March 1996

## General Description

The LM2588 series of regulators are monolithic integrated circuits specifically designed for flyback, step-up (boost), and forward converter applications. The device is available in 4 different output voltage versions: $3.3 \mathrm{~V}, 5.0 \mathrm{~V}, 12 \mathrm{~V}$, and adjustable.
Requiring a minimum number of external components, these regulators are cost effective, and simple to use. Included in the datasheet are typical circuits of boost and flyback regulators. Also listed are selector guides for diodes and capacitors and a family of standard inductors and flyback transformers designed to work with these switching regulators.
The power switch is a 5.0A NPN device that can stand-off 65 V . Protecting the power switch are current and thermal limiting circuits, and an undervoltage lockout circuit. This IC contains an adjustable frequency oscillator that can be programmed up to 200 kHz . The oscillator can also be synchronized with other devices, so that multiple devices can operate at the same switching frequency.
Other features include soft start mode to reduce in-rush current during start up, and current mode control for improved rejection of input voltage and output load transients and cy-cle-by-cycle current limiting. The device also has a shutdown pin, so that it can be turned off externally. An output voltage tolerance of $\pm 4 \%$, within specified input voltages and output load conditions, is guaranteed for the power supply system.

## Features

- Requires few external components
- Family of standard inductors and transformers
- NPN output switches 5.0 A , can stand off 65 V

■ Wide input voltage range: 4 V to 40 V
■ Adjustable switching frequency: 100 kHz to 200 kHz

- External shutdown capability
- Draws less than $60 \mu \mathrm{~A}$ when shut down
- Frequency synchronization
- Current-mode operation for improved transient response, line regulation, and current limit
- Internal soft-start function reduces in-rush current during start-up
- Output transistor protected by current limit, under voltage lockout, and thermal shutdown
■ System output voltage tolerance of $\pm 4 \%$ max over line and load conditions

Typical Applications

- Flyback regulator
- Forward converter
- Multiple-output regulator
- Simple boost regulator


## Flyback Regulator



TL/H/12420-1
Ordering Information

| Package Type | NSC Package <br> Drawing | Order Number |
| :--- | :---: | :---: |
| 7-Lead TO-220 Bent, Staggered Leads | TA07B | LM2588T-3.3, LM2588T-5.0, LM2588T-12, LM2588T-ADJ |
| 7-Lead TO-263 | TS7B | LM2588S-3.3, LM2588S-5.0, LM2588S-12, LM2588S-ADJ |
| 7-Lead TO-263 Tape and Reel | TS7B | LM2588SX-3.3, LM2588SX-5.0, LM2588SX-12, LM2588SX-ADJ |

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Absolute Maximum Ratings (Note 1)
If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications.

| Input Voltage | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq 45 \mathrm{~V}$ |
| :--- | ---: |
| Switch Voltage | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\text {SW }} \leq 65 \mathrm{~V}$ |
| Switch Current (Note 2) | Internally Limited |
| Compensation Pin Voltage | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\mathrm{COMP}} \leq 2.4 \mathrm{~V}$ |
| Feedback Pin Voltage | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\mathrm{FB}} \leq 2 \mathrm{~V}_{\mathrm{OUT}}$ |
| $\overline{\text { ON/OFF Pin Voltage }}$ | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\mathrm{SH}} \leq 6 \mathrm{~V}$ |
| Sync Pin Voltage | $-0.4 \mathrm{~V} \leq \mathrm{V}_{\text {SYNC }} \leq 2 \mathrm{~V}$ |


| Power Dissipation (Note 3) | Internally Limited |
| :--- | ---: |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 10 sec.$)$ | $260^{\circ} \mathrm{C}$ |
| Maximum Junction Temperature (Note 3) | $150^{\circ} \mathrm{C}$ |
| Minimum ESD Rating (C $=100 \mathrm{pF}, \mathrm{R}=1.5 \mathrm{k} \Omega$ ) | 2 kV |
| Operating Ratings |  |
| Cupply Voltage | $4 \mathrm{~V} \leq \mathrm{V}_{\mathrm{IN}} \leq 40 \mathrm{~V}$ |
| Output Switch Voltage | $0 \mathrm{~V} \leq \mathrm{V}_{\mathrm{SW}} \leq 60 \mathrm{~V}$ |
| Output Switch Current | $\mathrm{ISW} \leq 5.0 \mathrm{~A}$ |
| Junction Temperature Range | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{J}} \leq+125^{\circ} \mathrm{C}$ |

## Electrical Characteristics

Specifications with standard type face are for $T_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}$.

## LM2588-3.3

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SYSTEM PARAMETERS Test Circuit of Figure 1 (Note 4) |  |  |  |  |  |  |
| V OUT | Output Voltage | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=400 \mathrm{~mA} \text { to } 1.75 \mathrm{~A} \end{aligned}$ | 3.3 | 3.17/3.14 | 3.43/3.46 | V |
| $\Delta \mathrm{V}_{\text {OUT }} /$ <br> $\Delta \mathrm{V}_{\text {IN }}$ | Line Regulation | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=400 \mathrm{~mA} \end{aligned}$ | 20 |  | 50/100 | mV |
| $\Delta \mathrm{V}_{\text {OUT }} /$ <br> $\Delta I_{\text {LOAD }}$ | Load Regulation | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=400 \mathrm{~mA} \text { to } 1.75 \mathrm{~A} \end{aligned}$ | 20 |  | 50/100 | mV |
| $\eta$ | Efficiency | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ | 75 |  |  | \% |
| UNIQUE DEVICE PARAMETERS (Note 5) |  |  |  |  |  |  |
| $V_{\text {REF }}$ | Output Reference Voltage | Measured at Feedback Pin $\mathrm{V}_{\mathrm{COMP}}=1.0 \mathrm{~V}$ | 3.3 | 3.242/3.234 | 3.358/3.366 | V |
| $\Delta \mathrm{V}_{\text {REF }}$ | Reference Voltage Line Regulation | $\mathrm{V}_{\text {IN }}=4 \mathrm{~V}$ to 40 V | 2.0 |  |  | mV |
| $\mathrm{G}_{\mathrm{M}}$ | Error Amp <br> Transconductance | $\begin{aligned} & \mathrm{I}_{\mathrm{COMP}}=-30 \mu \mathrm{~A} \text { to }+30 \mu \mathrm{~A} \\ & \mathrm{~V}_{\mathrm{COMP}}=1.0 \mathrm{~V} \end{aligned}$ | 1.193 | 0.678 | 2.259 | mmho |
| Avol | Error Amp Voltage Gain | $\begin{aligned} & \mathrm{V}_{\mathrm{COMP}}=0.5 \mathrm{~V} \text { to } 1.6 \mathrm{~V} \\ & \mathrm{R}_{\mathrm{COMP}}=1.0 \mathrm{M} \Omega \text { (Note } 6 \text { ) } \end{aligned}$ | 260 | 151/75 |  | V/V |

## LM2588-5.0

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SYSTEM PARAMETERS Test Circuit of Figure 1 (Note 4) |  |  |  |  |  |  |
| V OUT | Output Voltage | $\begin{aligned} & \mathrm{V}_{\text {IN }}=4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=500 \mathrm{~mA} \text { to } 1.45 \mathrm{~A} \end{aligned}$ | 5.0 | 4.80/4.75 | 5.20/5.25 | V |
| $\Delta \mathrm{V}_{\text {OUT }} /$ <br> $\Delta V_{\text {IN }}$ | Line Regulation | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V} \text { to } 12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=500 \mathrm{~mA} \end{aligned}$ | 20 |  | 50/100 | mV |
| $\Delta \mathrm{V}_{\text {OUT }} /$ <br> $\Delta I_{\text {LOAD }}$ | Load Regulation | $\begin{aligned} & \mathrm{V}_{\text {IN }}=12 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=500 \mathrm{~mA} \text { to } 1.45 \mathrm{~A} \end{aligned}$ | 20 |  | 50/100 | mV |
| $\eta$ | Efficiency | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=750 \mathrm{~mA}$ | 80 |  |  | \% |

## Electrical Characteristics

Specifications with standard type face are for $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}$. (Continued)
LM2588-5.0 (Continued)

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| UNIQUE DEVICE PARAMETERS (Note 5) |  |  |  |  |  |  |
| $\mathrm{V}_{\text {REF }}$ | Output Reference Voltage | Measured at Feedback Pin $\mathrm{V}_{\mathrm{COMP}}=1.0 \mathrm{~V}$ | 5.0 | 4.913/4.900 | 5.088/5.100 | V |
| $\Delta \mathrm{V}_{\text {REF }}$ | Reference Voltage Line Regulation | $\mathrm{V}_{\text {IN }}=4 \mathrm{~V}$ to 40 V | 3.3 |  |  | mV |
| $\mathrm{G}_{\mathrm{M}}$ | Error Amp <br> Transconductance | $\begin{aligned} & \mathrm{I}_{\mathrm{COMP}}=-30 \mu \mathrm{~A} \text { to }+30 \mu \mathrm{~A} \\ & \mathrm{~V}_{\mathrm{COMP}}=1.0 \mathrm{~V} \end{aligned}$ | 0.750 | 0.447 | 1.491 | mmho |
| Avol | Error Amp <br> Voltage Gain | $\begin{aligned} & \mathrm{V}_{\mathrm{COMP}}=0.5 \mathrm{~V} \text { to } 1.6 \mathrm{~V} \\ & \mathrm{R}_{\mathrm{COMP}}=1.0 \mathrm{M} \Omega \text { (Note } 6 \text { ) } \end{aligned}$ | 165 | 99/49 |  | V/V |

## LM2588-12

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SYSTEM PARAMETERS Test Circuit of Figure 2 (Note 4) |  |  |  |  |  |  |
| $V_{\text {OUT }}$ | Output Voltage | $\begin{aligned} & \mathrm{V}_{I N}=4 \mathrm{~V} \text { to } 10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \text { to } 1.2 \mathrm{~A} \end{aligned}$ | 12.0 | 11.52/11.40 | 12.48/12.60 | V |
| $\Delta \mathrm{V}_{\text {OUT }} /$ <br> $\Delta \mathrm{V}_{\mathrm{IN}}$ | Line Regulation | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V} \text { to } 10 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{LOAD}}=300 \mathrm{~mA} \end{aligned}$ | 20 |  | 100/200 | mV |
| $\Delta \mathrm{V}_{\text {OUT }} /$ <br> $\Delta l_{\text {LOAD }}$ | Load Regulation | $\begin{aligned} & \mathrm{V}_{I N}=10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \text { to } 1.2 \mathrm{~A} \end{aligned}$ | 20 |  | 100/200 | mV |
| $\eta$ | Efficiency | $\mathrm{V}_{\text {IN }}=10 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ | 90 |  |  | \% |

UNIQUE DEVICE PARAMETERS (Note 5)

| $\mathrm{V}_{\text {REF }}$ | Output Reference <br> Voltage | Measured at Feedback Pin <br> $\mathrm{V}_{\mathrm{COMP}}=1.0 \mathrm{~V}$ | 12.0 | $11.79 / \mathbf{1 1 . 7 6}$ | $12.21 / \mathbf{1 2 . 2 4}$ | V |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| $\Delta \mathrm{V}_{\text {REF }}$ | Reference Voltage <br> Line Regulation | $\mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V}$ to 40 V | 7.8 |  |  | mV |
| $\mathrm{G}_{\mathrm{M}}$ | Error Amp <br> Transconductance | $\mathrm{I}_{\mathrm{COMP}}=-30 \mu \mathrm{~A}$ to $+30 \mu \mathrm{~A}$ <br> $\mathrm{~V}_{\mathrm{COMP}}=1.0 \mathrm{~V}$ | 0.328 | $\mathbf{0 . 1 8 6}$ | $\mathbf{0 . 6 2 1}$ | mmho |
| $\mathrm{A}_{\mathrm{VOL}}$ | Error Amp <br> Voltage | $\mathrm{V}_{\mathrm{COMP}}=0.5 \mathrm{~V}$ to 1.6 V <br> $\mathrm{R}_{\mathrm{COMP}}=1.0 \mathrm{M} \Omega($ Note 6$)$ | 70 | $41 / \mathbf{2 1}$ |  | $\mathrm{V} / \mathrm{V}$ |

## LM2588-ADJ

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SYSTEM PARAMETERS Test Circuit of Figure 2 (Note 4) |  |  |  |  |  |  |
| V OUT | Output Voltage | $\begin{aligned} & \mathrm{V}_{I N}=4 \mathrm{~V} \text { to } 10 \mathrm{~V} \\ & \mathrm{I}_{\mathrm{LOAD}}=300 \mathrm{~mA} \text { to } 1.2 \mathrm{~A} \end{aligned}$ | 12.0 | 11.52/11.40 | 12.48/12.60 | V |
| $\begin{aligned} & \Delta \mathrm{V}_{\text {OUT }} / \\ & \Delta \mathrm{V}_{\text {IN }} \\ & \hline \end{aligned}$ | Line Regulation | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=4 \mathrm{~V} \text { to } 10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \\ & \hline \end{aligned}$ | 20 |  | 100/200 | mV |
| $\begin{aligned} & \Delta V_{\text {OUT }} / \\ & \Delta l_{\text {LOAD }} \\ & \hline \end{aligned}$ | Load Regulation | $\begin{aligned} & \mathrm{V}_{I N}=10 \mathrm{~V} \\ & \mathrm{I}_{\text {LOAD }}=300 \mathrm{~mA} \text { to } 1.2 \mathrm{~A} \end{aligned}$ | 20 |  | 100/200 | mV |
| $\eta$ | Efficiency | $\mathrm{V}_{\mathrm{IN}}=10 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ | 90 |  |  | \% |

## Electrical Characteristics

Specifications with standard type face are for $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}$. (Continued)

## LM2588-ADJ (Continued)

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| UNIQUE DEVICE PARAMETERS (Note 5) |  |  |  |  |  |  |
| $\mathrm{V}_{\text {REF }}$ | Output Reference Voltage | Measured at Feedback Pin $\mathrm{V}_{\mathrm{COMP}}=1.0 \mathrm{~V}$ | 1.230 | 1.208/1.205 | 1.252/1.255 | V |
| $\Delta \mathrm{V}_{\text {REF }}$ | Reference Voltage Line Regulation | $\mathrm{V}_{\text {IN }}=4 \mathrm{~V}$ to 40 V | 1.5 |  |  | mV |
| $\mathrm{G}_{\mathrm{M}}$ | Error Amp <br> Transconductance | $\begin{aligned} & \mathrm{I}_{\mathrm{COMP}}=-30 \mu \mathrm{~A} \text { to }+30 \mu \mathrm{~A} \\ & \mathrm{~V}_{\mathrm{COMP}}=1.0 \mathrm{~V} \end{aligned}$ | 3.200 | 1.800 | 6.000 | mmho |
| Avol | Error Amp Voltage Gain | $\begin{aligned} & V_{\mathrm{COMP}}=0.5 \mathrm{~V} \text { to } 1.6 \mathrm{~V} \\ & R_{\mathrm{COMP}}=1.0 \mathrm{M} \Omega \text { (Note } 6 \text { ) } \end{aligned}$ | 670 | 400/200 |  | V/V |
| $\mathrm{I}_{\mathrm{B}}$ | Error Amp Input Bias Current | $\mathrm{V}_{\text {COMP }}=1.0 \mathrm{~V}$ | 125 |  | 425/600 | $n \mathrm{~A}$ |

COMMON DEVICE PARAMETERS for all versions (Note 5)

| Is | Input Supply Current | Switch Off <br> (Note 8) | 11 |  | 15.5/16.5 | mA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ISWITCH $=3.0 \mathrm{~A}$ | 85 |  | 140/165 | mA |
| $I_{\text {S/D }}$ | Shutdown Input Supply Current | $\mathrm{V}_{\mathrm{SH}}=3 \mathrm{~V}$ | 16 |  | 100/300 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\mathrm{UV}}$ | Input Supply Undervoltage Lockout | $\mathrm{R}_{\text {LOAD }}=100 \Omega$ | 3.30 | 3.05 | 3.75 | V |
| $\mathrm{fo}_{0}$ | Oscillator Frequency | Measured at Switch Pin $R_{\text {LOAD }}=100 \Omega, \mathrm{~V}_{\text {COMP }}=1.0 \mathrm{~V}$ Freq. Adj. Pin Open (Pin 1) | 100 | 85/75 | 115/125 | kHz |
|  |  | $\mathrm{R}_{\text {SET }}=22 \mathrm{k} \Omega$ | 200 |  |  | kHz |
| $\mathrm{f}_{\text {SC }}$ | Short-Circuit Frequency | Measured at Switch Pin <br> $R_{\text {LOAD }}=100 \Omega$ <br> $\mathrm{V}_{\text {FEEDBACK }}=1.15 \mathrm{~V}$ | 25 |  |  | kHz |
| $\mathrm{V}_{\text {EAO }}$ | Error Amplifier Output Swing | Upper Limit (Note 7) | 2.8 | 2.6/2.4 |  | V |
|  |  | Lower Limit (Note 8) | 0.25 |  | 0.40/0.55 | V |
| $I_{\text {EAO }}$ | Error Amp <br> Output Current <br> (Source or Sink) | (Note 9) | 165 | 110/70 | 260/320 | $\mu \mathrm{A}$ |
| Iss | Soft Start Current | $\begin{aligned} & \mathrm{V}_{\text {FEEDBACK }}=0.92 \mathrm{~V} \\ & \mathrm{~V}_{\text {COMP }}=1.0 \mathrm{~V} \end{aligned}$ | 11.0 | 8.0/7.0 | 17.0/19.0 | $\mu \mathrm{A}$ |
| $\mathrm{D}_{\text {MAX }}$ | Maximum Duty Cycle | $\begin{aligned} & R_{\text {LOAD }}=100 \Omega \\ & (\text { Note 7) } \end{aligned}$ | 98 | 93/90 |  | \% |
| $\mathrm{I}_{\mathrm{L}}$ | Switch Leakage Current | Switch Off $\mathrm{V}_{\text {SWITCH }}=60 \mathrm{~V}$ | 15 |  | 300/600 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {SUS }}$ | Switch Sustaining Voltage | $\mathrm{dV} / \mathrm{dT}=1.5 \mathrm{~V} / \mathrm{ns}$ |  | 65 |  | V |
| $\mathrm{V}_{\text {SAT }}$ | Switch Saturation Voltage | $\mathrm{I}_{\text {SWITCH }}=5.0 \mathrm{~A}$ | 0.7 |  | 1.1/1.4 | V |
| $\mathrm{I}_{\mathrm{CL}}$ | NPN Switch Current Limit |  | 6.5 | 5.0 | 9.5 | A |

## Electrical Characteristics

Specifications with standard type face are for $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, and those in bold type face apply over full Operating Temperature Range. Unless otherwise specified, $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}$. (Continued)

## LM2588-ADJ (Continued)

| Symbol | Parameters | Conditions | Typical | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| COMMON DEVICE PARAMETERS (Note 5) (Continued) |  |  |  |  |  |  |
| $\mathrm{V}_{\text {STH }}$ | Synchronization Threshold Voltage | $\begin{aligned} & \mathrm{F}_{\text {SYNC }}=200 \mathrm{kHz} \\ & \mathrm{~V}_{\mathrm{COMP}}=1 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=5 \mathrm{~V} \end{aligned}$ | 0.75 | 0.625/0.40 | 0.875/1.00 | V |
| $\mathrm{I}_{\text {SYNC }}$ | Synchronization Pin Current | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{COMP}}=1 \mathrm{~V}, \mathrm{~V}_{\mathrm{SYNC}}=\mathrm{V}_{\mathrm{STH}} \end{aligned}$ | 100 |  | 200 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {SHTH }}$ | $\overline{O N} / O F F$ Pin (Pin 1) <br> Threshold Voltage | $\begin{aligned} & \mathrm{V}_{\mathrm{COMP}}=1 \mathrm{~V} \\ & (\text { Note 10) } \end{aligned}$ | 1.6 | 1.0/0.8 | 2.2/2.4 | V |
| ISH | $\overline{O N} / O F F$ Pin (Pin 1) <br> Current | $\begin{aligned} & \mathrm{V}_{\mathrm{COMP}}=1 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{SH}}=\mathrm{V}_{\mathrm{SHTH}} \end{aligned}$ | 40 | 15/10 | 65/75 | $\mu \mathrm{A}$ |
| $\begin{aligned} & \theta_{\mathrm{JA}} \\ & \theta_{\mathrm{JA}} \\ & \theta_{\mathrm{JC}} \\ & \hline \end{aligned}$ | Thermal Resistance | T Package, Junction to Ambient (Note 11) T Package, Junction to Ambient (Note 12) T Package, Junction to Case | $\begin{gathered} 65 \\ 45 \\ 2 \end{gathered}$ |  |  |  |
| $\begin{aligned} & \theta_{\mathrm{JA}} \\ & \theta_{\mathrm{JA}} \\ & \theta_{\mathrm{JA}} \\ & \theta_{\mathrm{JC}} \\ & \hline \end{aligned}$ |  | S Package, Junction to Ambient (Note 13) <br> S Package, Junction to Ambient (Note 14) <br> S Package, Junction to Ambient (Note 15) <br> S Package, Junction to Case | $\begin{gathered} 56 \\ 35 \\ 26 \\ 2 \end{gathered}$ |  |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

Note 1: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. These ratings apply when the current is limited to less than 1.2 mA for pins $1,2,3$, and 6 . Operating ratings indicate conditions for which the device is intended to be functional, but device parameter specifications may not be guaranteed under these conditions. For guaranteed specifications and test conditions, see the Electrical Characteristics.
Note 2: Note that switch current and output current are not identical in a step-up regulator. Output current cannot be internally limited when the LM2588 is used as a step-up regulator. To prevent damage to the switch, the output current must be externally limited to 5 A . However, output current is internally limited when the LM2588 is used as a flyback regulator (see the Application Hints section for more information).
Note 3: The junction temperature of the device $\left(T_{J}\right)$ is a function of the ambient temperature ( $T_{A}$ ), the junction-to-ambient thermal resistance ( $\theta_{\mathrm{JA}}$ ), and the power dissipation of the device $\left(P_{D}\right)$. A thermal shutdown will occur if the temperature exceeds the maximum junction temperature of the device: $P_{D} \times \theta_{J A}+T_{A(M A X} \geq$
$T_{J(M A X)}$. For a safe thermal design, check that the maximum power dissipated by the device is less than: $P_{D} \leq\left[T_{J(M A X)}-T_{A(M A X)}\right] / \theta_{J A}$. When calculating the maximum allowable power dissipation, derate the maximum junction temperature-this ensures a margin of safety in the thermal design.
Note 4: External components such as the diode, inductor, input and output capacitors can affect switching regulator performance. When the LM2588 is used as shown in Figures 1 and 2, system performance will be as specified by the system parameters.
Note 5: All room temperature limits are 100\% production tested, and all limits at temperature extremes are guaranteed via correlation using standard Statistical Quality Control (SQC) methods.
Note 6: A $1.0 \mathrm{M} \Omega$ resistor is connected to the compensation pin (which is the error amplifier output) to ensure accuracy in measuring Avol.
Note 7: To measure this parameter, the feedback voltage is set to a low value, depending on the output version of the device, to force the error amplifier output high and the switch on.
Note 8: To measure this parameter, the feedback voltage is set to a high value, depending on the output version of the device, to force the error amplifier output ow and the switch off

Note 9: To measure the worst-case error amplifier output current, the LM2588 is tested with the feedback voltage set to its low value (specified in Note 7) and at its high value (specified in Note 8).
Note 10: When testing the minimum value, do not sink current from this pin-isolate it with a diode. If current is drawn from this pin, the frequency adjust circuit will begin operation (see Figure 41).
Note 11: Junction to ambient thermal resistance (no external heat sink) for the 7 lead TO-220 package mounted vertically, with $1 / 2$ inch leads in a socket, or on a PC board with minimum copper area.
Note 12: Junction to ambient thermal resistance (no external heat sink) for the 7 lead TO-220 package mounted vertically, with $1 / 2$ inch leads soldered to a PC board containing approximately 4 square inches of ( 1 oz. ) copper area surrounding the leads.
Note 13: Junction to ambient thermal resistance for the 7 lead TO-263 mounted horizontally against a PC board area of 0.136 square inches (the same size as the TO-263 package) of 1 oz . ( 0.0014 in . thick) copper.
Note 14: Junction to ambient thermal resistance for the 7 lead TO-263 mounted horizontally against a PC board area of 0.4896 square inches ( 3.6 times the area of the TO-263 package) of 1 oz . ( 0.0014 in. thick) copper.
Note 15: Junction to ambient thermal resistance for the 7 lead TO-263 mounted horizontally against a PC board copper area of 1.0064 square inches ( 7.4 times the area of the TO-263 package) of 1 oz. ( 0.0014 in. thick) copper. Additional copper area will reduce thermal resistance further. See the thermal model in Switchers Made Simple ${ }^{\circledR}$ software.

## Typical Performance Characteristics






Error Amp Transconductance vs Temperature
 TEMPERATURE (C) TL/H/12420-11


TL/H/12420-3


TL/H/12420-6

## Switch Transconductance

 vs Temperature

Error Amp Voltage Gain vs Temperature



TL/H/12420-4
Feedback Pin Bias Current vs Temperature


temperature (c)
TL/H/12420-10
Short Circuit Frequency vs Temperature


## Typical Performance Characteristics (Continued)



TL/H/12420-14


TL/H/12420-15


## Connection Diagrams



## Test Circuits



FIGURE 2. LM2588-12 and LM2588-ADJ

## Block Diagram



For Fixed Versions
$3.3 \mathrm{~V}, \mathrm{R} 1=3.4 \mathrm{k}, \mathrm{R} 2=2 \mathrm{k}$
$5.0 \mathrm{~V}, \mathrm{R} 1=6.15 \mathrm{k}, \mathrm{R} 2=2 \mathrm{k}$
$12 \mathrm{~V}, \mathrm{R} 1=8.73 \mathrm{k}, \mathrm{R} 2=1 \mathrm{k}$
For Adj. Version
R1 $=$ Short $(0 \Omega), R 2=$ Open

## FIGURE 3

## Flyback Regulator Operation

The LM2588 is ideally suited for use in the flyback regulator topology. The flyback regulator can produce a single output voltage, such as the one shown in Figure 4, or multiple output voltages. In Figure 4, the flyback regulator generates an output voltage that is inside the range of the input voltage. This feature is unique to flyback regulators and cannot be duplicated with buck or boost regulators.
The operation of a flyback regulator is as follows (refer to Figure 4): when the switch is on, current flows through the primary winding of the transformer, T 1 , storing energy in the magnetic field of the transformer. Note that the primary and secondary windings are out of phase, so no current flows through the secondary when current flows through the primary. When the switch turns off, the magnetic field col-
lapses, reversing the voltage polarity of the primary and secondary windings. Now rectifier D1 is forward biased and current flows through it, releasing the energy stored in the transformer. This produces voltage at the output.
The output voltage is controlled by modulating the peak switch current. This is done by feeding back a portion of the output voltage to the error amp, which amplifies the difference between the feedback voltage and a 1.230 V reference. The error amp output voltage is compared to a ramp voltage proportional to the switch current (i.e., inductor current during the switch on time). The comparator terminates the switch on time when the two voltages are equal, thereby controlling the peak switch current to maintain a constant output voltage.


TL/H/12420-24 As shown in Figure 4, the LM2588 can be used as a flyback regulator by using a minimum number of external components. The switching waveforms of this regulator are shown in Figure 5. Typical Performance Characteristics observed during the operation of this circuit are shown in Figure 6.

FIGURE 4. 12V Flyback Regulator Design Example

## Typical Performance Characteristics

A


TL/H/12420-60
FIGURE 5. Switching Waveforms


Horizontal: $2 \mathrm{~ms} / \mathrm{div}$
h Voltage, 10V/div
B: Switch Current, 5A/div
C: Output Rectifier Current, 5A/div
D: Output Ripple Voltage, $100 \mathrm{mV} / \mathrm{div}$
AC-Coupled
c
D

FIGURE 6. V ${ }_{\text {OUT }}$ Response to Load Current Step

## Typical Flyback Regulator Applications

Figures 7 through 12 show six typical flyback applications, varying from single output to triple output. Each drawing contains the part number(s) and manufacturer(s) for every component except the transformer. For the transformer part numbers and manufacturers' names, see the table in

Figure 13. For applications with different output voltagesrequiring the LM2588-ADJ-or different output configurations that do not match the standard configurations, refer to the Switchers Made Simple ${ }^{\circledR}$ software.


FIGURE 7. Single-Output Flyback Regulator


TL/H/12420-26
FIGURE 8. Single-Output Flyback Regulator

## Typical Flyback Regulator Applications (Continued)



TL/H/12420-27
FIGURE 9. Single-Output Flyback Regulator


FIGURE 10. Dual-Output Flyback Regulator
TL/H/12420-28

## FIGUE 10. Dual Output Flyback Regulator

Typical Flyback Regulator Applications (Continued)


## Typical Flyback Regulator Applications (Continued)

Transformer Selection (T)
Figure 13 lists the standard transformers available for flyback regulator applications. Included in the table are the turns ratio(s) for each transformer, as well as the output voltages, input voltage ranges, and the maximum load currents for each circuit.

| Applications | Figure 7 | Figure 8 | Figure 9 | Figure 10 | Figure 11 | Figure 12 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Transformers | T1 | T1 | T1 | T2 | T3 | T4 |
| $\mathrm{V}_{\text {IN }}$ | $4 \mathrm{~V}-6 \mathrm{~V}$ | $4 \mathrm{~V}-6 \mathrm{~V}$ | $8 \mathrm{~V}-16 \mathrm{~V}$ | $4 \mathrm{~V}-6 \mathrm{~V}$ | $18 \mathrm{~V}-36 \mathrm{~V}$ | $18 \mathrm{~V}-36 \mathrm{~V}$ |
| $\mathrm{~V}_{\text {OUT1 }}$ | 3.3 V | 5 V | 12 V | 12 V | 12 V | 5 V |
| $\mathrm{I}_{\text {OUT1 }}$ (Max) | 1.8 A | 1.4 A | 1.2 A | 0.3 A | 1 A | 2.5 A |
| $\mathrm{~N}_{1}$ | 1 | 1 | 1 | 2.5 | 0.8 | 0.35 |
| $\mathrm{~V}_{\text {OUT2 }}$ |  |  |  | -12 V | -12 V | 12 V |
| $\mathrm{I}_{\text {OUT2 }}$ (Max) |  |  |  | 0.3 A | 1 A | 0.5 A |
| $\mathrm{~N}_{2}$ |  |  | 2.5 | 0.8 | 0.8 |  |
| $\mathrm{~V}_{\text {OUT3 }}$ |  |  |  |  | -12 V |  |
| $\mathrm{I}_{\text {OUT3 }}$ (Max) |  |  |  |  |  | 0.5 A |
| $\mathrm{~N}_{3}$ |  |  |  |  | 0.8 |  |

FIGURE 13. Transformer Selection Table

| Transformer <br> Type | Manufacturers' Part Numbers |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Coilcraft <br> (Note 1) | Coilcraft (Note 1) <br> Surface Mount | Pulse (Note 2) <br> Surface Mount | Renco <br> (Note 3) | Schott <br> (Note 4) |
| T1 | Q4434-B | Q4435-B | PE-68411 | RL-5530 | 67141450 |
| T2 | Q4337-B | Q4436-B | PE-68412 | RL-5531 | 67140860 |
| T3 | Q4343-B | - | PE-68421 | RL-5534 | 67140920 |
| T4 | Q4344-B | - | PE-68422 | RL-5535 | 67140930 |


| Note 1: Coilcraft Inc., | Phone: (800) 322-2645 |
| :---: | :---: |
| 1102 Silver Lake Road, Cary, IL 60013 | Fax: (708) 639-1469 |
| European Headquarters, 21 Napier Place | Phone: + 441236730595 |
| Wardpark North, Cumbernauld, Scotland G68 0LL | Fax: +441236730627 |
| Note 2: Pulse Engineering Inc., | Phone: (619) 674-8100 |
| 12220 World Trade Drive, San Diego, CA 92128 | Fax: (619) 674-8262 |
| European Headquarters, Dunmore Road | Phone: + 3539324107 |
| Tuam, Co. Galway, Ireland | Fax: + 3539324459 |
| Note 3: Renco Electronics Inc., | Phone: (800) 645-5828 |
| 60 Jeffryn Blvd. East, Deer Park, NY 11729 | Fax: (516) 586-5562 |
| Note 4: Schott Corp., | Phone: (612) 475-1173 |
| 1000 Parkers Lane Road, Wayzata, MN 55391 | Fax: (612) 475-1786 |

FIGURE 14. Transformer Manufacturer Guide

## Typical Flyback Regulator Applications (Continued)

## Transformer Footprints

Figures 15 through 32 show the footprints of each transformer, listed in Figure 14.


FIGURE 15. Coilcraft Q4434-B


FIGURE 17. Coilcraft Q4343-B


FIGURE 19. Coilcraft Q4435-B (Surface Mount)


TL/H/12420-32
Top View FIGURE 16. Coilcraft Q4337-B


TL/H/12420-34
Top View
FIGURE 18. Coilcraft Q4344-B


FIGURE 20. Coilcraft Q4436-B (Surface Mount)

## Typical Flyback Regulator Applications (Continued)



FIGURE 21. Pulse PE-68411
(Surface Mount)


FIGURE 23. Pulse PE-68421
(Surface Mount)


TL/H/12420-41
Top View
FIGURE 25. Renco RL-5530

T2


FIGURE 22. Pulse PE-68412
(Surface Mount)


TL/H/12420-40
Top View
FIGURE 24. Pulse PE-68422 (Surface Mount)



## Step-Up (Boost) Regulator Operation

Figure 33 shows the LM2588 used as a step-up (boost) regulator. This is a switching regulator that produces an output voltage greater than the input supply voltage.
A brief explanation of how the LM2588 Boost Regulator works is as follows (refer to Figure 33). When the NPN switch turns on, the inductor current ramps up at the rate of $\mathrm{V}_{\mathrm{IN}} / \mathrm{L}$, storing energy in the inductor. When the switch turns
off, the lower end of the inductor flies above $\mathrm{V}_{\mathrm{IN}}$, discharging its current through diode (D) into the output capacitor (COUT) at a rate of $\left(\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }}\right) / \mathrm{L}$. Thus, energy stored in the inductor during the switch on time is transferred to the output during the switch off time. The output voltage is controlled by adjusting the peak switch current, as described in the flyback regulator section.


FIGURE 33. 12V Boost Regulator
By adding a small number of external components (as shown in Figure 33), the LM2588 can be used to produce a regulated output voltage that is greater than the applied input voltage. The switching waveforms observed during the operation of this circuit are shown in Figure 34. Typical performance of this regulator is shown in Figure 35.

## Typical Performance Characteristics



A: Switch Voltage,10V/div
B: Switch Current, 5A/div
C: Inductor Current, 5A/div
D: Output Ripple Voltage,
$100 \mathrm{mV} / \mathrm{div}$, AC-Coupled


FIGURE 35. V OUT Response to Load Current Step

FIGURE 34. Switching Waveforms

## Typical Boost Regulator Applications

Figures 36 and 38 through 40 show four typical boost appli-cations-one fixed and three using the adjustable version of the LM2588. Each drawing contains the part number(s) and manufacturer(s) for every component. For the fixed 12 V
output application, the part numbers and manufacturers' names for the inductor are listed in a table in Figure 37. For applications with different output voltages, refer to the Switchers Made Simple ${ }^{\circledR}$ software.


TL/H/12420-50
FIGURE 36. +5 V to $+\mathbf{1 2 V}$ Boost Regulator

Figure 37 contains a table of standard inductors, by part number and corresponding manufacturer, for the fixed output regulator of Figure 36.

| Coilcraft (Note 1) | Pulse (Note 2) | Renco (Note 3) | Schott (Note 4) |
| :---: | :---: | :---: | :---: |
| R4793-A | PE-53900 | RL-5472-5 | 67146520 |

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12220 World Trade Drive, San Diego, CA 92128
European Headquarters, Dunmore Road
Tuam, Co. Galway, Ireland
Note 3: Renco Electronics Inc.,
60 Jeffryn Blvd. East, Deer Park, NY 11729
Note 4: Schott Corp.,
Phone: (619) 674-8100 Fax: (619) 674-8262
Phone: + 3539324107 Fax: + 3539324459
Phone: (800) 645-5828 Fax: (516) 586-5562

1000 Parkers Lane Road, Wayzata, MN 55391
FIGURE 37. Inductor Selection Table

## Typical Boost Regulator Applications (Continued)



TL/H/12420-51
FIGURE 38. $+\mathbf{1 2 V}$ to +24 V Boost Regulator


TL/H/12420-53
FIGURE 40. +24 V to +48 V Boost Regulator
*The LM2588 will require a heat sink in these applications. The size of the heat sink will depend on the maximum ambient temperature. To calculate the thermal resistance of the IC and the size of the heat sink needed, see the "Heat Sink/Thermal Considerations" section in the Application Hints.

## Application Hints

LM2588 SPECIAL FEATURES


FIGURE 41. Shutdown Operation

## SHUTDOWN CONTROL

A feature of the LM2588 is its ability to be shut down using the ON/OFF pin (pin 1). This feature conserves input power by turning off the device when it is not in use. For proper operation, an isolation diode is required (as shown in Figure 41).

The device will shut down when 3 V or greater is applied on the $\overline{O N} / O F F$ pin, sourcing current into pin 1 . In shut down mode, the device will draw typically $56 \mu \mathrm{~A}$ of supply current ( $16 \mu \mathrm{~A}$ to $\mathrm{V}_{\mathrm{IN}}$ and $40 \mu \mathrm{~A}$ to the $\overline{\mathrm{ON}} /$ OFF pin). To turn the device back on, leave pin 1 floating, using an (isolation) diode, as shown in Figure 41 (for normal operation, do not source or sink current to or from this pin-see the next section).

## FREQUENCY ADJUSTMENT

The switching frequency of the LM2588 can be adjusted with the use of an external resistor. This feature allows the user to optimize the size of the magnetics and the output capacitor(s) by tailoring the operating frequency. A resistor connected from pin 1 (the Freq. Adj. pin) to ground will set the switching frequency from 100 kHz to 200 kHz (maximum). As shown in Figure 41, the pin can be used to adjust the frequency while still providing the shut down function. A curve in the Performance Characteristics Section graphs the resistor value to the corresponding switching frequency. The table in Figure 42 shows resistor values corresponding to commonly used frequencies.
However, changing the LM2588's operating frequency from its nominal value of 100 kHz will change the magnetics selection and compensation component values.

| $\mathbf{R}_{\mathbf{S E T}}(\mathbf{k} \Omega$ ) | Frequency (kHz) |
| :---: | :---: |
| Open | 100 |
| 200 | 125 |
| 47 | 150 |
| 33 | 175 |
| 22 | 200 |

FIGURE 42. Frequency Setting Resistor Guide


## FIGURE 43. Frequency Synchronization

## FREQUENCY SYNCHRONIZATION

Another feature of the LM2588 is the ability to synchronize the switching frequency to an external source, using the sync pin (pin 6). This feature allows the user to parallel multiple devices to deliver more output power.
A negative falling pulse applied to the sync pin will synchronize the LM2588 to an external oscillator (see Figures 43 and 44).
Use of this feature enables the LM2588 to be synchronized to an external oscillator, such as a system clock. This operation allows multiple power supplies to operate at the same frequency, thus eliminating frequency-related noise problems.


FIGURE 44. Waveforms of a Synchronized 12V Boost Regulator
The scope photo in Figure 44 shows a LM2588 12V Boost Regulator synchronized to a 200 kHz signal. There is a 700 ns delay between the falling edge of the sync signal and the turning on of the switch.

## Application Hints (Continued)



FIGURE 45. Boost Regulator

## PROGRAMMING OUTPUT VOLTAGE <br> output with an external current limit circuit. The external limit

 (SELECTING R1 AND R2)Referring to the adjustable regulator in Figure 45, the output voltage is programmed by the resistors R1 and R2 by the following formula:
$V_{\text {OUT }}=V_{\text {REF }}(1+R 1 / R 2) \quad$ where $V_{\text {REF }}=1.23 V$
Resistors R1 and R2 divide the output voltage down so that it can be compared with the 1.23 V internal reference. With R2 between 1 k and $5 \mathrm{k}, \mathrm{R} 1$ is:

$$
R 1=R 2\left(V_{\text {OUT }} / V_{R E F}-1\right) \quad \text { where } V_{R E F}=1.23 V
$$

For best temperature coefficient and stability with time, use $1 \%$ metal film resistors.

## SHORT CIRCUIT CONDITION

Due to the inherent nature of boost regulators, when the output is shorted (see Figure 45), current flows directly from the input, through the inductor and the diode, to the output, bypassing the switch. The current limit of the switch does not limit the output current for the entire circuit. To protect the load and prevent damage to the switch, the current must be externally limited, either by the input supply or at the
should be set to the maximum switch current of the device, which is 5 A .
In a flyback regulator application (Figure 46), using the standard transformers, the LM2588 will survive a short circuit to the main output. When the output voltage drops to $80 \%$ of its nominal value, the frequency will drop to 25 kHz . With a lower frequency, off times are larger. With the longer off times, the transformer can release all of its stored energy before the switch turns back on. Hence, the switch turns on initially with zero current at its collector. In this condition, the switch current limit will limit the peak current, saving the device.

## FLYBACK REGULATOR INPUT CAPACITORS

A flyback regulator draws discontinuous pulses of current from the input supply. Therefore, there are two input capacitors needed in a flyback regulator-one for energy storage and one for filtering (see Figure 46). Both are required due to the inherent operation of a flyback regulator. To keep a stable or constant voltage supply to the LM2588, a storage capacitor ( $2100 \mu \mathrm{~F}$ ) is required. If the input source is a


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FIGURE 46. Flyback Regulator

## Application Hints (Continued)

recitified DC supply and/or the application has a wide temperature range, the required rms current rating of the capacitor might be very large. This means a larger value of capacitance or a higher voltage rating will be needed for the input capacitor. The storage capacitor will also attenuate noise which may interfere with other circuits connected to the same input supply voltage.
In addition, a small bypass capacitor is required due to the noise generated by the input current pulses. To eliminate the noise, insert a $1.0 \mu \mathrm{~F}$ ceramic capacitor between $\mathrm{V}_{\mathrm{IN}}$ and ground as close as possible to the device.

## SWITCH VOLTAGE LIMITS

In a flyback regulator, the maximum steady-state voltage appearing at the switch, when it is off, is set by the transformer turns ratio, N , the output voltage, $\mathrm{V}_{\text {OUT }}$, and the maximum input voltage, $\mathrm{V}_{\mathrm{IN}}(\mathrm{Max})$ :

$$
V_{\text {SW }(\mathrm{OFF})}=\mathrm{V}_{\text {IN }}(\mathrm{Max})+\left(\mathrm{V}_{\text {OUT }}+\mathrm{V}_{\mathrm{F}}\right) / \mathrm{N}
$$

where $V_{F}$ is the forward biased voltage of the output diode, and is typically 0.5 V for Schottky diodes and 0.8 V for ultrafast recovery diodes. In certain circuits, there exists a voltage spike, $\mathrm{V}_{\mathrm{LL}}$, superimposed on top of the steady-state voltage (see Figure 5, waveform A). Usually, this voltage spike is caused by the transformer leakage inductance and/ or the output rectifier recovery time. To "clamp" the voltage at the switch from exceeding its maximum value, a transient suppressor in series with a diode is inserted across the transformer primary (as shown in the circuit in Figure 4 and other flyback regulator circuits throughout the datasheet). The schematic in Figure 46 shows another method of clamping the switch voltage. A single voltage transient suppressor (the SA51A) is inserted at the switch pin. This method clamps the total voltage across the switch, not just the voltage across the primary.
If poor circuit layout techniques are used (see the "Circuit Layout Guideline" section), negative voltage transients may appear on the Switch pin (pin 5). Applying a negative voltage (with respect to the IC's ground) to any monolithic IC pin causes erratic and unpredictable operation of that IC. This holds true for the LM2588 IC as well. When used in a flyback regulator, the voltage at the Switch pin (pin 5) can go negative when the switch turns on. The "ringing" voltage at the switch pin is caused by the output diode capacitance and the transformer leakage inductance forming a resonant circuit at the secondary(ies). The resonant circuit generates the "ringing" voltage, which gets reflected back through the transformer to the switch pin. There are two common methods to avoid this problem. One is to add an RC snubber around the output rectifier(s), as in Figure 46. The values of the resistor and the capacitor must be chosen so that the voltage at the Switch pin does not drop below -0.4 V . The resistor may range in value between $10 \Omega$ and $1 \mathrm{k} \Omega$, and the capacitor will vary from $0.001 \mu \mathrm{~F}$ to $0.1 \mu \mathrm{~F}$. Adding a snubber will (slightly) reduce the efficiency of the overall circuit.
The other method to reduce or eliminate the "ringing" is to insert a Schottky diode clamp between pins 5 and 4 (ground), also shown in Figure 46. This prevents the voltage at pin 5 from dropping below -0.4 V . The reverse voltage rating of the diode must be greater than the switch off voltage.


FIGURE 47. Input Line Filter

## OUTPUT VOLTAGE LIMITATIONS

The maximum output voltage of a boost regulator is the maximum switch voltage minus a diode drop. In a flyback regulator, the maximum output voltage is determined by the turns ratio, N , and the duty cycle, D , by the equation:

$$
V_{\text {OUT }} \approx N \times V_{\text {IN }} \times D /(1-D)
$$

The duty cycle of a flyback regulator is determined by the following equation:

$$
\mathrm{D}=\frac{\mathrm{V}_{\mathrm{OUT}}+\mathrm{V}_{\mathrm{F}}}{\mathrm{~N}\left(\mathrm{~V}_{\text {IN }}-\mathrm{V}_{\mathrm{SAT}}\right)+\mathrm{V}_{\mathrm{OUT}}+\mathrm{V}_{\mathrm{F}}} \approx \frac{\mathrm{~V}_{\mathrm{OUT}}}{\mathrm{~N}\left(\mathrm{~V}_{\text {IN }}\right)+\mathrm{V}_{\mathrm{OUT}}}
$$

Theoretically, the maximum output voltage can be as large as desired-just keep increasing the turns ratio of the transformer. However, there exists some physical limitations that prevent the turns ratio, and thus the output voltage, from increasing to infinity. The physical limitations are capacitances and inductances in the LM2588 switch, the output diode(s), and the transformer-such as reverse recovery time of the output diode (mentioned above).

## NOISY INPUT LINE CONDITION

A small, low-pass RC filter should be used at the input pin of the LM2588 if the input voltage has an unusually large amount of transient noise, such as with an input switch that bounces. The circuit in Figure 47 demonstrates the layout of the filter, with the capacitor placed from the input pin to ground and the resistor placed between the input supply and the input pin. Note that the values of $\mathrm{R}_{\text {IN }}$ and $\mathrm{C}_{I N}$ shown in the schematic are good enough for most applications, but some readjusting might be required for a particular application. If efficiency is a major concern, replace the resistor with a small inductor (say $10 \mu \mathrm{H}$ and rated at 200 mA ).

## STABILITY

All current-mode controlled regulators can suffer from an instability, known as subharmonic oscillation, if they operate with a duty cycle above $50 \%$. To eliminate subharmonic oscillations, a minimum value of inductance is required to ensure stability for all boost and flyback regulators. The minimum inductance is given by:

$$
\mathrm{L}(\operatorname{Min})=\frac{2.92\left[\left(\mathrm{~V}_{\mathrm{IN}}(\operatorname{Min})-\mathrm{V}_{\mathrm{SAT}}\right) \bullet(2 \mathrm{D}(\operatorname{Max})-1)\right]}{1-\mathrm{D}(\operatorname{Max})}(\mu \mathrm{H})
$$

where $\mathrm{V}_{\text {SAT }}$ is the switch saturation voltage and can be found in the Characteristic Curves.

## Application Hints (Continued)



TL/H/12420-59
FIGURE 48. Circuit Board Layout

## CIRCUIT LAYOUT GUIDELINES

As in any switching regulator, layout is very important. Rapidly switching currents associated with wiring inductance generate voltage transients which can cause problems. For minimal inductance and ground loops, keep the length of the leads and traces as short as possible. Use single point grounding or ground plane construction for best results. Separate the signal grounds from the power grounds (as indicated in Figure 48). When using the Adjustable version, physically locate the programming resistors as near the regulator IC as possible, to keep the sensitive feedback wiring short.

## HEAT SINK/THERMAL CONSIDERATIONS

In many cases, a heat sink is not required to keep the LM2588 junction temperature within the allowed operating temperature range. For each application, to determine whether or not a heat sink will be required, the following must be identified:

1) Maximum ambient temperature (in the application).
2) Maximum regulator power dissipation (in the application).
3) Maximum allowed junction temperature $\left(125^{\circ} \mathrm{C}\right.$ for the LM2588). For a safe, conservative design, a temperature approximately $15^{\circ} \mathrm{C}$ cooler than the maximum junction temperature should be selected $\left(110^{\circ} \mathrm{C}\right)$.
4) LM2588 package thermal resistances $\theta_{\mathrm{JA}}$ and $\theta_{\mathrm{JC}}$ (given in the Electrical Characteristics).
Total power dissipated ( $\mathrm{P}_{\mathrm{D}}$ ) by the LM2588 can be estimated as follows:
Boost:

$$
P_{D}=0.15 \Omega \cdot\left(\frac{I_{L O A D}}{1-D}\right)^{2} \bullet D+\frac{I_{L O A D}}{50 \bullet(1-D)} \bullet D \bullet V_{I N}
$$

Flyback:

$$
\begin{aligned}
\mathrm{P}_{\mathrm{D}}= & 0.15 \Omega \cdot\left(\frac{\mathrm{~N} \cdot \Sigma \mathrm{I}_{\mathrm{LOAD}}}{1-\mathrm{D}}\right)^{2} \bullet \mathrm{D} \\
& +\frac{\mathrm{N} \cdot \Sigma I_{\mathrm{LOAD}}}{50 \cdot(1-\mathrm{D})} \bullet \mathrm{D} \bullet \mathrm{~V}_{I N}
\end{aligned}
$$

$\mathrm{V}_{\mathrm{IN}}$ is the minimum input voltage, $\mathrm{V}_{\mathrm{OUT}}$ is the output voltage, N is the transformer turns ratio, D is the duty cycle, and $l_{\text {LOAD }}$ is the maximum load current (and $\Sigma$ lomad $_{\text {LOA }}$ is the sum of the maximum load currents for multiple-output flyback regulators). The duty cycle is given by:
Boost:

$$
\mathrm{D}=\frac{\mathrm{V}_{\text {OUT }}+\mathrm{V}_{\mathrm{F}}-\mathrm{V}_{\text {IN }}}{\mathrm{V}_{\text {OUT }}+\mathrm{V}_{\mathrm{F}}-\mathrm{V}_{\text {SAT }}} \approx \frac{\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }}}{\mathrm{V}_{\text {OUT }}}
$$

Flyback:

$$
\mathrm{D}=\frac{\mathrm{V}_{\mathrm{OUT}}+\mathrm{V}_{\mathrm{F}}}{\mathrm{~N}\left(\mathrm{~V}_{\text {IN }}-\mathrm{V}_{\mathrm{SAT}}\right)+\mathrm{V}_{\mathrm{OUT}}+\mathrm{V}_{\mathrm{F}}} \approx \frac{\mathrm{~V}_{\mathrm{OUT}}}{\mathrm{~N}\left(\mathrm{~V}_{\text {IN }}\right)+\mathrm{V}_{\mathrm{OUT}}}
$$

where $\mathrm{V}_{\mathrm{F}}$ is the forward biased voltage of the diode and is typically 0.5 V for Schottky diodes and 0.8 V for fast recovery diodes. $\mathrm{V}_{\text {SAT }}$ is the switch saturation voltage and can be found in the Characteristic Curves.
When no heat sink is used, the junction temperature rise is:

$$
\Delta T_{J}=P_{D} \bullet \theta_{J A} .
$$

Adding the junction temperature rise to the maximum ambient temperature gives the actual operating junction temperature:

$$
\mathrm{T}_{\mathrm{J}}=\Delta \mathrm{T}_{\mathrm{J}}+\mathrm{T}_{\mathrm{A}} .
$$

If the operating junction temperature exceeds the maximum junction temperatue in item 3 above, then a heat sink is required. When using a heat sink, the junction temperature rise can be determined by the following:

$$
\Delta \mathrm{T}_{\mathrm{J}}=\mathrm{P}_{\mathrm{D}} \bullet\left(\theta_{\mathrm{JC}}+\theta_{\text {Interface }}+\theta_{\text {Heat Sink }}\right)
$$

Again, the operating junction temperature will be:

$$
T_{J}=\Delta T_{J}+T_{A}
$$

## Application Hints (Continued)

As before, if the maximum junction temperature is exceeded, a larger heat sink is required (one that has a lower thermal resistance).
Included in the Switchers Made Simple ${ }^{\circledR}$ design software is a more precise (non-linear) thermal model that can be used to determine junction temperature with different inputoutput parameters or different component values. It can also calculate the heat sink thermal resistance required to maintain the regulator junction temperature below the maximum operating temperature.

To further simplify the flyback regulator design procedure, National Semiconductor is making available computer design software Switchers Made Simple ${ }^{\circledR}$ software is available on a ( $31 / 2^{\prime \prime}$ ) diskette for IBM compatible computers from a National Semiconductor sales office in your area or the National Semiconductor Customer Response Center (1-800-272-9959).

## Physical Dimensions inches (millimeters)


LM2588 SIMPLE SWITCHER 5A Flyback Regulator

Physical Dimensions inches (millimeters) (Continued)


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