## **Power MOSFET 60 Amps, 60 Volts, Logic Level** N-Channel TO-220 and D<sup>2</sup>PAK

Designed for low voltage, high speed switching applications in power supplies, converters, power motor controls and bridge circuits.

#### **Typical Applications**

- Power Supplies
- Converters
- Power Motor Controls
- Bridge Circuits

#### **MAXIMUM RATINGS** (T<sub>C</sub> = $25^{\circ}$ C unless otherwise noted)

Rating	Symbol	Value	Unit		
Drain-to-Source Voltage	V <sub>DSS</sub>	60	Vdc		
Drain-to-Gate Voltage ( $R_{GS}$ = 10 M $\Omega$ )	V <sub>DGR</sub>	60	Vdc		
Gate-to-Source Voltage - Continuous - Non-Repetitive (t <sub>p</sub> ≤10 ms)	V <sub>GS</sub> V <sub>GS</sub>	±15 ±20	Vdc		
Drain Current - Continuous @ $T_A = 25^{\circ}C$ - Continuous @ $T_A 100^{\circ}C$ - Single Pulse ( $t_p \le 10 \ \mu s$ )	I <sub>D</sub> I <sub>D</sub> I <sub>DM</sub>	60 42.3 180	Adc Apk		
Total Power Dissipation @ $T_A = 25^{\circ}C$ Derate above $25^{\circ}C$ Total Power Dissipation @ $T_A = 25^{\circ}C$ (Note 1)	P <sub>D</sub>	150 1.0 2.4	W W/°C W		
Operating and Storage Temperature Range	T <sub>J</sub> , T <sub>stg</sub>	- 55 to 175	°C		
Single Pulse Drain-to-Source Avalanche Energy - Starting $T_J = 25^{\circ}C$ ( $V_{DD} = 75$ Vdc, $V_{GS} = 5.0$ Vdc, L = 0.3 mH, I <sub>L</sub> (pk) = 55 A, V <sub>DS</sub> = 60 Vdc)	E <sub>AS</sub>	454	mJ		
Thermal Resistance - Junction-to-Case - Junction-to-Ambient (Note 1)	R <sub>θJC</sub> R <sub>θJA</sub>	1.0 62.5	°C/W		
Maximum Lead Temperature for Soldering Purposes, 1/8" from case for 10 seconds	ΤL	260	°C		

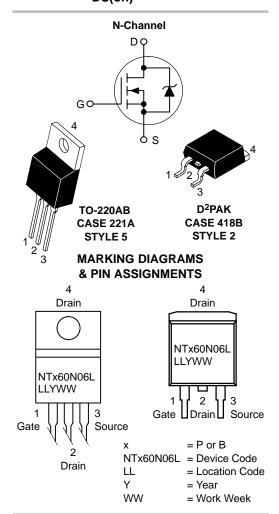
 When surface mounted to an FR4 board using the minimum recommended pad size, (Cu Area 0.412 in<sup>2</sup>).



## **ON Semiconductor®**

http://onsemi.com

60 AMPERES 60 VOLTS R<sub>DS(on)</sub> = 16 mΩ



#### **ORDERING INFORMATION**

Device	Package	Shipping
NTP60N06L	TO-220AB	50 Units/Rail
NTB60N06L	D <sup>2</sup> PAK	50 Units/Rail
NTB60N06LT4	D <sup>2</sup> PAK	800/Tape & Reel

1

#### **ELECTRICAL CHARACTERISTICS** ( $T_C = 25^{\circ}C$ unless otherwise noted)

Characteristic			Min	Тур	Мах	Unit
OFF CHARACTERISTICS						
Drain-to-Source Breakdown Voltage (Note 2) ( $V_{GS} = 0 \text{ Vdc}, I_D = 250 \mu \text{Adc}$ ) Temperature Coefficient (Positive)		V <sub>(BR)DSS</sub>	60 -	72.8 75.2	- -	Vdc mV/°C
Zero Gate Voltage Drain Cut ( $V_{DS} = 60 \text{ Vdc}, V_{GS} = 0 \text{ Vdc}$ ) ( $V_{DS} = 60 \text{ Vdc}, V_{GS} = 0 \text{ Vdc}$ )	dc)	I <sub>DSS</sub>	-		1.0 10	μAdc
Gate-Body Leakage Current	$(V_{GS} = \pm 15 \text{ Vdc}, V_{DS} = 0 \text{ Vdc})$	I <sub>GSS</sub>	-	-	±100	nAdc
ON CHARACTERISTICS (Not	e 2)					
Gate Threshold Voltage (Not ( $V_{DS} = V_{GS}$ , $I_D = 250 \mu$ Ad Threshold Temperature Coe	c)	V <sub>GS(th)</sub>	1.0 -	1.58 5.4	2.0	Vdc mV/°C
Static Drain-to-Source On-Resistance (Note 2) $(V_{GS} = 5.0 \text{ Vdc}, I_D = 30 \text{ Adc})$		R <sub>DS(on)</sub>	-	12.4	16	mΩ
Static Drain-to-Source On-Voltage (Note 2) ( $V_{GS} = 5.0$ Vdc, $I_D = 60$ Adc) ( $V_{GS} = 5.0$ Vdc, $I_D = 30$ Adc, $T_J = 150^{\circ}$ C)		V <sub>DS(on)</sub>		0.793 0.861	1.17 -	Vdc
Forward Transconductance (Note 2) ( $V_{DS}$ = 8.0 Vdc, $I_D$ = 12 Adc)		9 <sub>FS</sub>	-	48	-	mhos
OYNAMIC CHARACTERISTIC	S					
Input Capacitance		C <sub>iss</sub>	-	2195	3075	pF
Output Capacitance	(V <sub>DS</sub> = 25 Vdc, V <sub>GS</sub> = 0 Vdc, f = 1.0 MHz)	C <sub>oss</sub>	-	675	945	
Transfer Capacitance	, , , , , , , , , , , , , , , , , , ,	C <sub>rss</sub>	-	188	380	
SWITCHING CHARACTERIS	TICS (Note 3)					
Turn-On Delay Time		t <sub>d(on)</sub>	-	50.4	100	ns
Rise Time	$(V_{DD} = 48 \text{ Vdc}, I_D = 60 \text{ Adc}, V_{GS} = 5.0 \text{ Vdc},$	t <sub>r</sub>	-	576	1160	
Turn-Of f Delay Time	$R_{G} = 9.1 \Omega$ (Note 2)	t <sub>d(off)</sub>	-	100	200	
Fall Time		t <sub>f</sub>	-	237	480	
Gate Charge	(V <sub>DS</sub> = 48 Vdc, I <sub>D</sub> = 60 Adc, V <sub>GS</sub> = 5.0 Vdc) (Note 2)	QT	-	43.2	65	nC
		Q <sub>1</sub>	-	6.4	-	
		Q <sub>2</sub>	-	29	-	
SOURCE-DRAIN DIODE CH	ARACTERISTICS					
Forward On-Voltage	$      (I_S = 60 \text{ Adc}, \text{ V}_{GS} = 0 \text{ Vdc}) \text{ (Note 2)} \\       (I_S = 60 \text{ Adc}, \text{ V}_{GS} = 0 \text{ Vdc}, \text{ T}_J = 150^\circ\text{C}) $	$V_{SD}$	-	0.98 0.86	1.05 -	Vdc
Reverse Recovery Time	<i>(</i> , <u>, , , , , , , , , , , , , , , , , , </u>	t <sub>rr</sub>	-	81.9	-	ns
	(I <sub>S</sub> = 60 Adc, V <sub>GS</sub> = 0 Vdc, dI <sub>S</sub> /dt = 100 A/µs) (Note 2)	t <sub>a</sub>	-	42.1	-	
		t <sub>b</sub>	-	39.8	-	

Reverse Recovery Stored Charge

Pulse Test: Pulse Width ≤ 300 μs, Duty Cycle ≤ 2%.
Switching characteristics are independent of operating junction temperature.

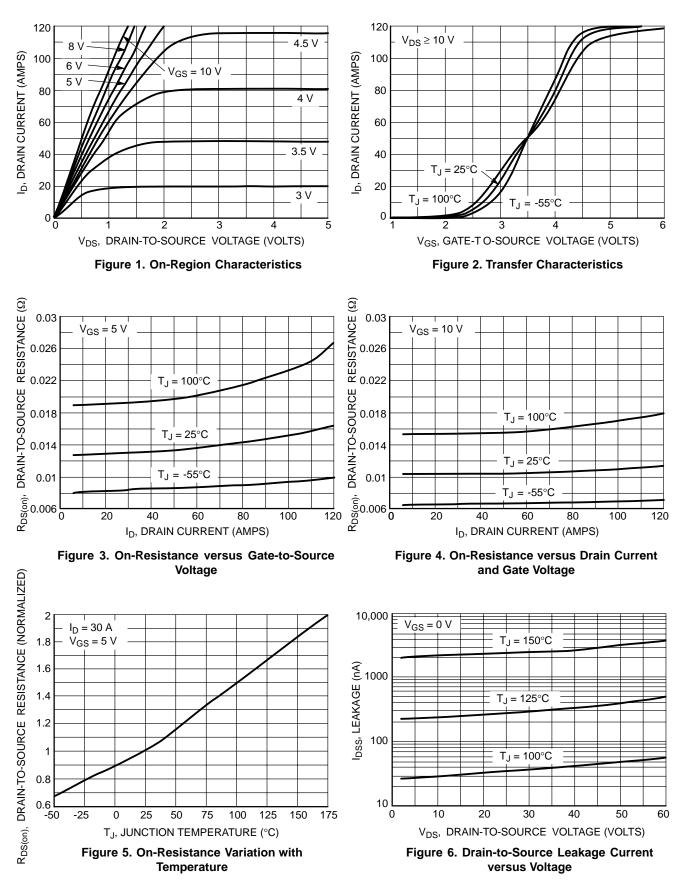
 $Q_{RR}$ 

-

0.172

-

μC



#### POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals ( $\Delta t$ ) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain-gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ( $I_{G(AV)}$ ) can be made from a rudimentary analysis of the drive circuit so that

 $t = Q/I_{G(AV)}$ 

During the rise and fall time interval when switching a resistive load,  $V_{GS}$  remains virtually constant at a level known as the plateau voltage,  $V_{SGP}$ . Therefore, rise and fall times may be approximated by the following:

 $t_r = Q_2 \ x \ R_G / (V_{GG} - V_{GSP})$  $t_f = Q_2 \ x \ R_G / V_{GSP}$ 

where

 $V_{GG}$  = the gate drive voltage, which varies from zero to  $V_{GG}$  $R_G$  = the gate drive resistance

and  $Q_2$  and  $V_{GSP}$  are read from the gate charge curve.

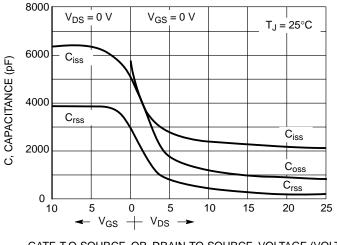
During the turn-on and turn-off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

$$\begin{split} t_{d(on)} &= R_G \; C_{iss} \; In \; [V_{GG}/(V_{GG} - \; V_{GSP})] \\ t_{d(off)} &= R_G \; C_{iss} \; In \; (V_{GG}/V_{GSP}) \end{split}$$

The capacitance ( $C_{iss}$ ) is read from the capacitance curve at a voltage corresponding to the off-state condition when calculating  $t_{d(on)}$  and is read at a voltage corresponding to the on-state when calculating  $t_{d(off)}$ .

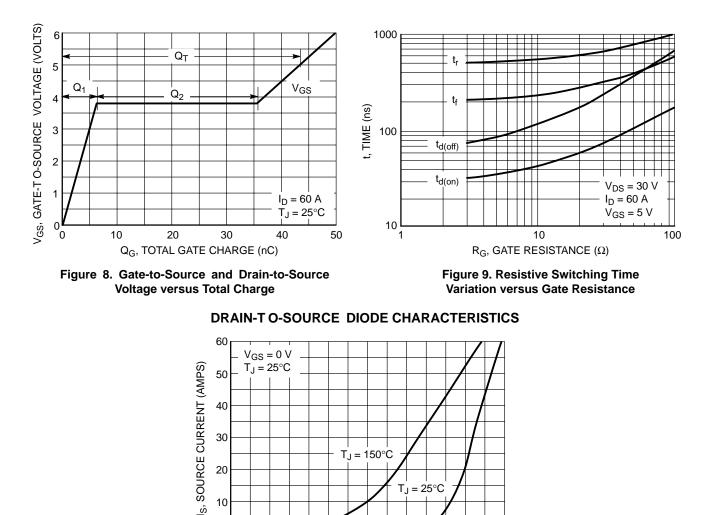
At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.



GATE-T O-SOURCE OR DRAIN-TO-SOURCE VOLTAGE (VOLTS)

Figure 7. Capacitance Variation



V<sub>SD</sub>, SOURCE-TO-DRAIN VOLTAGE (VOLTS) Figure 10. Diode Forward Voltage versus Current

0.62

 $T_J = 150^{\circ}C$ 

T<sub>J</sub> = 25°C

0.7

0.78

0.86

#### SAFE OPERATING AREA

0.54

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain-to-source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature ( $T_C$ ) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance -General Data and Its Use."

30

20

10

0 0.3

0.38

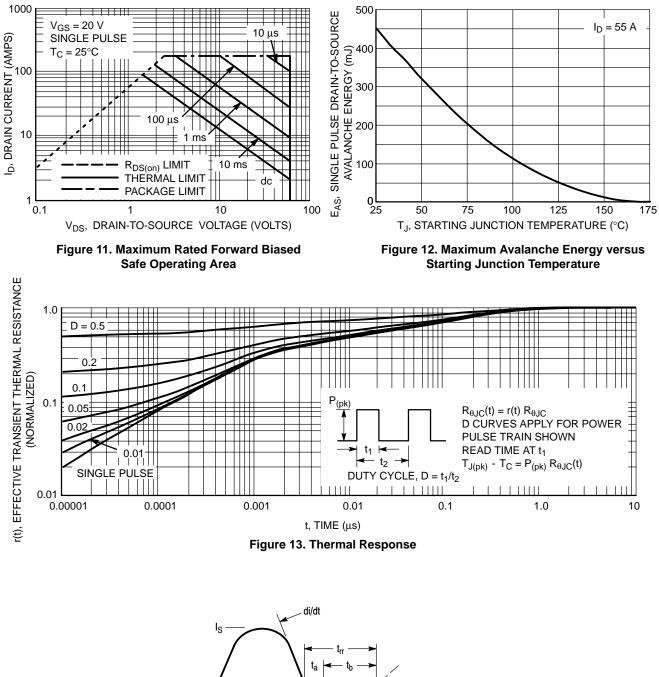
0.46

Switching between the off-state and the on-state may traverse any load line provided neither rated peak current (IDM) nor rated voltage (VDSS) is exceeded and the transition time  $(t_r, t_f)$  do not exceed 10 µs. In addition the total power averaged over a complete switching cycle must not exceed ( $T_{J(MAX)} - T_C$ )/( $R_{\theta JC}$ ).

A Power MOSFET designated E-FET can be safely used in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non-linearly with an increase of peak current in avalanche and peak junction temperature.

Although many E-FETs can withstand the stress of drain-to-source avalanche at currents up to rated pulsed current (I<sub>DM</sub>), the energy rating is specified at rated continuous current (I<sub>D</sub>), in accordance with industry custom. The energy rating must be derated for temperature as shown in the accompanying graph (Figure 12). Maximum energy at currents below rated continuous ID can safely be assumed to equal the values indicated.

#### SAFE OPERATING AREA



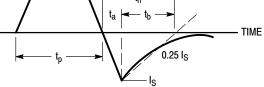
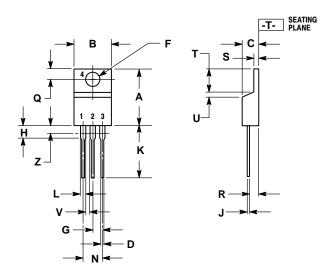


Figure 14. Diode Reverse Recovery Waveform

#### PACKAGE DIMENSIONS

**TO-220 THREE-LEAD TO-220AB** CASE 221A-09 **ISSUE AA** 



NOTES: 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982. 2. CONTROLLING DIMENSION: INCH. 3. DIMENSION Z DEFINES A ZONE WHERE ALL BODY AND LEAD IRREGULARITIES ARE ALLOWED.

	INC	HES	MILLIMETERS MIN MAX		
DIM	MIN	MAX			
Α	0.570	0.620	14.48	15.75	
В	0.380	0.405	9.66	10.28	
С	0.160	0.190	4.07	4.82	
D	0.025	0.035	0.64	0.88	
F	0.142	0.147	3.61	3.73	
G	0.095	0.105	2.42	2.66	
Η	0.110	0.155	2.80	3.93	
J	0.018	0.025	0.46	0.64	
K	0.500	0.562	12.70	14.27	
L	0.045	0.060	1.15	1.52	
Ν	0.190	0.210	4.83	5.33	
Q	0.100	0.120	2.54	3.04	
R	0.080	0.110	2.04	2.79	
S	0.045	0.055	1.15	1.39	
Т	0.235	0.255	5.97	6.47	
U	0.000	0.050	0.00	1.27	
٧	0.045		1.15		
Ζ		0.080		2.04	

PIN 1. GATE DRAIN 2.

3. SOURCE DRAIN 4.

С Ε ν -B-Α S 2 3 ۷ -Tκ SEATING → G 🔫 J н D 3 PL ⊕ 0.13 (0.005) M T B M

NOTES: 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982. 2. CONTROLLING DIMENSION: INCH.

	INCHES		MILLIN	IETERS
DIM	MIN	MAX	MIN	MAX
Α	0.340	0.380	8.64	9.65
В	0.380	0.405	9.65	10.29
С	0.160	0.190	4.06	4.83
D	0.020	0.035	0.51	0.89
Е	0.045	0.055	1.14	1.40
G	0.100	BSC	2.54 BSC	
Н	0.080	0.110	2.03	2.79
J	0.018	0.025	0.46	0.64
Κ	0.090	0.110	2.29	2.79
S	0.575	0.625	14.60	15.88
٧	0.045	0.055	1.14	1.40

STYLE 2: PIN 1. GATE 2. DRAIN 3. SOURCE 4. DRAIN

D<sup>2</sup>PAK CASE 418B-03 ISSUE D

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