## Power MOSFET 20 Amps, 60 Volts N-Channel DPAK

Designed for low voltage, high speed switching applications in power supplies, converters and power motor controls and bridge circuits.

#### Features

- Lower RDS(on)
- Lower V<sub>DS(on)</sub>
- Lower Capacitances
- Lower Total Gate Charge
- Lower and Tighter VSD
- Lower Diode Reverse Recovery Time
- Lower Reverse Recovery Stored Charge

#### **Typical Applications**

- Power Supplies
- Converters
- Power Motor Controls
- Bridge Circuits

#### **MAXIMUM RATINGS** (T<sub>J</sub> = $25^{\circ}$ C unless otherwise noted)

Rating	Symbol	Value	Unit
Drain-to-Source Voltage	VDSS	60	Vdc
Drain–to–Gate Voltage ( $R_{GS}$ = 10 M $\Omega$ )	VDGR	60	Vdc
Gate–to–Source Voltage – Continuous – Non–repetitive (t <sub>p</sub> ≤10 ms)	V <sub>GS</sub> V <sub>GS</sub>	±20 ±30	Vdc
Drain Current – Continuous @ $T_A = 25^{\circ}C$ – Continuous @ $T_A = 100^{\circ}C$ – Single Pulse ( $t_p \le 10 \ \mu s$ )	I <sub>D</sub> I <sub>D</sub> I <sub>DM</sub>	20 10 60	Adc Apk
Total Power Dissipation @ $T_A = 25^{\circ}C$ Derate above $25^{\circ}C$ Total Power Dissipation @ $T_A = 25^{\circ}C$ (Note 1.)Total Power Dissipation @ $T_A = 25^{\circ}C$ (Note 2.)	PD	60 0.40 1.88 1.36	W W/°C W W
Operating and Storage Temperature Range	T <sub>J</sub> , T <sub>stg</sub>	–55 to 175	°C
Single Pulse Drain–to–Source Avalanche Energy – Starting T <sub>J</sub> = $25^{\circ}$ C (V <sub>DD</sub> = $25$ Vdc, V <sub>GS</sub> = 10 Vdc, L = 1.0 mH, I <sub>L</sub> (pk) = 18.4 A, V <sub>DS</sub> = 60 Vdc)	E <sub>AS</sub>	170	mJ
Thermal Resistance – Junction–to–Case – Junction–to–Ambient (Note 1.) – Junction–to–Ambient (Note 2.)	R <sub>θ</sub> JC R <sub>θ</sub> JA R <sub>θ</sub> JA	2.5 80 110	°C/W
Maximum Lead Temperature for Soldering Purposes, 1/8" from case for 10 seconds	т∟	260	°C

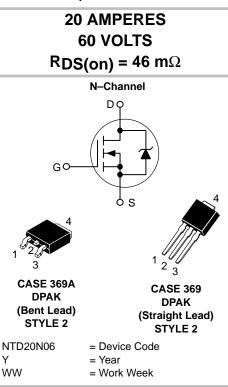
1. When surface mounted to an FR4 board using 1" pad size, (Cu Area 1.127 in<sup>2</sup>).

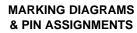
 When surface mounted to an FR4 board using the minimum recommended pad size, (Cu Area 0.412 in<sup>2</sup>).

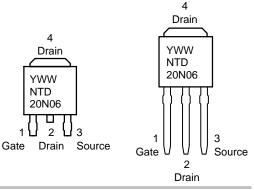


## ON Semiconductor<sup>™</sup>

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#### ORDERING INFORMATION

Device	Package	Shipping
NTD20N06	DPAK	75 Units/Rail
NTD20N06-1	DPAK Straight Lead	75 Units/Rail
NTD20N06T4	DPAK	2500 Tape & Reel

#### **ELECTRICAL CHARACTERISTICS** (T<sub>J</sub> = $25^{\circ}$ C unless otherwise noted)

	Symbol	Min	Тур	Max	Unit	
OFF CHARACTERISTICS						
Drain–to–Source Breakdown (V <sub>GS</sub> = 0 Vdc, I <sub>D</sub> = 250 μA Temperature Coefficient (Pos	V(BR)DSS	60 -	71.7 79.4		Vdc mV/°C	
Zero Gate Voltage Drain Curr ( $V_{DS} = 60 \text{ Vdc}, V_{GS} = 0 \text{ V}$ ( $V_{DS} = 60 \text{ Vdc}, V_{GS} = 0 \text{ V}$	IDSS			1.0 10	μAdc	
Gate-Body Leakage Current	$(V_{GS} = \pm 20 \text{ Vdc}, V_{DS} = 0 \text{ Vdc})$	IGSS	-	-	±100	nAdc
ON CHARACTERISTICS (Note	NO TAG)					
Gate Threshold Voltage (Note (V <sub>DS</sub> = V <sub>GS</sub> , I <sub>D</sub> = 250 μAd Threshold Temperature Coeff	VGS(th)	2.0 _	2.91 6.9	4.0	Vdc mV/°C	
Static Drain-to-Source On-R (V <sub>GS</sub> = 10 Vdc, I <sub>D</sub> = 10 Ad	R <sub>DS(on)</sub>	_	37.5	46	mΩ	
Static Drain-to-Source On-V (V <sub>GS</sub> = 10 Vdc, I <sub>D</sub> = 20 Ad (V <sub>GS</sub> = 10 Vdc, I <sub>D</sub> = 10 Ad	VDS(on)		0.78 1.57	1.10 -	Vdc	
Forward Transconductance (I	9FS	-	13.2	-	mhos	
DYNAMIC CHARACTERISTIC	S					
Input Capacitance		C <sub>iss</sub>	-	725	1015	pF
Output Capacitance	(V <sub>DS</sub> = 25 Vdc, V <sub>GS</sub> = 0 Vdc, f = 1.0 MHz)	C <sub>OSS</sub>	-	213	300	
Transfer Capacitance	,	C <sub>rss</sub>	-	58	120	
SWITCHING CHARACTERIST	ICS (Note NO TAG)					
Turn–On Delay Time		<sup>t</sup> d(on)	_	9.5	20	ns
Rise Time	(V <sub>DD</sub> = 30 Vdc, I <sub>D</sub> = 20 Adc, V <sub>GS</sub> = 10 Vdc,	tr	_	60.5	120	
Turn-Off Delay Time	$R_G = 9.1 \Omega$ ) (Note NO TAG)	<sup>t</sup> d(off)	_	27.1	60	
Fall Time		tf	-	37.1	80	
Gate Charge		QT	-	21.2	30	nC
	$(V_{DS} = 48 \text{ Vdc}, I_D = 20 \text{ Adc}, V_{GS} = 10 \text{ Vdc})$ (Note NO TAG)	Q <sub>1</sub>	-	5.6	-	_
		Q <sub>2</sub>	-	7.3	-	
SOURCE-DRAIN DIODE CHA	RACTERISTICS					
Forward On–Voltage	$(I_{S} = 20 \text{ Adc}, V_{GS} = 0 \text{ Vdc}) \text{ (Note}$ NO TAG) $(I_{S} = 20 \text{ Adc}, V_{GS} = 0 \text{ Vdc}, T_{J} = 150^{\circ}\text{C})$	V <sub>SD</sub>		1.0 0.87	1.2 _	Vdc
Reverse Recovery Time		t <sub>rr</sub>	-	42.9	-	ns
	$(I_S = 20 \text{ Adc}, V_{GS} = 0 \text{ Vdc},$ dI <sub>S</sub> /dt = 100 A/ $\mu$ s) (Note NO TAG)	<sup>t</sup> a	-	33	-	1
		tb	-	9.9	_	1

Reverse Recovery Stored Charge

Pulse Test: Pulse Width ≤ 300 μs, Duty Cycle ≤ 2%.
Switching characteristics are independent of operating junction temperatures.

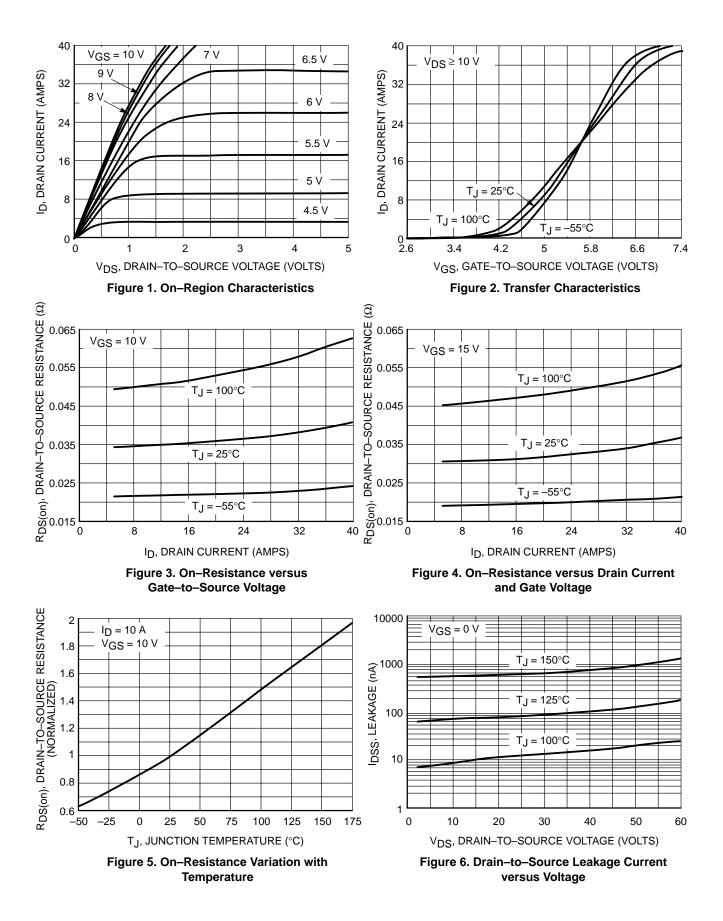
 $Q_{RR}$ 

0.084

\_

μC

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#### POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals ( $\Delta t$ ) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ( $I_G(AV)$ ) can be made from a rudimentary analysis of the drive circuit so that

 $t = Q/I_{G(AV)}$ 

During the rise and fall time interval when switching a resistive load,  $V_{GS}$  remains virtually constant at a level known as the plateau voltage,  $V_{SGP}$ . Therefore, rise and fall times may be approximated by the following:

 $t_r = Q_2 \times R_G / (V_{GG} - V_{GSP})$  $t_f = Q_2 \times R_G / V_{GSP}$ 

where

 $V_{GG}$  = the gate drive voltage, which varies from zero to  $V_{GG}$ 

 $R_G$  = the gate drive resistance

and  $Q_2$  and  $V_{\ensuremath{GSP}}$  are read from the gate charge curve.

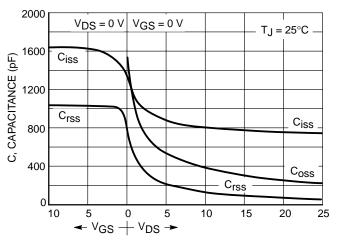
During the turn–on and turn–off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

$$\begin{split} t_{d(on)} &= R_G \ C_{iss} \ In \ [V_{GG}/(V_{GG} - V_{GSP})] \\ t_{d(off)} &= R_G \ C_{iss} \ In \ (V_{GG}/V_{GSP}) \end{split}$$

The capacitance ( $C_{ISS}$ ) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating  $t_{d(on)}$  and is read at a voltage corresponding to the on–state when calculating  $t_{d(off)}$ .

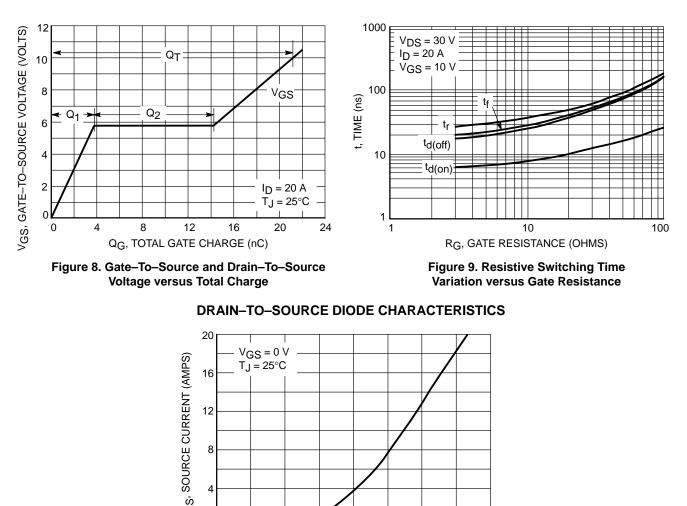
At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.



GATE-TO-SOURCE OR DRAIN-TO-SOURCE VOLTAGE (VOLTS)

Figure 7. Capacitance Variation



VSD, SOURCE-TO-DRAIN VOLTAGE (VOLTS) Figure 10. Diode Forward Voltage versus Current

0.8

0.9

#### SAFE OPERATING AREA

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain-to-source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature ( $T_C$ ) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance -General Data and Its Use."

12

8

4

0 0.6

0.7

Switching between the off-state and the on-state may traverse any load line provided neither rated peak current (IDM) nor rated voltage (VDSS) is exceeded and the transition time  $(t_r, t_f)$  do not exceed 10 µs. In addition the total power averaged over a complete switching cycle must not exceed  $(T_{J}(MAX) - T_{C})/(R_{\theta JC})$ .

A Power MOSFET designated E-FET can be safely used in switching circuits with unclamped inductive loads. For

reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non-linearly with an increase of peak current in avalanche and peak junction temperature.

1

Although many E-FETs can withstand the stress of drain-to-source avalanche at currents up to rated pulsed current (IDM), the energy rating is specified at rated continuous current (ID), in accordance with industry custom. The energy rating must be derated for temperature as shown in the accompanying graph (Figure 12). Maximum energy at currents below rated continuous ID can safely be assumed to equal the values indicated.

#### SAFE OPERATING AREA

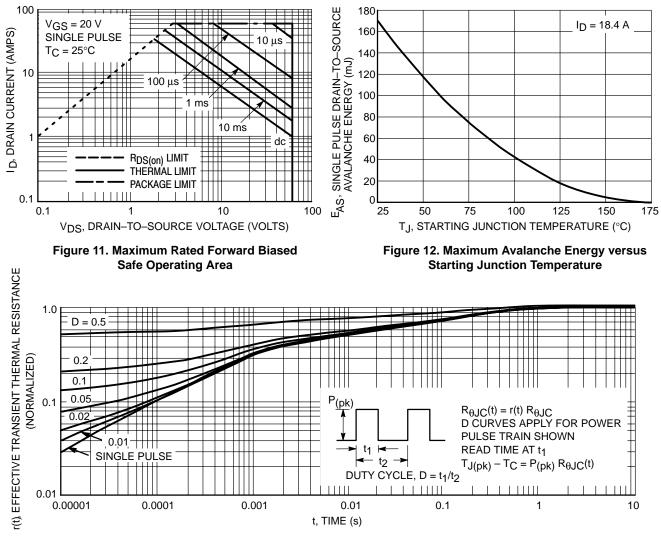


Figure 13. Thermal Response

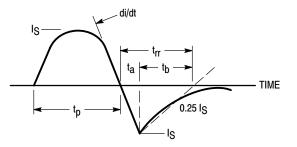
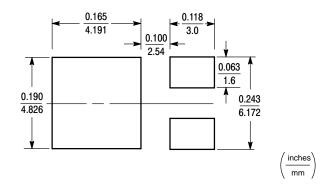


Figure 14. Diode Reverse Recovery Waveform

## INFORMATION FOR USING THE DPAK SURFACE MOUNT PACKAGE

### **RECOMMENDED FOOTPRINT FOR SURFACE MOUNTED APPLICATIONS**

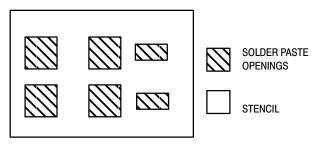
Surface mount board layout is a critical portion of the total design. The footprint for the semiconductor packages must be the correct size to ensure proper solder connection interface between the board and the package. With the correct pad geometry, the packages will self align when subjected to a solder reflow process.



#### SOLDER STENCIL GUIDELINES

Prior to placing surface mount components onto a printed circuit board, solder paste must be applied to the pads. Solder stencils are used to screen the optimum amount. These stencils are typically 0.008 inches thick and may be made of brass or stainless steel. For packages such as the SC-59, SC-70/SOT-323, SOD-123, SOT-23, SOT-143, SOT-223, SO-8, SO-14, SO-16, and SMB/SMC diode packages, the stencil opening should be the same as the pad size or a 1:1 registration. This is not the case with the DPAK and D<sup>2</sup>PAK packages. If one uses a 1:1 opening to screen solder onto the drain pad, misalignment and/or "tombstoning" may occur due to an excess of solder. For these two packages, the opening in the stencil for the paste should be approximately 50% of the tab area. The opening for the leads is still a 1:1 registration. Figure 15 shows a typical stencil for the DPAK and D<sup>2</sup>PAK packages. The

pattern of the opening in the stencil for the drain pad is not critical as long as it allows approximately 50% of the pad to be covered with paste.



#### Figure 15. Typical Stencil for DPAK and D<sup>2</sup>PAK Packages

## SOLDERING PRECAUTIONS

The melting temperature of solder is higher than the rated temperature of the device. When the entire device is heated to a high temperature, failure to complete soldering within a short time could result in device failure. Therefore, the following items should always be observed in order to minimize the thermal stress to which the devices are subjected.

- Always preheat the device.
- The delta temperature between the preheat and soldering should be 100°C or less.\*
- When preheating and soldering, the temperature of the leads and the case must not exceed the maximum temperature ratings as shown on the data sheet. When using infrared heating with the reflow soldering method, the difference shall be a maximum of 10°C.
- The soldering temperature and time shall not exceed 260°C for more than 10 seconds.

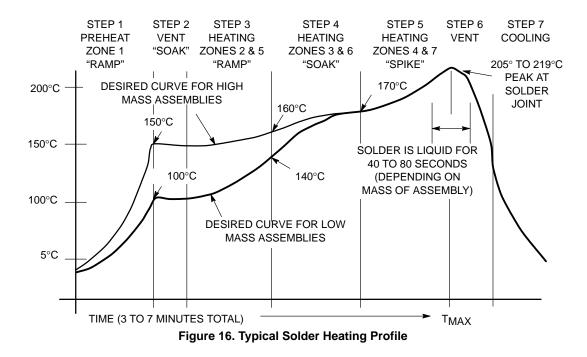
- When shifting from preheating to soldering, the maximum temperature gradient shall be 5°C or less.
- After soldering has been completed, the device should be allowed to cool naturally for at least three minutes. Gradual cooling should be used as the use of forced cooling will increase the temperature gradient and result in latent failure due to mechanical stress.
- Mechanical stress or shock should not be applied during cooling.

\* Soldering a device without preheating can cause excessive thermal shock and stress which can result in damage to the device.

\* Due to shadowing and the inability to set the wave height to incorporate other surface mount components, the D<sup>2</sup>PAK is not recommended for wave soldering.

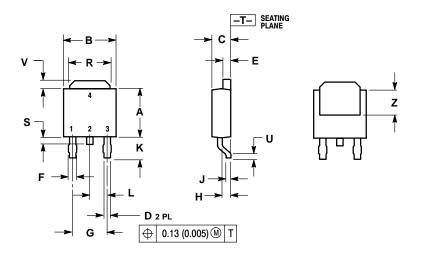
#### **TYPICAL SOLDER HEATING PROFILE**

For any given circuit board, there will be a group of control settings that will give the desired heat pattern. The operator must set temperatures for several heating zones, and a figure for belt speed. Taken together, these control settings make up a heating "profile" for that particular circuit board. On machines controlled by a computer, the computer remembers these profiles from one operating session to the next. Figure 16 shows a typical heating profile for use when soldering a surface mount device to a printed circuit board. This profile will vary among soldering systems but it is a good starting point. Factors that can affect the profile include the type of soldering system in use, density and types of components on the board, type of solder used, and the type of board or substrate material being used. This profile shows temperature versus time. The line on the graph shows the actual temperature that might be experienced on the surface of a test board at or near a central solder joint. The two profiles are based on a high density and a low density board. The Vitronics SMD310 convection/infrared reflow soldering system was used to generate this profile. The type of solder used was 62/36/2 Tin Lead Silver with a melting point between 177–189°C. When this type of furnace is used for solder reflow work, the circuit boards and solder joints tend to heat first. The components on the board are then heated by conduction. The circuit board, because it has a large surface area, absorbs the thermal energy more efficiently, then distributes this energy to the component may be up to 30 degrees cooler than the adjacent solder joint.



## PACKAGE DIMENSIONS

DPAK CASE 369A–13 ISSUE AB



NOTES: 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.

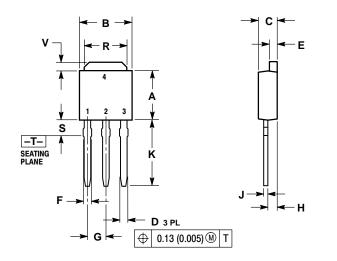
	114.000, 1002.
2.	CONTROLLING DIMENSION: INCH.

	INCHES		MILLIN	IETERS
DIM	MIN	MAX	MIN	MAX
Α	0.235	0.250	5.97	6.35
В	0.250	0.265	6.35	6.73
С	0.086	0.094	2.19	2.38
D	0.027	0.035	0.69	0.88
Е	0.033	0.040	0.84	1.01
F	0.037	0.047	0.94	1.19
G	0.180 BSC		4.58 BSC	
Н	0.034	0.040	0.87	1.01
J	0.018	0.023	0.46	0.58
K	0.102	0.114	2.60	2.89
L	0.090 BSC		BSC 2.29 BSC	
R	0.175	0.215	4.45	5.46
S	0.020	0.050	0.51	1.27
U	0.020		0.51	
۷	0.030	0.050	0.77	1.27
Z	0.138		3.51	

STYLE 2: PIN 1. GATE 2. DRAIN 3. SOURCE 4. DRAIN

## PACKAGE DIMENSIONS







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F	0.037	0.047	0.94	1.19
G	0.090 BSC		2.29 BSC	
Η	0.034	0.040	0.87 1.0	
ſ	0.018	0.023	0.46	0.58
Κ	0.350	0.380	8.89	9.65
R	0.175	0.215	4.45	5.46
s	0.050	0.090	1.27	2.28
٧	0.030	0.050	0.77	1.27

STYLE 2: PIN 1. GATE 2. DRAIN 3. SOURCE 4. DRAIN

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