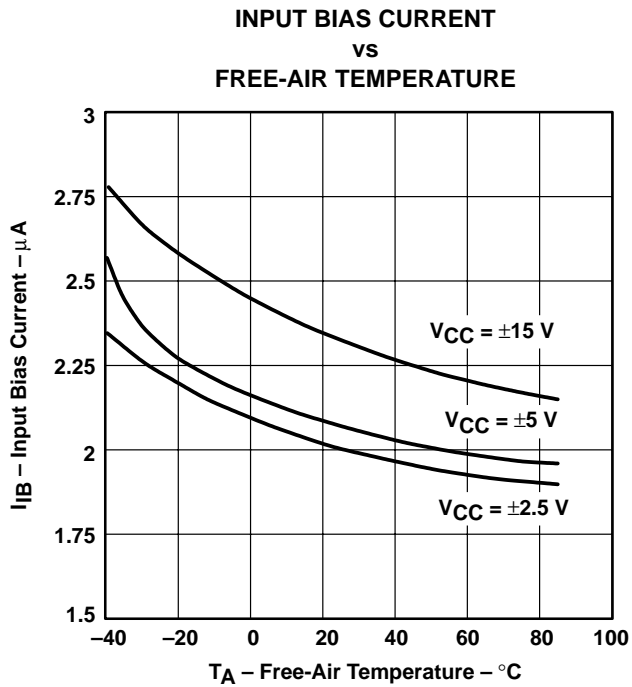


Figure 1

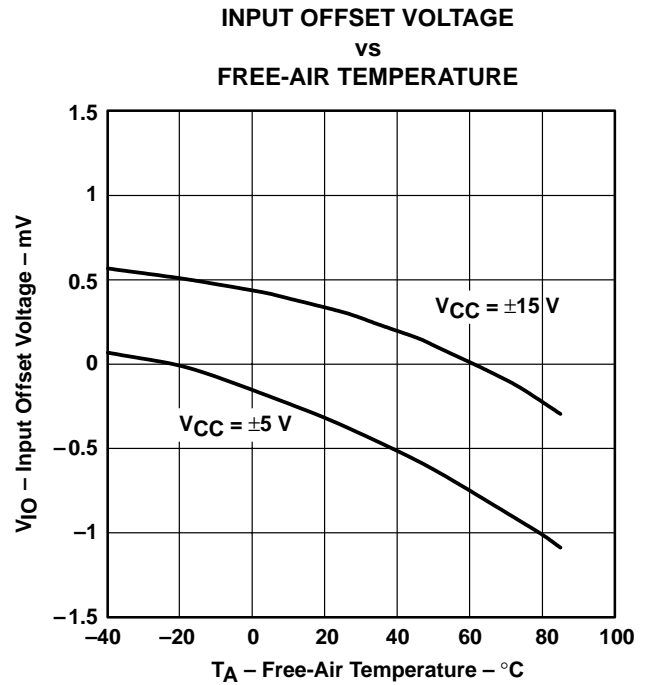


Figure 2

**OPEN-LOOP GAIN AND PHASE
vs
FREQUENCY**

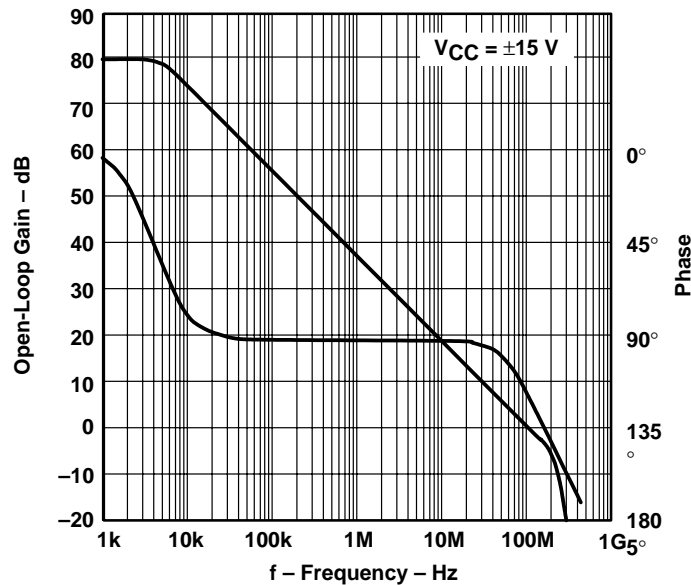


Figure 3

THS4001
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TYPICAL CHARACTERISTICS

**DIFFERENTIAL GAIN AND
DIFFERENTIAL PHASE
vs
DC VOLTAGE**

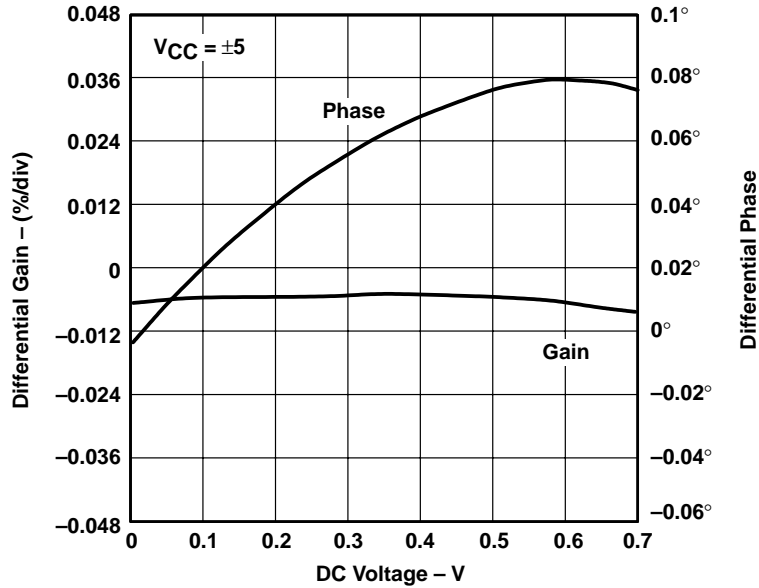


Figure 4

**DIFFERENTIAL GAIN AND
DIFFERENTIAL PHASE
vs
DC VOLTAGE**

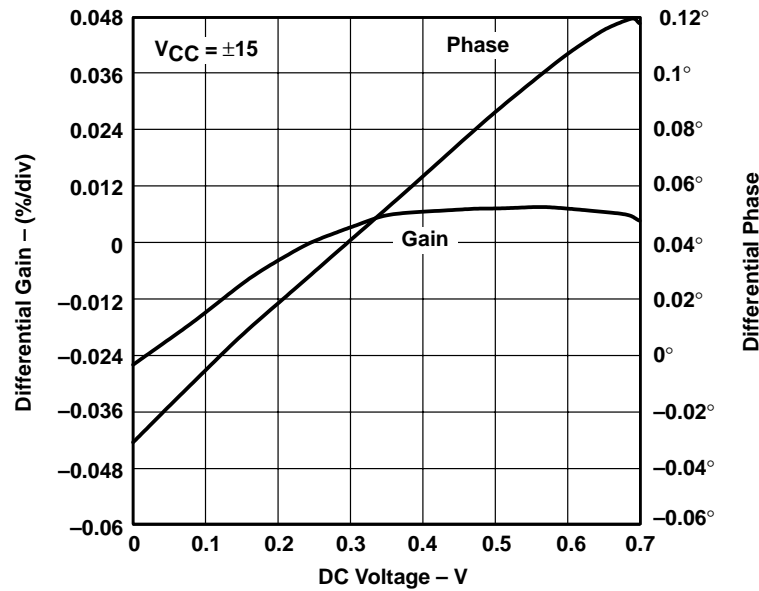


Figure 5



TYPICAL CHARACTERISTICS

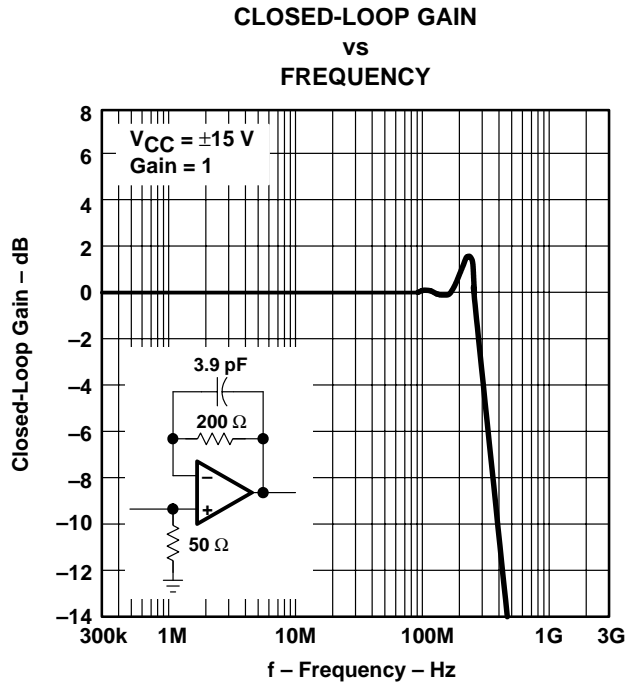


Figure 6

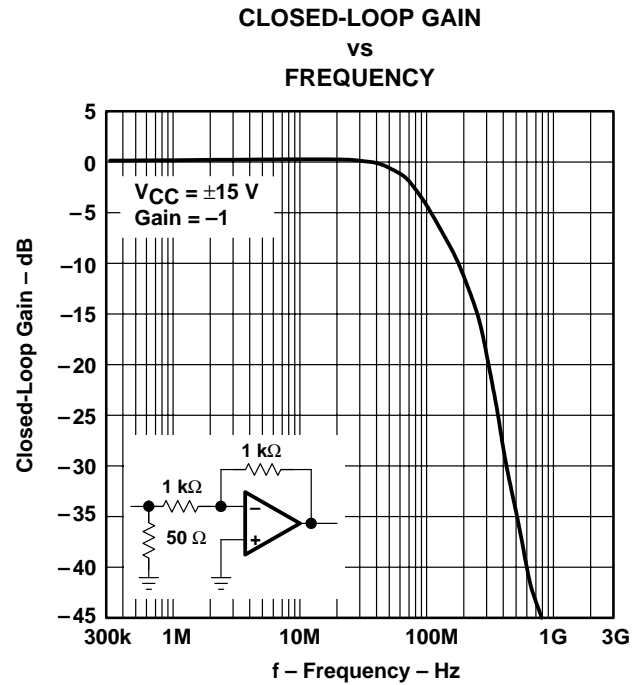


Figure 7

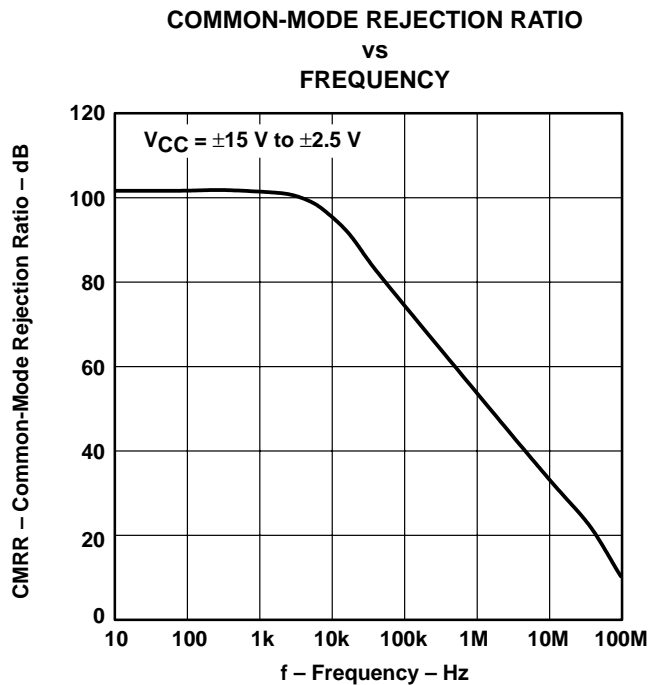


Figure 8

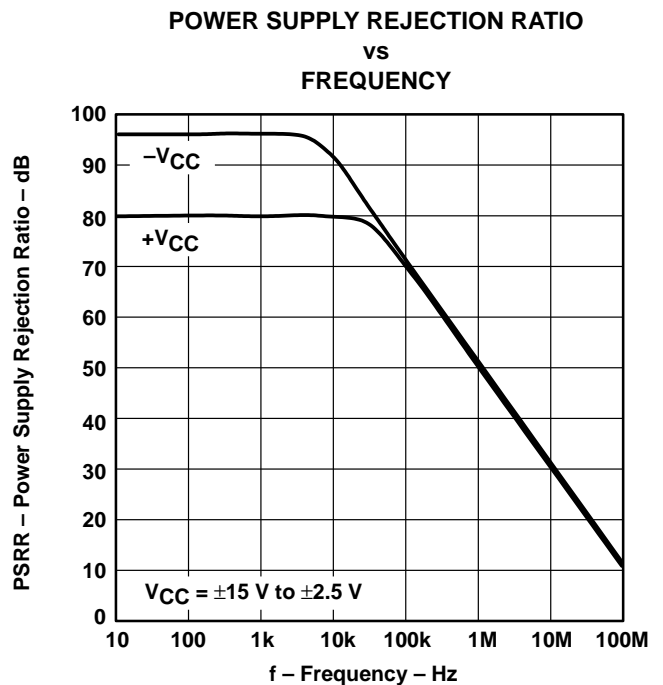


Figure 9

TYPICAL CHARACTERISTICS

POWER SUPPLY REJECTION RATIO
vs
FREE-AIR TEMPERATURE

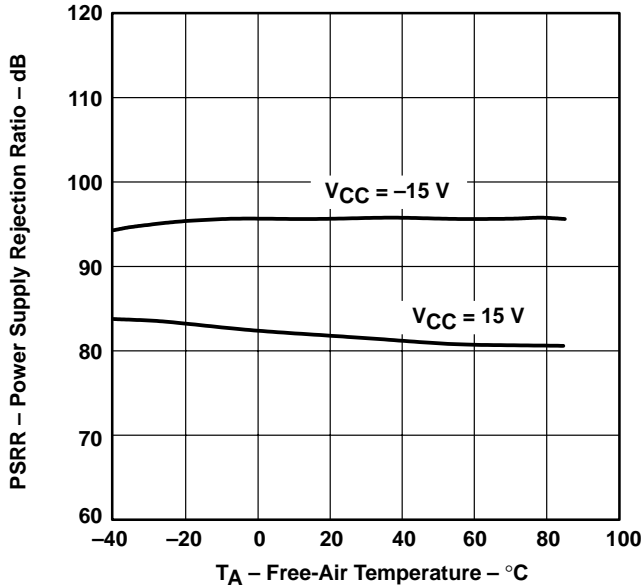


Figure 10

OUTPUT VOLTAGE SWING
vs
SUPPLY VOLTAGE

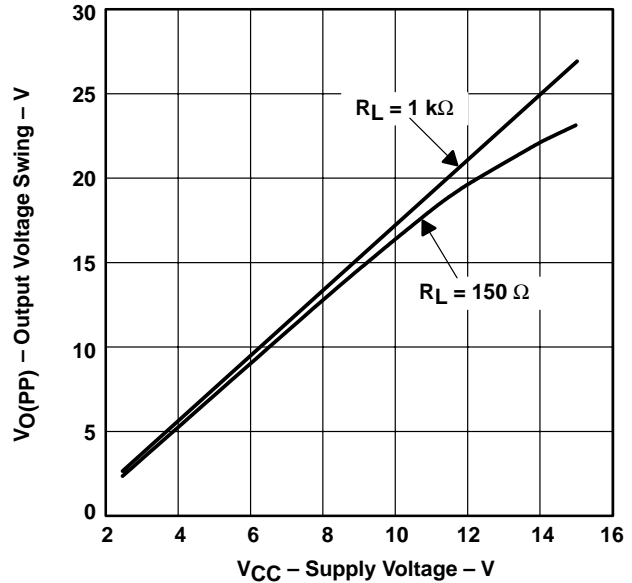


Figure 11

OUTPUT VOLTAGE SWING
vs
LOAD RESISTANCE

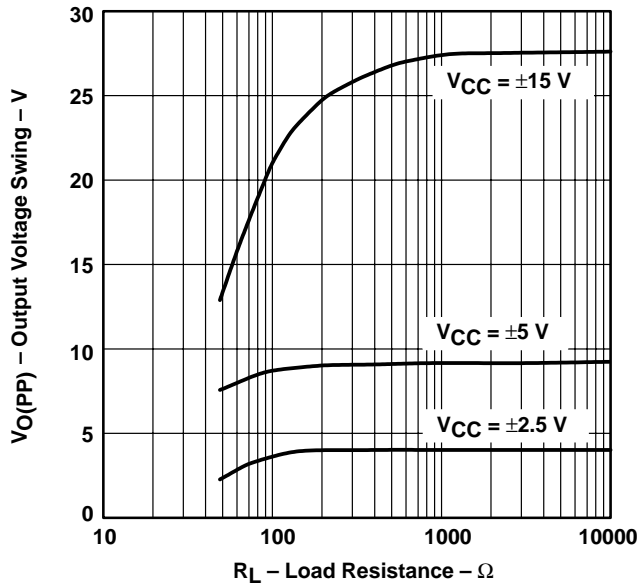


Figure 12

BANDWIDTH (-3 dB)
vs
FEEDBACK RESISTANCE

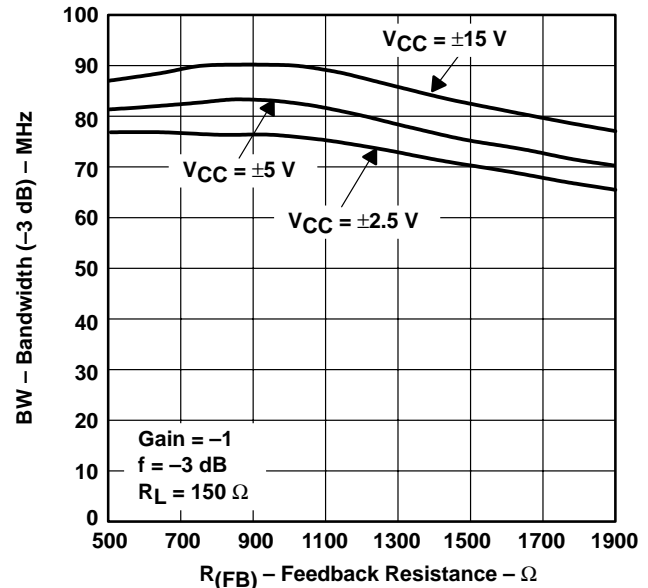


Figure 13

TYPICAL CHARACTERISTICS

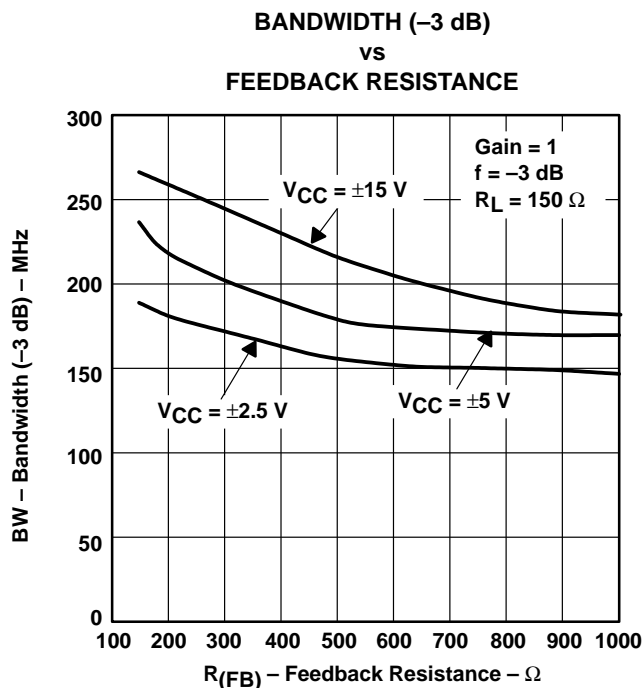


Figure 14

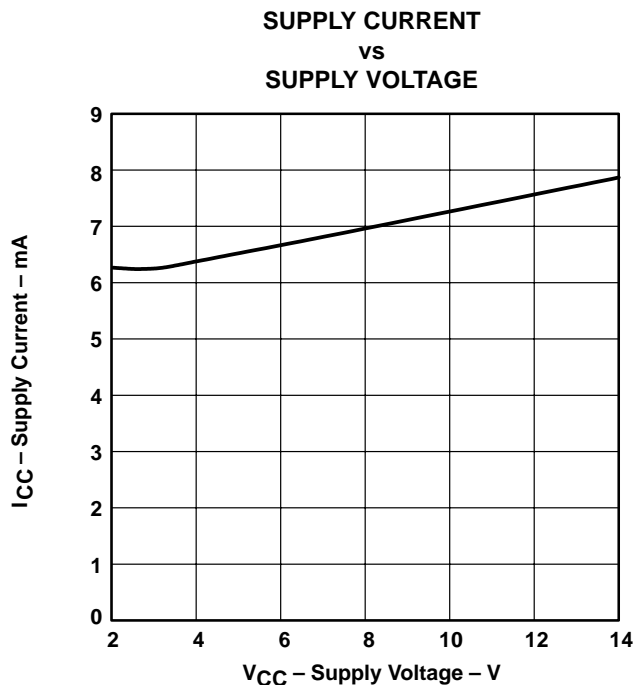


Figure 15

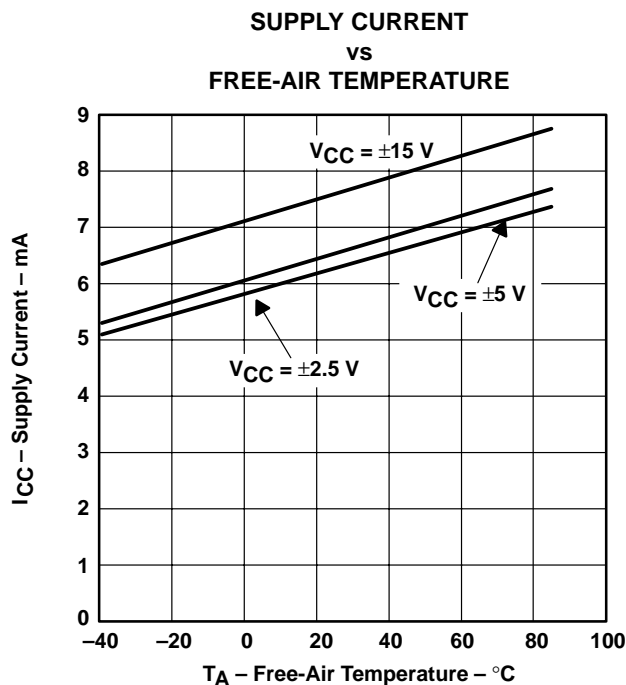


Figure 16

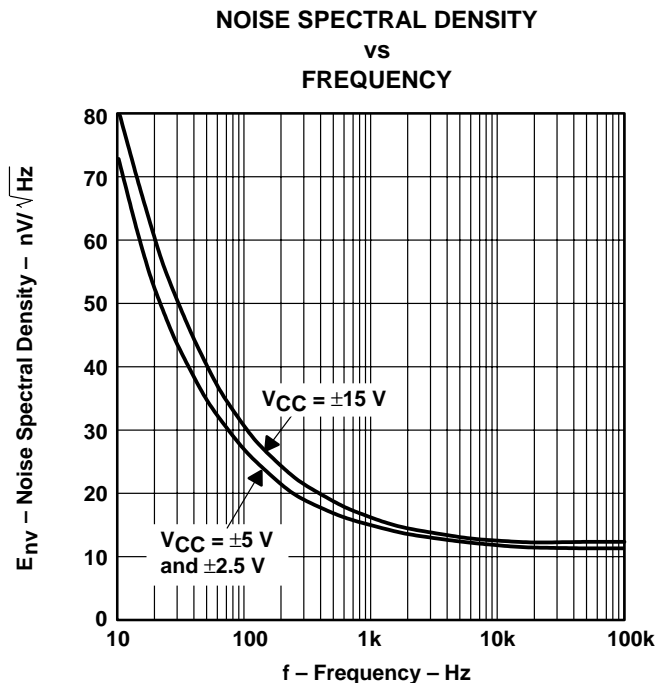


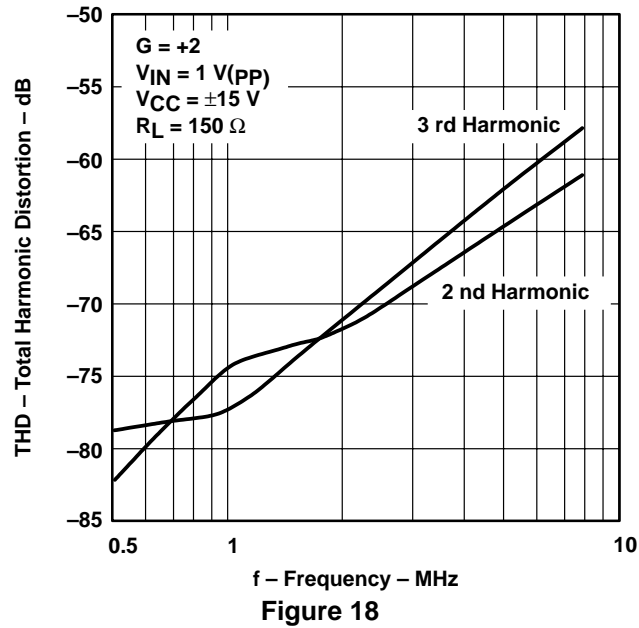
Figure 17

THS4001 270-MHz HIGH-SPEED AMPLIFIER

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TYPICAL CHARACTERISTICS

TOTAL HARMONIC DISTORTION vs FREQUENCY



APPLICATION INFORMATION

theory of operation

The THS4001 is a high speed, operational amplifier configured in a voltage feedback architecture. It is built using a 30-V, dielectrically isolated, complementary bipolar process with NPN and PNP transistors possessing f_T s of several GHz. This results in an exceptionally high performance amplifier that has a wide bandwidth, high slew rate, fast settling time, and low distortion. A simplified schematic is shown in Figure 19.

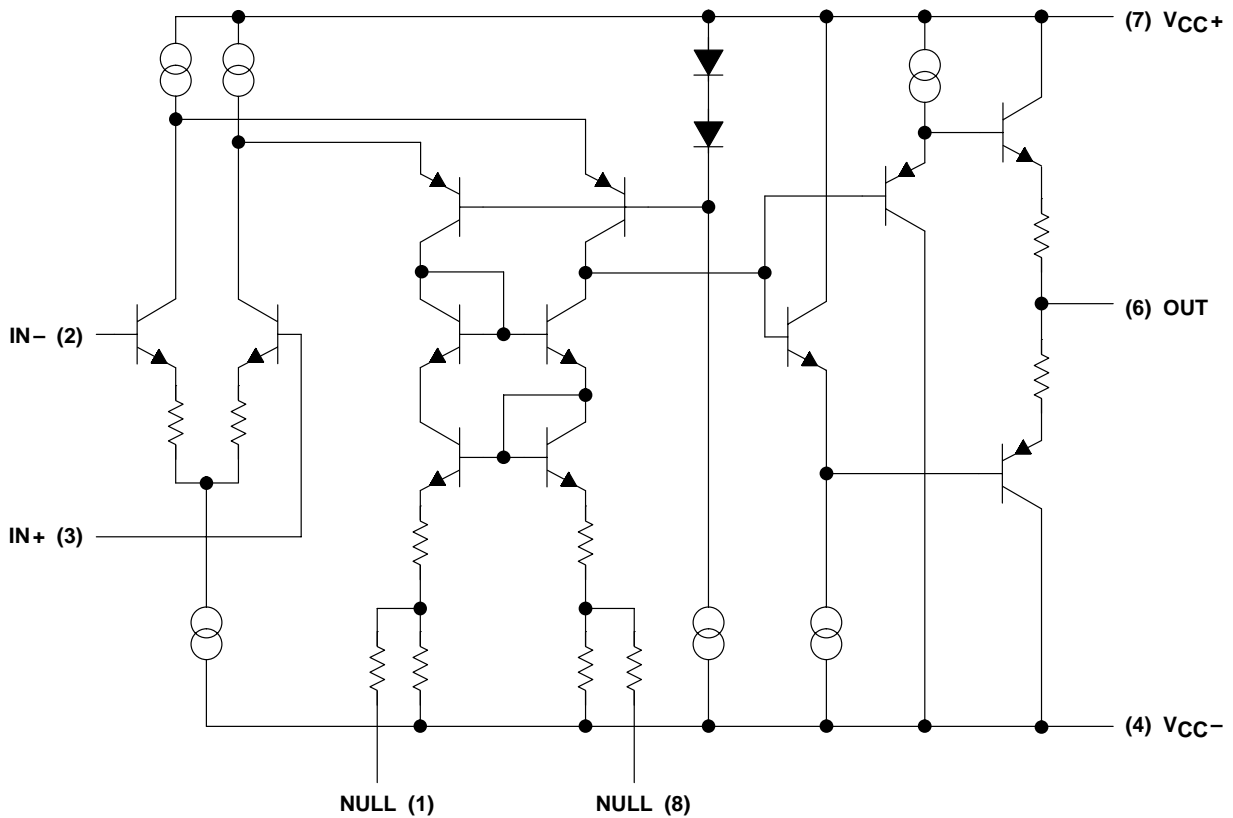


Figure 19. THS4001 Simplified Schematic

THS4001 270-MHz HIGH-SPEED AMPLIFIER

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APPLICATION INFORMATION

offset nulling

The THS4001 has very low input offset voltage for a high-speed amplifier. However, if additional correction is required, an offset nulling function has been provided. By placing a potentiometer between terminals 1 and 8 of the device and tying the wiper to the negative supply, the input offset can be adjusted. This is shown in Figure 20.

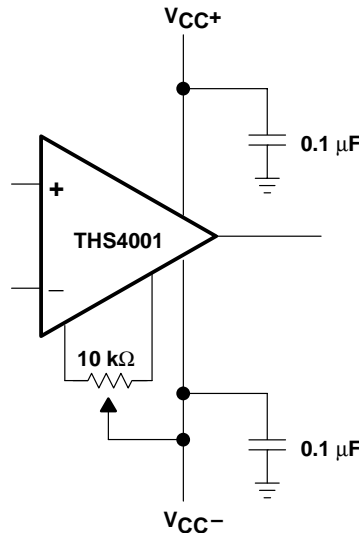


Figure 20. Offset Nulling Schematic

optimizing unity gain response

Internal frequency compensation of the THS4001 was selected to provide very wideband performance yet still maintain stability when operated in a noninverting unity gain configuration. When amplifiers are compensated in this manner there is usually peaking in the closed loop response and some ringing in the step response for very fast input edges, depending upon the application. This is because a minimum phase margin is maintained for the $G=+1$ configuration. For optimum settling time and minimum ringing, a feedback resistor of 200 Ω should be used as shown in Figure 21. Additional capacitance can also be used in parallel with the feedback resistance if even finer optimization is required.

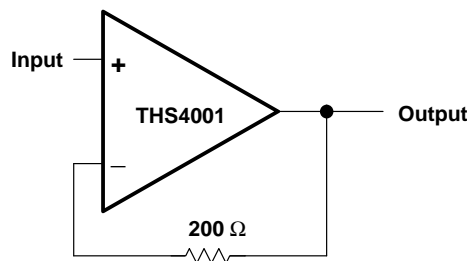


Figure 21. Noninverting, Unity Gain Schematic

APPLICATION INFORMATION

driving a capacitive load

Driving capacitive loads with high performance amplifiers is not a problem as long as certain precautions are taken. The first is to realize that the THS4001 has been internally compensated to maximize its bandwidth and slew rate performance. When the amplifier is compensated in this manner, capacitive loading directly on the output will decrease the device's phase margin leading to high frequency ringing or oscillations. Therefore, for capacitive loads of greater than 10 pF, it is recommended that a resistor be placed in series with the output of the amplifier, as shown in Figure 22. A minimum value of 20 Ω should work well for most applications. For example, in 75- Ω transmission systems, setting the series resistor value to 75 Ω both isolates any capacitance loading and provides the proper line impedance matching at the source end.

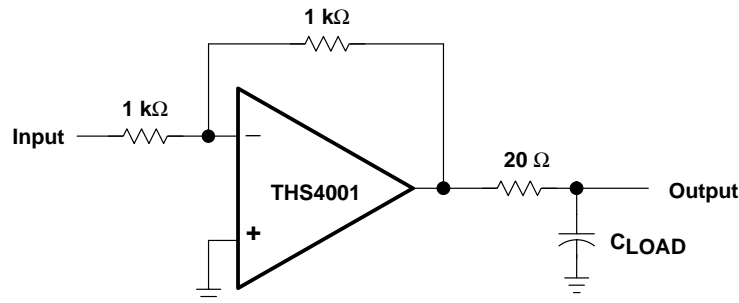


Figure 22. Driving a Capacitive Load

circuit layout considerations

In order to achieve the levels of high frequency performance of the THS4001, it is essential that proper printed-circuit board high frequency design techniques be followed. A general set of guidelines is given below. In addition, a THS4001 evaluation board is available to use as a guide for layout or for evaluating the device performance.

- Ground planes – It is highly recommended that a ground plane be used on the board to provide all components with a low inductive ground connection. However, in the areas of the amplifier inputs and output, the ground plane can be removed to minimize the stray capacitance.
- Proper power supply decoupling – Use a 6.8- μ F tantalum capacitor in parallel with a 0.1- μ F ceramic capacitor on each supply terminal. It may be possible to share the tantalum among several amplifiers depending on the application, but a 0.1- μ F ceramic capacitor should always be used on the supply terminal of every amplifier. In addition, the 0.1- μ F capacitor should be placed as close as possible to the supply terminal. As this distance increases, the inductance in the connecting trace makes the capacitor less effective. The designer should strive for distances of less than 0.1 inches between the device power terminals and the ceramic capacitors.
- Sockets – Sockets are not recommended for high speed op amps. The additional lead inductance in the socket pins will often lead to stability problems. Surface-mount packages soldered directly to the printed-circuit board is the best implementation.
- Short trace runs/compact part placements – Optimum high frequency performance is achieved when stray series inductance has been minimized. To realize this, the circuit layout should be made as compact as possible thereby minimizing the length of all trace runs. Particular attention should be paid to the inverting input of the amplifier. Its length should be kept as short as possible. This will help to minimize stray capacitance at the input of the amplifier.

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APPLICATION INFORMATION

circuit layout considerations (continued)

- Surface-mount passive components – Using surface mount passive components is recommended for high frequency amplifier circuits for several reasons. First, because of the extremely low lead inductance of surface-mount components, the problem with stray series inductance is greatly reduced. Second, the small size of surface-mount components naturally leads to a more compact layout thereby minimizing both stray inductance and capacitance. If leaded components are used, it is recommended that the lead lengths be kept as short as possible.

evaluation board

An evaluation board is available for the THS4001 (literature number SLOP119). This board has been configured for very low parasitic capacitance in order to realize the full performance of the amplifier. A schematic of the evaluation board is shown in Figure 23. The circuitry has been designed so that the amplifier may be used in either an inverting or noninverting configuration. To order the evaluation board contact your local TI sales office or distributor. For more detailed information, refer to the *THS4001 EVM User's Manual* (literature number SLOU017).

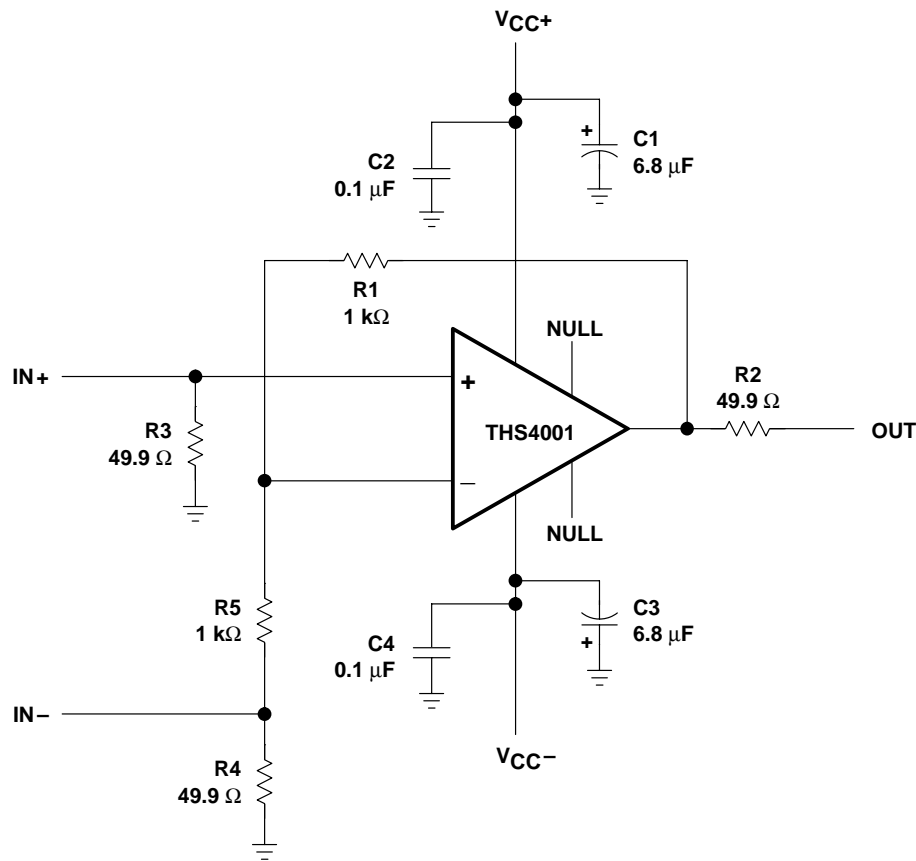


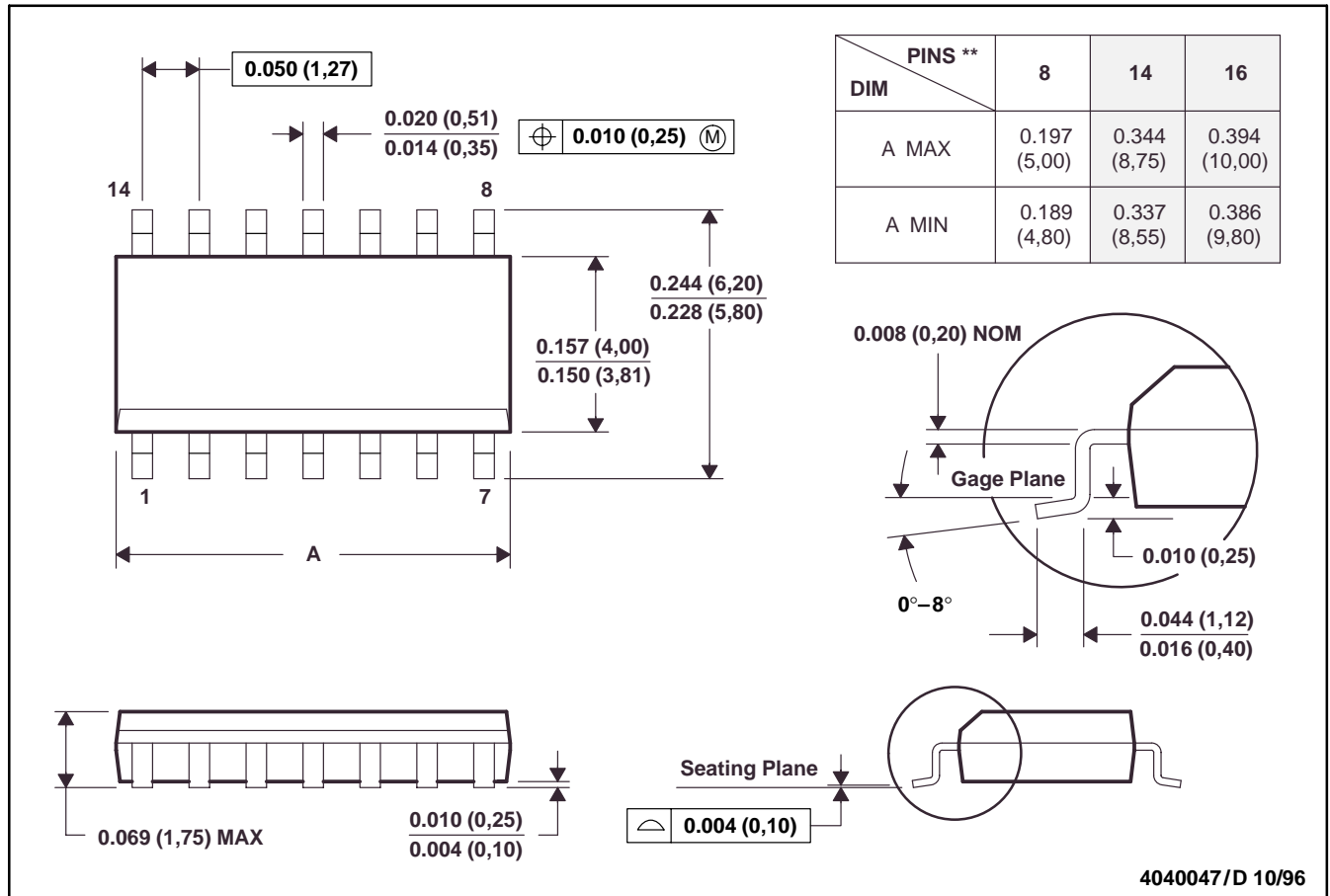
Figure 23.

MECHANICAL INFORMATION

D (R-PDSO-G**)

PLASTIC SMALL-OUTLINE PACKAGE

14 PIN SHOWN



- NOTES: A. All linear dimensions are in inches (millimeters).
 B. This drawing is subject to change without notice.
 C. Body dimensions do not include mold flash or protrusion, not to exceed 0.006 (0,15).
 D. Falls within JEDEC MS-012

PACKAGING INFORMATION

| Orderable Device | Status ⁽¹⁾ | Package Type | Package Drawing | Pins | Package Qty | Eco Plan ⁽²⁾ | Lead/Ball Finish | MSL Peak Temp ⁽³⁾ |
|------------------|-----------------------|--------------|-----------------|------|-------------|-------------------------|------------------|---|
| THS4001CD | ACTIVE | SOIC | D | 8 | 75 | Pb-Free (RoHS) | CU NIPDAU | Level-2-260C-1YEAR/ Level-1-220C-UNLIM |
| THS4001CDR | ACTIVE | SOIC | D | 8 | 2500 | Pb-Free (RoHS) | CU NIPDAU | Level-2-260C-1YEAR/ Level-1-220C-UNLIM |
| THS4001ID | ACTIVE | SOIC | D | 8 | 75 | Pb-Free (RoHS) | CU NIPDAU | Level-2-260C-1YEAR/ Level-1-220C-UNLIM |
| THS4001IDR | ACTIVE | SOIC | D | 8 | 2500 | Pb-Free (RoHS) | CU NIPDAU | Level-2-260C-1YEAR/ Level-1-220C-UNLIM |

⁽¹⁾ The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ Eco Plan - May not be currently available - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

None: Not yet available Lead (Pb-Free).

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Green (RoHS & no Sb/Br): TI defines "Green" to mean "Pb-Free" and in addition, uses package materials that do not contain halogens, including bromine (Br) or antimony (Sb) above 0.1% of total product weight.

⁽³⁾ MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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