# TLC080, TLC081, TLC082, TLC083, TLC084, TLC085, TLC08xA FAMILY OF WIDE-BANDWIDTH HIGH-OUTPUT-DRIVE SINGLE SUPPLY OPERATIONAL AMPLIFIERS 

- Wide Bandwidth ... 10 MHz
- High Output Drive
- $\mathrm{I}_{\mathrm{OH}} \ldots 57 \mathrm{~mA}$ at $\mathrm{V}_{\mathrm{DD}}-1.5 \mathrm{~V}$
- I OL . . 55 mA at 0.5 V
- High Slew Rate
- SR+... 16 V/us
- SR-... 19 V/ $\mu \mathrm{s}$
- Wide Supply Range ... 4.5 V to 16 V
- Supply Current . . . $1.9 \mathrm{~mA} /$ Channel
- Ultralow Power Shutdown Mode IDD... $125 \mu \mathrm{~A} /$ Channel
- Low Input Noise Voltage . . . $8.5 \mathrm{nV} \sqrt{\mathrm{Hz}}$
- Wide $\mathrm{V}_{\mathrm{ICR}} \ldots 0$ to $\mathrm{V}_{\mathrm{DD}}-1 \mathrm{~V}$
- Input Offset Voltage ... $60 \mu \mathrm{~V}$
- Ultra-Small Packages
- 8 or 10 Pin MSOP (TLC080/1/2/3)


## Operational Amplifier



## description

The first members of TI's new BiMOS general-purpose operational amplifier family are the TLC08x. The BiMOS family concept is simple: provide an upgrade path for BiFET users who are moving away from dual-supply to single-supply systems and demand higher ac and dc performance. With performance rated from 4.5 V to 16 V across commercial $\left(0^{\circ} \mathrm{C}\right.$ to $\left.70^{\circ} \mathrm{C}\right)$ and an extended industrial temperature range $\left(-40^{\circ} \mathrm{C}\right.$ to $\left.125^{\circ} \mathrm{C}\right)$, BiMOS suits a wide range of audio, automotive, industrial, and instrumentation applications. Familiar features like offset nulling pins, and new features like MSOP PowerPADTM packages and shutdown modes, enable higher levels of performance in a variety of applications.
Developed in Tl's patented LBC3 BiCMOS process, the new BiMOS amplifiers combine a very high input impedance, low-noise CMOS front end with a high-drive bipolar output stage, thus providing the optimum performance features of both. AC performance improvements over the TL08x BiFET predecessors include a bandwidth of 10 MHz (an increase of $300 \%$ ) and voltage noise of $8.5 \mathrm{nV} / \sqrt{\mathrm{Hz}}$ (an improvement of $60 \%$ ). DC improvements include an ensured $\mathrm{V}_{I C R}$ that includes ground, a factor of 4 reduction in input offset voltage down to 1.5 mV (maximum) in the standard grade, and a power supply rejection improvement of greater than 40 dB to 130 dB . Added to this list of impressive features is the ability to drive $\pm 50-\mathrm{mA}$ loads comfortably from an ultrasmall-footprint MSOP PowerPAD package, which positions the TLC08x as the ideal high-performance general-purpose operational amplifier family.

FAMILY PACKAGE TABLE

| DEVICE | NO. OF CHANNELS | PACKAGE TYPES |  |  |  | SHUTDOWN | UNIVERSAL EVM BOARD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MSOP | PDIP | SOIC | TSSOP |  |  |
| TLC080 | 1 | 8 | 8 | 8 | - | Yes | Refer to the EVM Selection Guide (Lit\# SLOU060) |
| TLC081 | 1 | 8 | 8 | 8 | - |  |  |
| TLC082 | 2 | 8 | 8 | 8 | - | - |  |
| TLC083 | 2 | 10 | 14 | 14 | - | Yes |  |
| TLC084 | 4 | - | 14 | 14 | 20 | - |  |
| TLC085 | 4 | - | 16 | 16 | 20 | Yes |  |

TLC080 and TLC081 AVAILABLE OPTIONS

| $\mathrm{T}_{\mathbf{A}}$ | PACKAGED DEVICES |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | SMALL OUTLINE <br> (D) ${ }^{\dagger}$ | SMALL OUTLINE (DGN) $\dagger$ | SYMBOL | PLASTIC DIP <br> ( P ) |
| $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | $\begin{aligned} & \hline \text { TLC080CD } \\ & \text { TLC081CD } \end{aligned}$ | TLC080CDGN TLC081CDGN | xxTIACW <br> xxTIACY | $\begin{aligned} & \hline \text { TLC080CP } \\ & \text { TLC081CP } \end{aligned}$ |
| $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | $\begin{aligned} & \hline \text { TLC080ID } \\ & \text { TLC081ID } \end{aligned}$ | TLC080IDGN TLC081IDGN | $\begin{aligned} & \hline x x \operatorname{TIACX} \\ & \text { xxTIACZ } \end{aligned}$ | TLC080IP TLC081IP |
|  | $\begin{aligned} & \hline \text { TLC080AID } \\ & \text { TLC081AID } \end{aligned}$ | - | - | TLC080AIP TLC081AIP |

† This package is available taped and reeled. To order this packaging option, add an R suffix to the part number (e.g., TLC080CDR).
TLC082 and TLC083 AVAILABLE OPTIONS

| $\mathrm{T}_{\text {A }}$ | PACKAGED DEVICES |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SMALL OUTLINE (D) $\dagger$ | MSOP |  |  |  | PLASTIC DIP (N) | PLASTIC (P) |
|  |  | (DGN) $\dagger$ | SYMBOL $\ddagger$ | (DGQ) $\dagger$ | SYMBOLキ |  |  |
| $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | $\begin{aligned} & \hline \text { TLC082CD } \\ & \text { TLC083CD } \end{aligned}$ | TLC082CDGN | xxTIADZ | $\begin{gathered} - \\ \text { TLC083CDGQ } \end{gathered}$ | xxTIAEB | TLC083CN | TLC082CP |
| $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | TLC082ID TLC083ID | TLC082IDGN | xxTIAEA | $\overline{-}$ | xxTIAEC | $\overline{-}$ | TLC082IP |
|  | $\begin{aligned} & \hline \text { TLC082AID } \\ & \text { TLC083AID } \end{aligned}$ | - | - | - | - | TLC083AIN | TLC082AIP |

$\dagger$ This package is available taped and reeled. To order this packaging option, add an $R$ suffix to the part number (e.g., TLC082CDR).
$\ddagger x x$ represents the device date code.
TLC084 and TLC085 AVAILABLE OPTIONS

| $\mathbf{T}_{\mathbf{A}}$ | PACKAGED DEVICES |  |  |
| :---: | :---: | :---: | :---: |
|  | SMALL OUTLINE <br> (D) $\dagger$ | PLASTIC DIP <br> (N) | TSSOP <br> (PWP) $\dagger$ |
| $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ | TLC084CD | TLC084CN | TLC084CPWP |
|  | TLC085CD | TLC085CN | TLC085CPWP |
| $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | TLC084ID | TLC084IN | TLC084IPWP |
|  | TLC085ID | TLC085IN | TLC085IPWP |
|  | TLC084AID | TLC084AIN | TLC084AIPWP |
|  | TLC085AID | TLC085AIN | TLC085AIPWP |

$\dagger$ This package is available taped and reeled. To order this packaging option, add an $R$ suffix to the part number (e.g., TLC084CDR).

## TLC08x PACKAGE PINOUTS

TLC080
D, DGN, OR P PACKAGE
(TOP VIEW)


TLC083
DGQ PACKAGE
(TOP VIEW)


PWP PACKAGE
(TOP VIEW)


TLC081
D, DGN, OR P PACKAGE
(TOP VIEW)


TLC083
D OR N PACKAGE
(TOP VIEW)


TLC085
D OR N PACKAGE
(TOP VIEW)


NC - No internal connection

## TLC080, TLC081, TLC082, TLC083, TLC084, TLC085, TLC08xA

 FAMILY OF WIDE-BANDWIDTH HIGH-OUTPUT-DRIVE SINGLE SUPPLY OPERATIONAL AMPLIFIERSSLOS254C - JUNE 1999 - REVISED NOVEMBER 2000

## absolute maximum ratings over operating free-air temperature range (unless otherwise noted) $\dagger$

| Supply voltage, V ${ }_{\text {DD }}$ (see Note 1) |  | 17 V |
| :---: | :---: | :---: |
| Differential input voltage range, $\mathrm{V}_{\mathrm{ID}}$ |  | $\pm \mathrm{V}_{\mathrm{DD}}$ |
| Continuous total power dissipation |  | See Dissipation Rating Table |
| Operating free-air temperature range, $\mathrm{T}_{\mathrm{A}}$ : | C suffix I suffix | $\ldots 0^{\circ} \mathrm{C} \text { to } 70^{\circ} \mathrm{C}$ $-40^{\circ} \mathrm{C} \text { to } 125^{\circ} \mathrm{C}$ |
| Maximum junction temperature, $\mathrm{T}_{\mathrm{J}}$ |  | $150^{\circ} \mathrm{C}$ |
| Storage temperature range, $\mathrm{T}_{\text {stg }}$ |  | $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ |
| Lead temperature $1,6 \mathrm{~mm}$ (1) | case for 10 seconds | $260^{\circ} \mathrm{C}$ |

$\dagger$ Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
NOTE 1: All voltage values, except differential voltages, are with respect to GND.

DISSIPATION RATING TABLE

| PACKAGE | $\theta \mathbf{J C}$ <br> $\left({ }^{\circ} \mathbf{C} / \mathbf{W}\right)$ | $\theta \mathbf{J A}$ <br> $\left({ }^{\circ} \mathbf{C} / \mathbf{W}\right)$ | $\mathbf{T} \mathbf{A} \leq \mathbf{2 5}{ }^{\circ} \mathbf{C}$ <br> POWER RATING |
| :---: | :---: | :---: | :---: |
| $\mathrm{D}(8)$ | 38.3 | 176 | 710 mW |
| $\mathrm{D}(14)$ | 26.9 | 122.3 | 1022 mW |
| $\mathrm{D}(16)$ | 25.7 | 114.7 | 1090 mW |
| $\mathrm{DGN}(8)$ | 4.7 | 52.7 | 2.37 W |
| $\mathrm{DGQ}(10)$ | 4.7 | 52.3 | 2.39 W |
| $\mathrm{~N}(14,16)$ | 32 | 78 | 1600 mW |
| $\mathrm{P}(8)$ | 41 | 104 | 1200 mW |
| PWP $(20)$ | 1.40 | 26.1 | 4.79 W |

recommended operating conditions

|  |  | MIN | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: |
|  | Single supply | 4.5 | 16 |  |
| Supply volage, VDD | Split supply | $\pm 2.25$ | $\pm 8$ |  |
| Common-mode input voltage, VICR |  | GND | $\mathrm{V}_{\mathrm{DD}}{ }^{-1}$ | V |
| down on/off voltage level $\ddagger$ | $\mathrm{V}_{\mathrm{IH}}$ | 2 |  | V |
|  | $\mathrm{V}_{\text {IL }}$ |  | 0.8 |  |
| perating free-air temperature, $\mathrm{T}_{\text {A }}$ | C-suffix | 0 | 70 | ${ }^{\circ} \mathrm{C}$ |
| Serating free-air temperature, $\mathrm{T}_{\text {A }}$ | I-suffix | -40 | 125 | C |

$\ddagger$ Relative to the voltage on the GND terminal of the device.

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electrical characteristics at specified free-air temperature, $\mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}$ (unless otherwise noted)

|  | PARAMETER | TEST CONDITIONS |  | $\mathrm{T}_{\mathrm{A}}{ }^{\dagger}$ | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VIO | Input offset voltage | $\begin{aligned} & \mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}, \\ & \mathrm{~V}_{\mathrm{IC}}=2.5 \mathrm{~V}, \\ & \mathrm{~V}_{\mathrm{O}}=2.5 \mathrm{~V}, \\ & \mathrm{RS}_{\mathrm{S}}=50 \Omega \end{aligned}$ | TLC080/1/2/3 | $25^{\circ} \mathrm{C}$ |  | 60 | 1000 | $\mu \mathrm{V}$ |
|  |  |  |  | Full range |  |  | 1500 |  |
|  |  |  | TLC080/1/2/3A | $25^{\circ} \mathrm{C}$ |  | 20 | 750 |  |
|  |  |  |  | Full range |  |  | 1000 |  |
|  |  |  | TLC084/5 | $25^{\circ} \mathrm{C}$ |  | 390 | 1900 |  |
|  |  |  |  | Full range |  |  | 3000 |  |
|  |  |  | TLC084/5A | $25^{\circ} \mathrm{C}$ |  | 390 | 1400 |  |
|  |  |  |  | Full range |  |  | 2000 |  |
| $\alpha \mathrm{VIO}$ | Temperature coefficient of input offset voltage |  |  |  |  | 1.2 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| ${ }^{1} \mathrm{O}$ | Input offset current | $\begin{aligned} & \mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}, \\ & \mathrm{~V}_{\mathrm{IC}}=2.5 \mathrm{~V}, \\ & \mathrm{~V}_{\mathrm{O}}=2.5 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{S}}=50 \Omega \end{aligned}$ |  | $25^{\circ} \mathrm{C}$ |  | 1.9 | 50 | pA |
|  |  |  | TLC08XC | Full range |  |  | 100 |  |
|  |  |  | TLC08XI |  |  |  | 700 |  |
| ${ }^{\text {IIB }}$ | Input bias current |  |  | $25^{\circ} \mathrm{C}$ |  | 3 | 50 | pA |
|  |  |  | TLC08XC | Full range |  |  | 100 |  |
|  |  |  | TLC08XI |  |  |  | 700 |  |
| VICR | Common-mode input voltage | CMRR > 70 dB , | $\mathrm{R}_{\mathrm{S}}=50 \Omega$ | $25^{\circ} \mathrm{C}$ | $\begin{array}{r} 0 \\ \text { to } \\ 3.5 \end{array}$ |  |  | V |
|  |  | CMRR > 52 dB , | $R_{S}=50 \Omega$ | Full range | $\begin{array}{r} 0 \\ \text { to } \\ 3.5 \end{array}$ |  |  |  |
| VOH | High-level output voltage | $\mathrm{V}_{\text {IC }}=2.5 \mathrm{~V}$ | $\mathrm{IOH}=-1 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ | 4.1 | 4.3 |  | V |
|  |  |  |  | Full range | 3.9 |  |  |  |
|  |  |  | $\mathrm{IOH}=-20 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ | 3.7 | 4 |  |  |
|  |  |  |  | Full range | 3.5 |  |  |  |
|  |  |  | $\mathrm{IOH}=-35 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ | 3.4 | 3.8 |  |  |
|  |  |  |  | Full range | 3.2 |  |  |  |
|  |  |  | $\mathrm{I} \mathrm{OH}=-50 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ | 3.2 | 3.6 |  |  |
|  |  |  |  | $\begin{array}{\|c\|} \hline-40^{\circ} \mathrm{C} \text { to } \\ 85^{\circ} \mathrm{C} \\ \hline \end{array}$ | 3 |  |  |  |
| VOL | Low-level output voltage | $\mathrm{V}_{\text {IC }}=2.5 \mathrm{~V}$ | $\mathrm{I} \mathrm{OL}=1 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ |  | 0.18 | 0.25 | V |
|  |  |  |  | Full range |  |  | 0.35 |  |
|  |  |  | $\mathrm{IOL}=20 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ |  | 0.35 | 0.39 |  |
|  |  |  |  | Full range |  |  | 0.45 |  |
|  |  |  | $\mathrm{IOL}=35 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ |  | 0.43 | 0.55 |  |
|  |  |  |  | Full range |  |  | 0.7 |  |
|  |  |  | ${ }^{\mathrm{I}} \mathrm{OL}=50 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ |  | 0.45 | 0.63 |  |
|  |  |  |  | $\begin{array}{\|c\|} \hline-40^{\circ} \mathrm{C} \text { to } \\ 85^{\circ} \mathrm{C} \end{array}$ |  |  | 0.7 |  |
| Ios | Short-circuit output current | Sourcing |  | $25^{\circ} \mathrm{C}$ |  | 100 |  | mA |
|  |  | Sinking |  | $25^{\circ} \mathrm{C}$ |  | 100 |  |  |
| Io | Output current | $\mathrm{V}_{\mathrm{OH}}=1.5 \mathrm{~V}$ from positive rail |  | $25^{\circ} \mathrm{C}$ |  | 57 |  | mA |
|  |  | $\mathrm{V}_{\mathrm{OL}}=0.5 \mathrm{~V}$ from | tive rail | $25^{\circ} \mathrm{C}$ |  | 55 |  |  |

$\dagger$ Full range is $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ for C suffix and $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ for I suffix. If not specified, full range is $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$.

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electrical characteristics at specified free-air temperature, $\mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}$ (unless otherwise noted) (continued)

|  | PARAMETER | TEST CONDITIONS |  | $\mathrm{T}_{\mathbf{A}}{ }^{\dagger}$ | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AVD | Large-signal differential voltage amplification | $\mathrm{V}_{\mathrm{O}}(\mathrm{PP})=3 \mathrm{~V}$, | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | $25^{\circ} \mathrm{C}$ | 100 | 120 |  | dB |
|  |  |  |  | Full range | 100 |  |  |  |
| $\mathrm{ri}_{\text {( }}(\mathrm{d})$ | Differential input resistance |  |  | $25^{\circ} \mathrm{C}$ |  | 1000 |  | $\mathrm{G} \Omega$ |
| CIC | Common-mode input capacitance | $\mathrm{f}=10 \mathrm{kHz}$ |  | $25^{\circ} \mathrm{C}$ |  | 22.9 |  | pF |
| $\mathrm{z}_{0}$ | Closed-loop output impedance | $\mathrm{f}=10 \mathrm{kHz}$, | $A_{V}=10$ | $25^{\circ} \mathrm{C}$ |  | 0.25 |  | $\Omega$ |
| CMRR | Common-mode rejection ratio | VIC $=0$ to 3 V , | $\mathrm{R}_{S}=50 \Omega$ | $25^{\circ} \mathrm{C}$ | 100 | 140 |  | dB |
|  |  |  |  | Full range | 100 |  |  |  |
| kSVR | Supply voltage rejection ratio ( $\Delta \mathrm{V}_{\mathrm{DD}} / \Delta \mathrm{V}_{\mathrm{IO}}$ ) | $V_{D D}=4.5 \mathrm{~V} \text { to } 16 \mathrm{~V},$ <br> No load | $\mathrm{V}_{\mathrm{IC}}=\mathrm{V}_{\mathrm{DD} / 2}$, | $25^{\circ} \mathrm{C}$ | 95 | 130 |  | dB |
|  |  |  |  | Full range | 95 |  |  |  |
|  | Supply current (per channel) | $\mathrm{V}_{\mathrm{O}}=2.5 \mathrm{~V}$, | No load | $25^{\circ} \mathrm{C}$ |  | 1.8 | 2.5 | mA |
|  |  |  |  | Full range |  |  | 3.5 |  |
| IDD(SHDN) | Supply current in shutdown mode (per channel) (TLC080, TLC083, TLC085) | $\overline{\mathrm{SHDN}} \leq 0.8 \mathrm{~V}$ |  | $25^{\circ} \mathrm{C}$ |  | 125 | 200 | $\mu \mathrm{A}$ |
|  |  |  |  | Full range |  |  | 250 |  |

$\dagger$ Full range is $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ for C suffix and $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ for I suffix. If not specified, full range is $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$.

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operating characteristics at specified free-air temperature, $\mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}$ (unless otherwise noted)

| PARAMETER |  | TEST CONDITIONS |  | TA ${ }^{\dagger}$ | MIN TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR+ | Positive slew rate at unity gain | $\begin{aligned} & \mathrm{V}_{\mathrm{O}}(\mathrm{PP})=0.8 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | $\mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}$, | $25^{\circ} \mathrm{C}$ | $10 \quad 16$ |  | V/us |
|  |  |  |  | Full range | 9.5 |  |  |
| SR- | Negative slew rate at unity gain | $\begin{aligned} & \mathrm{V}_{\mathrm{O}(\mathrm{PP})}=0.8 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | $C_{L}=50 \mathrm{pF}$, | $25^{\circ} \mathrm{C}$ | 12.519 |  | V/us |
|  |  |  |  | Full range | 10 |  |  |
| $\mathrm{V}_{\mathrm{n}}$ | Equivalent input noise voltage | $\mathrm{f}=100 \mathrm{~Hz}$ |  | $25^{\circ} \mathrm{C}$ | 12 |  | $\mathrm{nV} / \mathrm{NHz}$ |
|  |  | $\mathrm{f}=1 \mathrm{kHz}$ |  | $25^{\circ} \mathrm{C}$ | 8.5 |  |  |
| In | Equivalent input noise current | $\mathrm{f}=1 \mathrm{kHz}$ |  | $25^{\circ} \mathrm{C}$ | 0.6 |  | $\mathrm{fA} / \sqrt{\mathrm{Hz}}$ |
| THD + N | Total harmonic distortion plus noise | $\begin{aligned} & \mathrm{V}_{\mathrm{O}(\mathrm{PP})}=3 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \text { and } 250 \Omega, \\ & \mathrm{f}=1 \mathrm{kHz} \end{aligned}$ | $A_{V}=1$ | $25^{\circ} \mathrm{C}$ | 0.002\% |  |  |
|  |  |  | $A_{V}=10$ |  | 0.012\% |  |  |
|  |  |  | AV $=100$ |  | 0.085\% |  |  |
| t(on) | Amplifier turnon time $\ddagger$ | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ |  | $25^{\circ} \mathrm{C}$ | 0.15 |  | $\mu \mathrm{s}$ |
| t(off) | Amplifier turnoff time $\ddagger$ |  |  | $25^{\circ} \mathrm{C}$ | 1.3 |  | $\mu \mathrm{s}$ |
|  | Gain-bandwidth product | $\mathrm{f}=10 \mathrm{kHz}$, | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | $25^{\circ} \mathrm{C}$ | 10 |  | MHz |
| $\mathrm{t}_{\mathrm{s}}$ | Settling time | $\begin{aligned} & \mathrm{V}_{(\mathrm{STEP}} \mathrm{PP}=1 \mathrm{~V}, \\ & \mathrm{AV}=-1, \\ & C_{L}=10 \mathrm{pF}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | 0.1\% | $25^{\circ} \mathrm{C}$ | 0.18 |  | $\mu \mathrm{s}$ |
|  |  |  | 0.01\% |  | 0.39 |  |  |
|  |  | $\begin{aligned} & \mathrm{V}_{(\mathrm{STEP}) \mathrm{PP}}=1 \mathrm{~V}, \\ & \mathrm{~A}_{\mathrm{V}}=-1, \\ & \mathrm{C}_{\mathrm{L}}=47 \mathrm{pF}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | 0.1\% |  | 0.18 |  |  |
|  |  |  | 0.01\% |  | 0.39 |  |  |
| $\phi_{\mathrm{m}}$ | Phase margin | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, | $\mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}$ | $25^{\circ} \mathrm{C}$ | $32^{\circ}$ |  |  |
|  |  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, | $\mathrm{C}_{\mathrm{L}}=0 \mathrm{pF}$ |  | $40^{\circ}$ |  |  |
| Gain margin |  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, | $\mathrm{CLL}_{\text {= }} 50 \mathrm{pF}$ | $25^{\circ} \mathrm{C}$ | 2.2 |  | dB |
|  |  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, | $\mathrm{C}_{\mathrm{L}}=0 \mathrm{pF}$ |  | 3.3 |  |  |

$\dagger$ Full range is $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ for C suffix and $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ for I suffix. If not specified, full range is $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$.
$\ddagger$ Disable time and enable time are defined as the interval between application of the logic signal to SHDN and the point at which the supply current has reached half its final value.

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electrical characteristics at specified free-air temperature, $\mathrm{V}_{\mathrm{DD}}=12 \mathrm{~V}$ (unless otherwise noted)

|  | PARAMETER | TEST CONDITIONS |  | $\mathrm{T}_{\mathbf{A}}{ }^{\text {¢ }}$ | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{10}$ | Input offset voltage | $\begin{aligned} & \mathrm{V}_{\mathrm{DD}}=12 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{IC}}=6 \mathrm{~V}, \\ & \mathrm{~V}_{\mathrm{O}}=6 \mathrm{~V}, \\ & \mathrm{RS}_{\mathrm{S}}=50 \Omega \end{aligned}$ | TLC080/1/2/3 | $25^{\circ} \mathrm{C}$ |  | 60 | 1000 | $\mu \mathrm{V}$ |
|  |  |  |  | Full range |  |  | 1500 |  |
|  |  |  | TLC080/1/2/3A | $25^{\circ} \mathrm{C}$ |  | 20 | 750 |  |
|  |  |  |  | Full range |  |  | 1000 |  |
|  |  |  | TLC084/5 | $25^{\circ} \mathrm{C}$ |  | 390 | 1900 |  |
|  |  |  |  | Full range |  |  | 3000 |  |
|  |  |  | TLC084/5A | $25^{\circ} \mathrm{C}$ |  | 390 | 1400 |  |
|  |  |  |  | Full range |  |  | 2000 |  |
| $\alpha \mathrm{VIO}$ | Temperature coefficient of input offset voltage |  |  |  |  | 1.2 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| IIO | Input offset current | $\begin{aligned} & \mathrm{V}_{\mathrm{DD}}=12 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{IC}}=6 \mathrm{~V}, \\ & \mathrm{~V}_{\mathrm{O}}=6 \mathrm{~V}, \\ & \mathrm{RS}_{\mathrm{S}}=50 \Omega \end{aligned}$ |  | $25^{\circ} \mathrm{C}$ |  | 1.5 | 50 | pA |
|  |  |  | TLC08xC | Full range |  |  | 100 |  |
|  |  |  | TLC08x |  |  |  | 700 |  |
| ${ }^{\text {IIB }}$ | Input bias current |  |  | $25^{\circ} \mathrm{C}$ |  | 2 | 50 | pA |
|  |  |  | TLC08xC | Full range |  |  | 100 |  |
|  |  |  | TLC08x |  |  |  | 700 |  |
| VICR | Common-mode input voltage | CMRR > 70 dB , | $\mathrm{R}_{S}=50 \Omega$ | $25^{\circ} \mathrm{C}$ | $\begin{array}{r} 0 \\ \text { to } \\ 10.5 \\ \hline \end{array}$ |  |  | V |
|  |  | CMRR > 52 dB , | $\mathrm{R}_{\mathrm{S}}=50 \Omega$ | Full range | $\begin{array}{r} 0 \\ \text { to } \\ 10.5 \end{array}$ |  |  |  |
| VOH | High-level output voltage | $\mathrm{V}_{\text {IC }}=6 \mathrm{~V}$ | $\mathrm{IOH}=-1 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ | 11.1 | 11.2 |  | V |
|  |  |  |  | Full range | 11 |  |  |  |
|  |  |  | $\mathrm{I} \mathrm{OH}=-20 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ | 10.8 | 11 |  |  |
|  |  |  |  | Full range | 10.7 |  |  |  |
|  |  |  | $\mathrm{I} \mathrm{OH}=-35 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ | 10.6 | 10.7 |  |  |
|  |  |  |  | Full range | 10.3 |  |  |  |
|  |  |  | $\mathrm{IOH}=-50 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ | 10.3 | 10.5 |  |  |
|  |  |  |  | $\begin{array}{\|c\|} \hline-40^{\circ} \mathrm{C} \text { to } \\ 85^{\circ} \mathrm{C} \end{array}$ | 10.2 |  |  |  |
| VOL | Low-level output voltage | V IC $=6 \mathrm{~V}$ | $\mathrm{IOL}=1 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ |  | 0.17 | 0.25 | V |
|  |  |  |  | Full range |  |  | 0.35 |  |
|  |  |  | $\mathrm{lOL}=20 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ |  | 0.35 | 0.45 |  |
|  |  |  |  | Full range |  |  | 0.5 |  |
|  |  |  | $\mathrm{l} \mathrm{OL}=35 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ |  | 0.4 | 0.52 |  |
|  |  |  |  | Full range |  |  | 0.6 |  |
|  |  |  | $\mathrm{IOL}=50 \mathrm{~mA}$ | $25^{\circ} \mathrm{C}$ |  | 0.45 | 0.6 |  |
|  |  |  |  | $\begin{array}{\|c\|} \hline-40^{\circ} \mathrm{C} \text { to } \\ 85^{\circ} \mathrm{C} \\ \hline \end{array}$ |  |  | 0.65 |  |
| los | Short-circuit output current | Sourcing |  | $25^{\circ} \mathrm{C}$ |  | 150 |  | mA |
|  |  | Sinking |  | $25^{\circ} \mathrm{C}$ |  | 150 |  |  |
| Io | Output current | $\mathrm{V}_{\mathrm{OH}}=1.5 \mathrm{~V}$ from positive rail |  | $25^{\circ} \mathrm{C}$ |  | 57 |  | mA |
|  |  | $\mathrm{V}_{\mathrm{OL}}=0.5 \mathrm{~V}$ from negative rail |  | $25^{\circ} \mathrm{C}$ |  | 55 |  |  |

[^0]
# TLC080, TLC081, TLC082, TLC083, TLC084, TLC085, TLC08xA FAMILY OF WIDE-BANDWIDTH HIGH-OUTPUT-DRIVE SINGLE SUPPLY OPERATIONAL AMPLIFIERS 

electrical characteristics at specified free-air temperature, $\mathrm{V}_{\mathrm{DD}}=12 \mathrm{~V}$ (unless otherwise noted) (continued)

|  | PARAMETER | TEST CONDITIONS |  | $\mathrm{T}_{\mathbf{A}}{ }^{\dagger}$ | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AVD | Large-signal differential voltage amplification | $\mathrm{V}_{\mathrm{O}}(\mathrm{PP})=8 \mathrm{~V}$, | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | $25^{\circ} \mathrm{C}$ | 120 | 140 |  | dB |
|  |  |  |  | Full range | 120 |  |  |  |
| ri(d) | Differential input resistance |  |  | $25^{\circ} \mathrm{C}$ |  | 1000 |  | G $\Omega$ |
| CIC | Common-mode input capacitance | $\mathrm{f}=10 \mathrm{kHz}$ |  | $25^{\circ} \mathrm{C}$ |  | 21.6 |  | pF |
| $\mathrm{z}_{0}$ | Closed-loop output impedance | $\mathrm{f}=10 \mathrm{kHz}$, | $A_{V}=10$ | $25^{\circ} \mathrm{C}$ |  | 0.25 |  | $\Omega$ |
| CMRR | Common-mode rejection ratio | V IC $=0$ to 10 V , | $\mathrm{RS}=50 \Omega$ | $25^{\circ} \mathrm{C}$ | 100 | 140 |  | dB |
|  |  |  |  | Full range | 100 |  |  |  |
| kSVR | Supply voltage rejection ratio $\left(\Delta V_{D D} / \Delta V_{I O}\right)$ | $\mathrm{V}_{\mathrm{DD}}=4.5 \mathrm{~V} \text { to } 16 \mathrm{~V} \text {, }$ <br> No load | $\mathrm{V}_{\mathrm{IC}}=\mathrm{V}_{\mathrm{DD}} / 2$, | $25^{\circ} \mathrm{C}$ | 95 | 130 |  | dB |
|  |  |  |  | Full range | 95 |  |  |  |
|  | Supply current (per channel) | $\mathrm{V}_{\mathrm{O}}=7.5 \mathrm{~V}$, | No load | $25^{\circ} \mathrm{C}$ |  | 1.9 | 2.9 | mA |
|  |  |  |  | Full range |  |  | 3.5 |  |
| IDD(SHDN) | Supply current in shutdown mode (TLC080, TLC083, TLC085) (per channel) | $\overline{\mathrm{SHDN}} \leq 0.8 \mathrm{~V}$ |  | $25^{\circ} \mathrm{C}$ |  | 125 | 200 | $\mu \mathrm{A}$ |
|  |  |  |  | Full range |  |  | 250 |  |

$\dagger$ Full range is $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ for C suffix and $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ for I suffix. If not specified, full range is $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$.

## TLC080, TLC081, TLC082, TLC083, TLC084, TLC085, TLC08xA FAMILY OF WIDE-BANDWIDTH HIGH-OUTPUT-DRIVE SINGLE SUPPLY OPERATIONAL AMPLIFIERS <br> SLOS254C - JUNE 1999 - REVISED NOVEMBER 2000

operating characteristics at specified free-air temperature, $\mathrm{V}_{\mathrm{DD}}=12 \mathrm{~V}$ (unless otherwise noted)

| PARAMETER |  | TEST CONDITIONS |  | $\mathrm{T}_{\mathbf{A}}{ }^{\text {¢ }}$ | MIN TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR+ | Positive slew rate at unity gain | $\begin{aligned} & \mathrm{V}_{\mathrm{O}(\mathrm{PP})}=2 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | $C_{L}=50 \mathrm{pF}$, | $25^{\circ} \mathrm{C}$ | $10 \quad 16$ |  | V/us |
|  |  |  |  | Full range | 9.5 |  |  |
| SR- | Negative slew rate at unity gain | $\begin{aligned} & \mathrm{V}_{\mathrm{O}(\mathrm{PP})}=2 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | $C_{L}=50 \mathrm{pF}$, | $25^{\circ} \mathrm{C}$ | 12.519 |  | V/us |
|  |  |  |  | Full range | 10 |  |  |
| $V_{n}$ | Equivalent input noise voltage | $\mathrm{f}=100 \mathrm{~Hz}$ |  | $25^{\circ} \mathrm{C}$ | 14 |  | $\mathrm{nV} / \mathrm{VHz}$ |
|  |  | $\mathrm{f}=1 \mathrm{kHz}$ |  | $25^{\circ} \mathrm{C}$ | 8.5 |  |  |
| $\mathrm{I}_{\mathrm{n}}$ | Equivalent input noise current | $\mathrm{f}=1 \mathrm{kHz}$ |  | $25^{\circ} \mathrm{C}$ | 0.6 |  | $\mathrm{fA} / \sqrt{\mathrm{Hz}}$ |
| THD + N | Total harmonic distortion plus noise | $\begin{aligned} & V_{O(P P)}=8 \mathrm{~V}, \\ & R_{L}=10 \mathrm{k} \Omega \text { and } 250 \Omega, \\ & \mathrm{f}=1 \mathrm{kHz} \end{aligned}$ | $A_{V}=1$ | $25^{\circ} \mathrm{C}$ | 0.002\% |  |  |
|  |  |  | $A_{V} \mathrm{~V}=10$ |  | 0.005\% |  |  |
|  |  |  | $A_{V}=100$ |  | 0.022\% |  |  |
| t(on) | Amplifier turnon time $\ddagger$ | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ |  | $25^{\circ} \mathrm{C}$ | 0.47 |  | $\mu \mathrm{s}$ |
| t(off) | Amplifier turnoff time $\ddagger$ |  |  | $25^{\circ} \mathrm{C}$ | 2.5 |  | $\mu \mathrm{s}$ |
|  | Gain-bandwidth product | $\mathrm{f}=10 \mathrm{kHz}$, | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | $25^{\circ} \mathrm{C}$ | 10 |  | MHz |
| $t_{s}$ | Settling time | $\begin{aligned} & \mathrm{V}_{(\mathrm{STEP}} \mathrm{PP}=1 \mathrm{~V}, \\ & \mathrm{~A}_{\mathrm{V}}=-1, \\ & C_{\mathrm{L}}=10 \mathrm{pF}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | 0.1\% | $25^{\circ} \mathrm{C}$ | 0.17 |  | $\mu \mathrm{s}$ |
|  |  |  | 0.01\% |  | 0.22 |  |  |
|  |  | $\begin{aligned} & \mathrm{V}_{(\mathrm{STEP}} \mathrm{PP}=1 \mathrm{~V}, \\ & \mathrm{AV}=-1, \\ & C_{\mathrm{L}}=47 \mathrm{pF}, \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | 0.1\% |  | 0.17 |  |  |
|  |  |  | 0.01\% |  | 0.29 |  |  |
| $\phi_{\text {m }}$ | Phase margin | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, | $\mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}$ | $25^{\circ} \mathrm{C}$ | $37^{\circ}$ |  |  |
|  |  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, | $\mathrm{C}_{\mathrm{L}}=0 \mathrm{pF}$ |  | $42^{\circ}$ |  |  |
|  | Gain margin | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, | $\mathrm{CL}_{\mathrm{L}}=50 \mathrm{pF}$ | $25^{\circ} \mathrm{C}$ | 3.1 |  | dB |
|  |  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$, | $\mathrm{C}_{\mathrm{L}}=0 \mathrm{pF}$ |  | 4 |  |  |

$\dagger$ Full range is $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ for C suffix and $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ for I suffix. If not specified, full range is $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$.
$\ddagger$ Disable time and enable time are defined as the interval between application of the logic signal to SHDN and the point at which the supply current has reached half its final value.

## TLC080, TLC081, TLC082, TLC083, TLC084, TLC085, TLC08xA FAMILY OF WIDE-BANDWIDTH HIGH-OUTPUT-DRIVE SINGLE SUPPLY OPERATIONAL AMPLIFIERS

TYPICAL CHARACTERISTICS

Table of Graphs

|  |  |  | FIGURE |
| :---: | :---: | :---: | :---: |
| $\mathrm{V}_{1 \mathrm{O}}$ | Input offset voltage | vs Common-mode input voltage | 1, 2 |
| IIO | Input offset current | vs Free-air temperature | 3, 4 |
| IIB | Input bias current | vs Free-air temperature | 3, 4 |
| $\mathrm{V}_{\mathrm{OH}}$ | High-level output voltage | vs High-level output current | 5, 7 |
| $\mathrm{V}_{\mathrm{OL}}$ | Low-level output voltage | vs Low-level output current | 6, 8 |
| $\mathrm{Z}_{0}$ | Output impedance | vs Frequency | 9 |
| IDD | Supply current | vs Supply voltage | 10 |
| PSRR | Power supply rejection ratio | vs Frequency | 11 |
| CMRR | Common-mode rejection ratio | vs Frequency | 12 |
| $\mathrm{V}_{\mathrm{n}}$ | Equivalent input noise voltage | vs Frequency | 13 |
| $\mathrm{V}_{\mathrm{O} \text { (PP) }}$ | Peak-to-peak output voltage | vs Frequency | 14, 15 |
|  | Crosstalk | vs Frequency | 16 |
|  | Differential voltage gain | vs Frequency | 17, 18 |
|  | Phase | vs Frequency | 17, 18 |
| $\phi \mathrm{m}$ | Phase margin | vs Load capacitance | 19, 20 |
|  | Gain margin | vs Load capacitance | 21, 22 |
|  | Gain-bandwidth product | vs Supply voltage | 23 |
| SR | Slew rate | vs Supply voltage vs Free-air temperature | $\begin{gathered} 24 \\ 25,26 \end{gathered}$ |
|  |  | vs Frequency | 27, 28 |
| THD + N | Total harmonic distortion plus noise | vs Peak-to-peak output voltage | 29, 30 |
|  | Large-signal follower pulse response |  | 31, 32 |
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## TYPICAL CHARACTERISTICS



Figure 1
INPUT BIAS CURRENT AND INPUT OFFSET CURRENT
vs


Figure 4

HIGH-LEVEL OUTPUT VOLTAGE
vs
HIGH-LEVEL OUTPUT CURRENT



Figure 2

HIGH-LEVEL OUTPUT VOLTAGE
HIGH-LEVEL OUTPUT CURRENT


Figure 5

LOW-LEVEL OUTPUT VOLTAGE vs
LOW-LEVEL OUTPUT CURRENT


INPUT BIAS CURRENT AND INPUT OFFSET CURRENT
vs


Figure 3

LOW-LEVEL OUTPUT VOLTAGE
vs
LOW-LEVEL OUTPUT CURRENT


Figure 6

OUTPUT IMPEDANCE
vs
FREQUENCY


Figure 9

## TYPICAL CHARACTERISTICS



## TYPICAL CHARACTERISTICS




Figure 19


Figure 22


Figure 20

GAIN BANDWIDTH PRODUCT
vs
SUPPLY VOLTAGE


Figure 23

GAIN MARGIN
vs
LOAD CAPACITANCE


Figure 21

SLEW RATE
vs
SUPPLY VOLTAGE


Figure 24

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## TYPICAL CHARACTERISTICS




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## TYPICAL CHARACTERISTICS



Figure 43


Figure 44

PARAMETER MEASUREMENT INFORMATION


Figure 45

## APPLICATION INFORMATION

input offset voltage null circuit
The TLC080 and TLC081 has an input offset nulling function. Refer to Figure 46 for the diagram.


NOTE A: R1 $=5.6 \mathrm{k} \Omega$ for offset voltage adjustment of $\pm 10 \mathrm{mV}$.
R1 $=20 \mathrm{k} \Omega$ for offset voltage adjustment of $\pm 3 \mathrm{mV}$.
Figure 46. Input Offset Voltage Null Circuit

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## APPLICATION INFORMATION

## driving a capacitive load

When the amplifier is configured in this manner, capacitive loading directly on the output will decrease the device's phase margin leading to high frequency ringing or oscillations. Therefore, for capacitive loads of greater than 10 pF , it is recommended that a resistor be placed in series ( $\mathrm{R}_{\text {NULL }}$ ) with the output of the amplifier, as shown in Figure 47. A minimum value of $20 \Omega$ should work well for most applications.


Figure 47. Driving a Capacitive Load

## offset voltage

The output offset voltage, ( $\mathrm{V}_{\mathrm{OO}}$ ) is the sum of the input offset voltage $\left(\mathrm{V}_{\mathrm{IO}}\right)$ and both input bias currents $\left(\mathrm{I}_{\mathrm{IB}}\right)$ times the corresponding gains. The following schematic and formula can be used to calculate the output offset voltage:


Figure 48. Output Offset Voltage Model

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## APPLICATION INFORMATION

## high speed CMOS input amplifiers

The TLC08x is a family of high-speed low-noise CMOS input operational amplifiers that has an input capacitance of the order of 20 pF . Any resistor used in the feedback path adds a pole in the transfer function equivalent to the input capacitance multiplied by the combination of source resistance and feedback resistance. For example, a gain of -10 , a source resistance of $1 \mathrm{k} \Omega$, and a feedback resistance of $10 \mathrm{k} \Omega$ add an additional pole at approximately 8 MHz . This is more apparent with CMOS amplifiers than bipolar amplifiers due to their greater input capacitance.
This is of little consequence on slower CMOS amplifiers, as this pole normally occurs at frequencies above their unity-gain bandwidth. However, the TLC08x with its $10-\mathrm{MHz}$ bandwidth means that this pole normally occurs at frequencies where there is on the order of 5 dB gain left and the phase shift adds considerably.
The effect of this pole is the strongest with large feedback resistances at small closed loop gains. As the feedback resistance is increased, the gain peaking increases at a lower frequency and the $180^{\circ}$ phase shift crossover point also moves down in frequency, decreasing the phase margin.

For the TLC08x, the maximum feedback resistor recommended is $5 \mathrm{k} \Omega$; larger resistances can be used but a capacitor in parallel with the feedback resistor is recommended to counter the effects of the input capacitance pole.
The TLC083 with a 1-V step response has an $80 \%$ overshoot with a natural frequency of 3.5 MHz when configured as a unity gain buffer and with a $10-\mathrm{k} \Omega$ feedback resistor. By adding a $10-\mathrm{pF}$ capacitor in parallel with the feedback resistor, the overshoot is reduced to $40 \%$ and eliminates the natural frequency, resulting in a much faster settling time (see Figure 49). The 10-pF capacitor was chosen for convenience only.
Load capacitance had little effect on these measurements due to the excellent output drive capability of the TLC08x.


Figure 49. 1-V Step Response

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## APPLICATION INFORMATION

## general configurations

When receiving low-level signals, limiting the bandwidth of the incoming signals into the system is often required. The simplest way to accomplish this is to place an RC filter at the noninverting terminal of the amplifier (see Figure 50).


Figure 50. Single-Pole Low-Pass Filter
If even more attenuation is needed, a multiple pole filter is required. The Sallen-Key filter can be used for this task. For best results, the amplifier should have a bandwidth that is 8 to 10 times the filter frequency bandwidth. Failure to do this can result in phase shift of the amplifier.

$\mathbf{R 1}=\mathbf{R} \mathbf{2}=\mathbf{R}$
$\mathrm{C} 1=\mathrm{C} 2=\mathrm{C}$
Q = Peaking Factor
(Butterworth Q = 0.707)
${ }^{\mathrm{f}}-3 \mathrm{~dB}=\frac{1}{2 \pi \mathrm{RC}}$
$R_{G}=\frac{R_{F}}{\left(2-\frac{1}{Q}\right)}$

Figure 51. 2-Pole Low-Pass Sallen-Key Filter

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## APPLICATION INFORMATION

## shutdown function

Three members of the TLC08x family (TLC080/3/5) have a shutdown terminal ( $\overline{\mathrm{SHDN}}$ ) for conserving battery life in portable applications. When the shutdown terminal is tied low, the supply current is reduced to 125 $\mu \mathrm{A} /$ channel, the amplifier is disabled, and the outputs are placed in a high-impedance mode. To enable the amplifier, the shutdown terminal can either be left floating or pulled high. When the shutdown terminal is left floating, care should be taken to ensure that parasitic leakage current at the shutdown terminal does not inadvertently place the operational amplifier into shutdown. The shutdown terminal threshold is always referenced to the voltage on the GND terminal of the device. Therefore, when operating the device with split supply voltages (e.g. $\pm 2.5 \mathrm{~V}$ ), the shutdown terminal needs to be pulled to $\mathrm{V}_{\mathrm{DD}}$ ( (not system ground) to disable the operational amplifier.

The amplifier's output with a shutdown pulse is shown in Figures 43 and 44 . The amplifier is powered with a single $5-\mathrm{V}$ supply and is configured as noninverting with a gain of 5 . The amplifier turnon and turnoff times are measured from the $50 \%$ point of the shutdown pulse to the $50 \%$ point of the output waveform. The times for the single, dual, and quad are listed in the data tables.
Figures $37,38,39$, and 40 show the amplifier's forward and reverse isolation in shutdown. The operational amplifier is configured as a voltage follower $\left(A_{V}=1\right)$. The isolation performance is plotted across frequency using 0.1 $\mathrm{V}_{\mathrm{PP}, 2} 2.5 \mathrm{~V}_{\mathrm{PP}}$, and $5 \mathrm{~V}_{\mathrm{PP}}$ input signals at $\pm 2.5 \mathrm{~V}$ supplies and $0.1 \mathrm{~V}_{\mathrm{PP}}, 8 \mathrm{~V}_{\mathrm{PP}}$, and $12 \mathrm{~V}_{\mathrm{PP}}$ input signals at $\pm 6 \mathrm{~V}$ supplies.

## circuit layout considerations

To achieve the levels of high performance of the TLC08x, follow proper printed-circuit board design techniques. A general set of guidelines is given in the following.

- Ground planes - It is highly recommended that a ground plane be used on the board to provide all components with a low inductive ground connection. However, in the areas of the amplifier inputs and output, the ground plane can be removed to minimize the stray capacitance.
- Proper power supply decoupling - Use a $6.8-\mu \mathrm{F}$ tantalum capacitor in parallel with a $0.1-\mu \mathrm{F}$ ceramic capacitor on each supply terminal. It may be possible to share the tantalum among several amplifiers depending on the application, but a $0.1-\mu \mathrm{F}$ ceramic capacitor should always be used on the supply terminal of every amplifier. In addition, the $0.1-\mu \mathrm{F}$ capacitor should be placed as close as possible to the supply terminal. As this distance increases, the inductance in the connecting trace makes the capacitor less effective. The designer should strive for distances of less than 0.1 inches between the device power terminals and the ceramic capacitors.
- Sockets - Sockets can be used but are not recommended. The additional lead inductance in the socket pins will often lead to stability problems. Surface-mount packages soldered directly to the printed-circuit board is the best implementation.
- Short trace runs/compact part placements - Optimum high performance is achieved when stray series inductance has been minimized. To realize this, the circuit layout should be made as compact as possible, thereby minimizing the length of all trace runs. Particular attention should be paid to the inverting input of the amplifier. Its length should be kept as short as possible. This will help to minimize stray capacitance at the input of the amplifier.
- Surface-mount passive components - Using surface-mount passive components is recommended for high performance amplifier circuits for several reasons. First, because of the extremely low lead inductance of surface-mount components, the problem with stray series inductance is greatly reduced. Second, the small size of surface-mount components naturally leads to a more compact layout thereby minimizing both stray inductance and capacitance. If leaded components are used, it is recommended that the lead lengths be kept as short as possible.


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## APPLICATION INFORMATION

## general PowerPAD design considerations

The TLC08x is available in a thermally-enhanced PowerPAD family of packages. These packages are constructed using a downset leadframe upon which the die is mounted [see Figure 52(a) and Figure 52(b)]. This arrangement results in the lead frame being exposed as a thermal pad on the underside of the package [see Figure 52(c)]. Because this thermal pad has direct thermal contact with the die, excellent thermal performance can be achieved by providing a good thermal path away from the thermal pad.

The PowerPAD package allows for both assembly and thermal management in one manufacturing operation. During the surface-mount solder operation (when the leads are being soldered), the thermal pad can also be soldered to a copper area underneath the package. Through the use of thermal paths within this copper area, heat can be conducted away from the package into either a ground plane or other heat dissipating device.
The PowerPAD package represents a breakthrough in combining the small area and ease of assembly of surface mount with the, heretofore, awkward mechanical methods of heatsinking.


NOTE B: The thermal pad is electrically isolated from all terminals in the package.
Figure 52. Views of Thermally Enhanced DGN Package
Although there are many ways to properly heatsink the PowerPAD package, the following steps illustrate the recommended approach.

Thermal Pad Area


Figure 53. PowerPAD PCB Etch and Via Pattern

## APPLICATION INFORMATION

## general PowerPAD design considerations (continued)

1. Prepare the PCB with a top side etch pattern as shown in Figure 53. There should be etch for the leads as well as etch for the thermal pad.
2. Place five holes (dual) or nine holes (quad) in the area of the thermal pad. These holes should be 13 mils in diameter. Keep them small so that solder wicking through the holes is not a problem during reflow.
3. Additional vias may be placed anywhere along the thermal plane outside of the thermal pad area. This helps dissipate the heat generated by the TLC08x IC. These additional vias may be larger than the 13 -mil diameter vias directly under the thermal pad. They can be larger because they are not in the thermal pad area to be soldered so that wicking is not a problem.
4. Connect all holes to the internal ground plane.
5. When connecting these holes to the ground plane, do not use the typical web or spoke via connection methodology. Web connections have a high thermal resistance connection that is useful for slowing the heat transfer during soldering operations. This makes the soldering of vias that have plane connections easier. In this application, however, low thermal resistance is desired for the most efficient heat transfer. Therefore, the holes under the TLC08x PowerPAD package should make their connection to the internal ground plane with a complete connection around the entire circumference of the plated-through hole.
6. The top-side solder mask should leave the terminals of the package and the thermal pad area with its five holes (dual) or nine holes (quad) exposed. The bottom-side solder mask should cover the five or nine holes of the thermal pad area. This prevents solder from being pulled away from the thermal pad area during the reflow process.
7. Apply solder paste to the exposed thermal pad area and all of the IC terminals.
8. With these preparatory steps in place, the TLC08x IC is simply placed in position and run through the solder reflow operation as any standard surface-mount component. This results in a part that is properly installed.
For a given $\theta_{\mathrm{JA}}$, the maximum power dissipation is shown in Figure 54 and is calculated by the following formula:

Where:

$$
P_{D}=\left(\frac{T_{M A X}{ }^{-T} A}{{ }_{\mathrm{JA}}}\right)
$$

$$
\begin{aligned}
& \mathrm{P}_{\mathrm{D}}=\text { Maximum power dissipation of TLC08x IC (watts) } \\
& \mathrm{T}_{\mathrm{MAX}}=\text { Absolute maximum junction temperature }\left(150^{\circ} \mathrm{C}\right) \\
& \mathrm{T}_{\mathrm{A}}=\text { Free-ambient air temperature }\left({ }^{\circ} \mathrm{C}\right) \\
& \theta_{\mathrm{JA}}=\theta_{\mathrm{JC}}+\theta_{\mathrm{CA}} \\
& \theta_{\mathrm{JC}}=\text { Thermal coefficient from junction to case } \\
& \theta_{\mathrm{CA}}=\text { Thermal coefficient from case to ambient air }\left({ }^{\circ} \mathrm{C} / \mathrm{W}\right)
\end{aligned}
$$

# TLC080, TLC081, TLC082, TLC083, TLC084, TLC085, TLC08xA FAMILY OF WIDE-BANDWIDTH HIGH-OUTPUT-DRIVE SINGLE SUPPLY OPERATIONAL AMPLIFIERS <br> SLOS254C - JUNE 1999 - REVISED NOVEMBER 2000 

## APPLICATION INFORMATION

## general PowerPAD design considerations (continued)

MAXIMUM POWER DISSIPATION
VS
FREE-AIR TEMPERATURE


NOTE A: Results are with no air flow and using JEDEC Standard Low-K test PCB.
Figure 54. Maximum Power Dissipation vs Free-Air Temperature
The next consideration is the package constraints. The two sources of heat within an amplifier are quiescent power and output power. The designer should never forget about the quiescent heat generated within the device, especially multi-amplifier devices. Because these devices have linear output stages (Class A-B), most of the heat dissipation is at low output voltages with high output currents.
The other key factor when dealing with power dissipation is how the devices are mounted on the PCB. The PowerPAD devices are extremely useful for heat dissipation. But, the device should always be soldered to a copper plane to fully use the heat dissipation properties of the PowerPAD. The SOIC package, on the other hand, is highly dependent on how it is mounted on the PCB. As more trace and copper area is placed around the device, $\theta_{J A}$ decreases and the heat dissipation capability increases. The currents and voltages shown in these graphs are for the total package. For the dual or quad amplifier packages, the sum of the RMS output currents and voltages should be used to choose the proper package.

# TLC080, TLC081, TLC082, TLC083, TLC084, TLC085, TLC08xA FAMILY OF WIDE-BANDWIDTH HIGH-OUTPUT-DRIVE SINGLE SUPPLY <br> OPERATIONAL AMPLIFIERS <br> SLOS254C - JUNE 1999 - REVISED NOVEMBER 2000 

## APPLICATION INFORMATION

## macromodel information

Macromodel information provided was derived using Microsim Parts ${ }^{\text {TM }}$, the model generation software used with Microsim PSpice ${ }^{T M}$. The Boyle macromodel (see Note 1) and subcircuit in Figure 55 are generated using the TLC08x typical electrical and operating characteristics at $T_{A}=25^{\circ} \mathrm{C}$. Using this information, output simulations of the following key parameters can be generated to a tolerance of $20 \%$ (in most cases):

- Maximum positive output voltage swing
- Maximum negative output voltage swing
- Slew rate
- Quiescent power dissipation
- Input bias current
- Open-loop voltage amplification
- Unity-gain frequency
- Common-mode rejection ratio
- Phase margin
- DC output resistance
- AC output resistance
- Short-circuit output current limit

NOTE 2: G. R. Boyle, B. M. Cohn, D. O. Pederson, and J. E. Solomon, "Macromodeling of Integrated Circuit Operational Amplifiers," IEEE Journal of Solid-State Circuits, SC-9, 353 (1974).

[^1]
## APPLICATION INFORMATION





Figure 55. Boyle Macromodel and Subcircuit

MECHANICAL DATA
D (R-PDSO-G**)
PLASTIC SMALL-OUTLINE PACKAGE
14 PIN SHOWN


| PINS ** | $\mathbf{8}$ | $\mathbf{1 4}$ | 16 |
| :---: | :---: | :---: | :---: |
| A MAX | 0.197 <br> $(5,00)$ | 0.344 <br> $(8,75)$ | 0.394 <br> $(10,00)$ |
| A MIN | 0.189 <br> $(4,80)$ | 0.337 <br> $(8,55)$ | 0.386 <br> $(9,80)$ |

NOTES: A. All linear dimensions are in inches (millimeters).
B. This drawing is subject to change without notice
C. Body dimensions do not include mold flash or protrusion, not to exceed $0.006(0,15)$.
D. Falls within JEDEC MS-012


4073271/A 04/98

NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. Body dimensions include mold flash or protrusions.
D. The package thermal performance may be enhanced by attaching an external heat sink to the thermal pad. This pad is electrically and thermally connected to the backside of the die and possibly selected leads.
E. Falls within JEDEC MO-187

# TLC080, TLC081, TLC082, TLC083, TLC084, TLC085, TLC08xA FAMILY OF WIDE-BANDWIDTH HIGH-OUTPUT-DRIVE SINGLE SUPPLY OPERATIONAL AMPLIFIERS <br> SLOS254C - JUNE 1999 - REVISED NOVEMBER 2000 

MECHANICAL INFORMATION
DGQ (S-PDSO-G10)
PowerPADTM PLASTIC SMALL-OUTLINE PACKAGE


NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. Body dimensions do not include mold flash or protrusion.
D. The package thermal performance may be enhanced by bonding the thermal pad to an external thermal plane This pad is electrically and thermally connected to the backside of the die and possibly selected leads.

## TLC080, TLC081, TLC082, TLC083, TLC084, TLC085, TLC08xA

 FAMILY OF WIDE-BANDWIDTH HIGH-OUTPUT-DRIVE SINGLE SUPPLY OPERATIONAL AMPLIFIERSSLOS254C - JUNE 1999 - REVISED NOVEMBER 2000
MECHANICAL INFORMATION
N (R-PDIP-T**)
PLASTIC DUAL-IN-LINE PACKAGE
16 PIN SHOWN


NOTES: A. All linear dimensions are in inches (millimeters).
B. This drawing is subject to change without notice.
C. Falls within JEDEC MS-001 ( 20 pin package is shorter then MS-001.)

MECHANICAL INFORMATION
P (R-PDIP-T8)
PLASTIC DUAL-IN-LINE PACKAGE


NOTES: A. All linear dimensions are in inches (millimeters).
B. This drawing is subject to change without notice.
C. Falls within JEDEC MS-001

## MECHANICAL INFORMATION

PWP (R-PDSO-G**)
PowerPAD ${ }^{\text {TM }}$ PLASTIC SMALL-OUTLINE
20 PINS SHOWN


| PIM PINS ** | $\mathbf{1 4}$ | $\mathbf{1 6}$ | $\mathbf{2 0}$ | $\mathbf{2 4}$ | $\mathbf{2 8}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A MAX | 5,10 | 5,10 | 6,60 | 7,90 | 9,80 |
| A MIN | 4,90 | 4,90 | 6,40 | 7,70 | 9,60 |

NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. Body dimensions do not include mold flash or protrusions.
D. The package thermal performance may be enhanced by bonding the thermal pad to an external thermal plane. This pad is electrically and thermally connected to the backside of the die and possibly selected leads.
E. Falls within JEDEC MO-153

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[^0]:    † Full range is $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ for C suffix and $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ for I suffix. If not specified, full range is $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$.

[^1]:    PSpice and Parts are trademarks of MicroSim Corporation.

