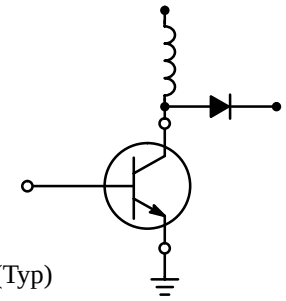
BUV48
BUV48A

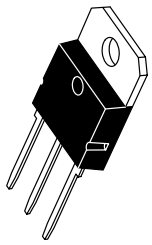
SWITCHMODE™ II Series NPN Silicon Power Transistors

The BUV48/BUV48A transistors are designed for high–voltage, high–speed, power switching in inductive circuits where fall time is critical. They are particularly suited for line–operated SWITCHMODE applications such as:

- Switching Regulators
- Inverters
- Solenoid and Relay Drivers
- Motor Controls
- Deflection Circuits
- Fast Turn–Off Times
  - 60 ns Inductive Fall Time — 25°C (Typ)
  - 120 ns Inductive Crossover Time — 25°C (Typ)
- Operating Temperature Range –65 to +175°C
- 100°C Performance Specified for:
  - Reverse–Biased SOA with Inductive Loads
  - Switching Times with Inductive Loads
  - Saturation Voltage
  - Leakage Currents (125°C)



15 AMPERES
NPN SILICON
POWER TRANSISTORS
400 AND 450 VOLTS
$V_{(BR)CEO}$
850–1000 VOLTS
$V_{(BR)CEX}$
150 WATTS



CASE 340D–02
TO–218 TYPE

MAXIMUM RATINGS

Rating	Symbol	BUV48	BUV48A	Unit
Collector–Emitter Voltage	$V_{CEO(sus)}$	400	450	Vdc
Collector–Emitter Voltage (V_{BE} = –1.5 V)	V_{CEX}	850	1000	Vdc
Emitter Base Voltage	V_{EB}	7		Vdc
Collector Current — Continuous — Peak (1) — Overload	I_C I_{CM} I_{OI}	15 30 60		Adc
Base Current — Continuous — Peak (1)	I_B I_{BM}	5 20		Adc
Total Power Dissipation — T_C = 25°C — T_C = 100°C Derate above 25°C	P_D	150 75 1		Watts W/°C
Operating and Storage Junction Temperature Range	T_J, T_{stg}	–65 to +175		°C

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1	°C/W
Maximum Lead Temperature for Soldering Purposes: 1/8″ from Case for 5 Seconds	T_L	275	°C

(1) Pulse Test: Pulse Width = 5 ms, Duty Cycle ≤ 10%.

March, 2001 – Rev. 10
Publication Order Number:
BUV48/D

ELECTRICAL CHARACTERISTICS (T_C = 25°C unless otherwise noted)

Characteristic		Symbol	Min	Typ	Max	Unit
OFF CHARACTERISTICS (1)						
Collector–Emitter Sustaining Voltage (Table 1)		$V_{CEO(sus)}$				Vdc
(I_C = 200 mA, I_B = 0) L = 25 mH	BUV48		400	—	—	
	BUV48A		450	—	—	
Collector Cutoff Current		I_{CEX}				mAdc
(V_{CEX} = Rated Value, $V_{BE(off)}$ = 1.5 Vdc)			—	—	0.2	
(V_{CEX} = Rated Value, $V_{BE(off)}$ = 1.5 Vdc, T_C = 125°C)			—	—	2	
Collector Cutoff Current		I_{CER}				mAdc
(V_{CE} = Rated V_{CEX}, R_{BE} = 10 Ω)	T_C = 25°C		—	—	0.5	
	T_C = 125°C		—	—	3	
Emitter Cutoff Current		I_{EBO}	—	—	0.1	mAdc
(V_{EB} = 5 Vdc, I_C = 0)						
Emitter–Base Breakdown Voltage		$V_{(BR)EBO}$	7	—	—	Vdc
(I_E = 50 mA – I_C = 0)						
SECOND BREAKDOWN						
Second Breakdown Collector Current with Base Forward Biased		$I_{S/b}$	See Figure 12			
Clamped Inductive SOA with Base Reverse Biased		RBSOA	See Figure 13			
ON CHARACTERISTICS (1)						
DC Current Gain		h_{FE}				
(I_C = 10 Adc, V_{CE} = 5 Vdc)	BUV48		8	—	—	
(I_C = 8 Adc, V_{CE} = 5 Vdc)	BUV48A		8	—	—	
Collector–Emitter Saturation Voltage		$V_{CE(sat)}$				Vdc
(I_C = 10 Adc, I_B = 2 Adc)			—	—	1.5	
(I_C = 15 Adc, I_B = 3 Adc)	BUV48		—	—	5	
(I_C = 10 Adc, I_B = 2 Adc, T_C = 100°C)			—	—	2	
(I_C = 8 Adc, I_B = 1.6 Adc)			—	—	1.5	
(I_C = 12 Adc, I_B = 2.4 Adc)	BUV48A		—	—	5	
(I_C = 8 Adc, I_B = 1.6 Adc, T_C = 100°C)			—	—	2	
Base–Emitter Saturation Voltage		$V_{BE(sat)}$				Vdc
(I_C = 10 Adc, I_B = 2 Adc)	BUV48		—	—	1.6	
(I_C = 10 Adc, I_B = 2 Adc, T_C = 100°C)			—	—	1.6	
(I_C = 8 Adc, I_B = 1.6 Adc)	BUV48A		—	—	1.6	
(I_C = 8 Adc, I_B = 1.6 Adc, T_C = 100°C)			—	—	1.6	
DYNAMIC CHARACTERISTICS						
Output Capacitance		C_{ob}	—	—	350	pF
(V_{CB} = 10 Vdc, I_E = 0, f_{test} = 1 MHz)						

SWITCHING CHARACTERISTICS

Resistive Load (Table 1)

Delay Time	I_C = 10 A, I_B, = 2 A I_C = 8 A, I_B, = 1.6 A Duty Cycle ≤ 2%, $V_{BE(off)}$ = 5 V T_p = 30 µs, V_{CC} = 300 V	BUV48 BUV48A	t_d	—	0.1	0.2	µs
Rise Time			t_r	—	0.4	0.7	
Storage Time			t_s	—	1.3	2	
Fall Time			t_f	—	0.2	0.4	

Inductive Load, Clamped (Table 1)

Storage Time	I_C = 10 A I_{B1} = 2 A	BUV48	(T_C = 25°C)	t_{sv}	—	1.3	—	µs
Fall Time				t_{fi}	—	0.06	—	
Storage Time	I_C = 8 A I_{B1} = 1.6 A	BUV48A	(T_C = 100°C)	t_{sv}	—	1.5	2.5	
Crossover Time				t_c	—	0.3	0.6	
Fall Time				t_{fi}	—	0.17	0.35	

(1) Pulse Test: Pulse Width = 300 µs, Duty Cycle ≤ 2%.

Vcl = 300 V, $V_{BE(off)}$ = 5 V, Lc = 180 µH

DC CHARACTERISTICS

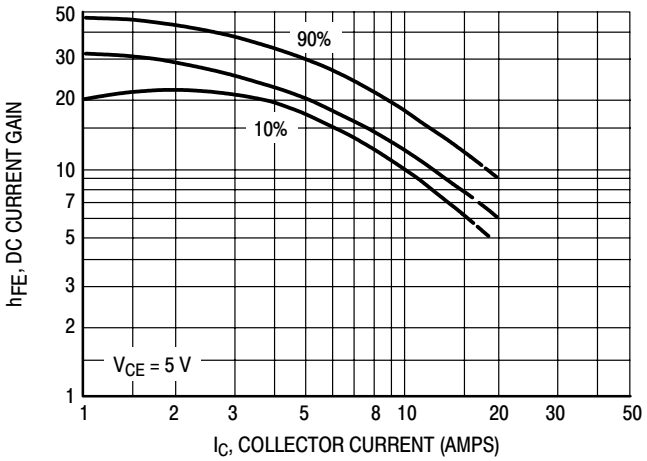


Figure 1. DC Current Gain

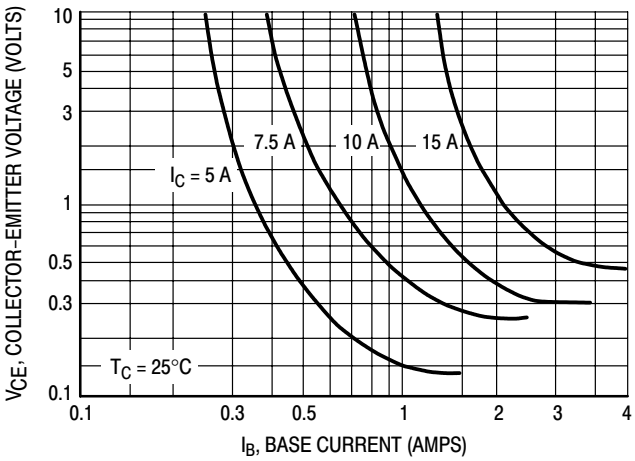


Figure 2. Collector Saturation Region

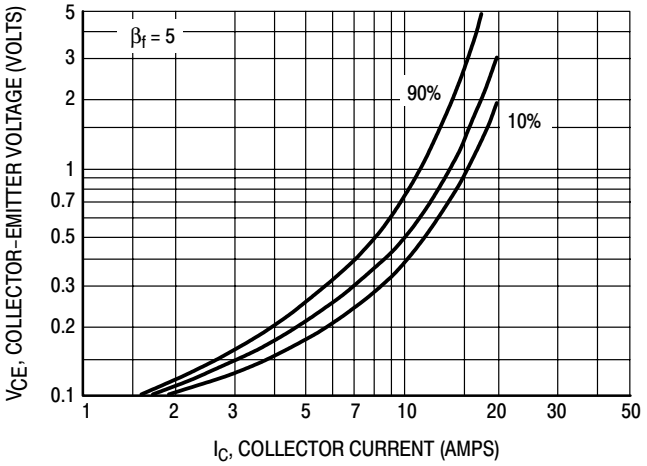


Figure 3. Collector–Emitter Saturation Voltage

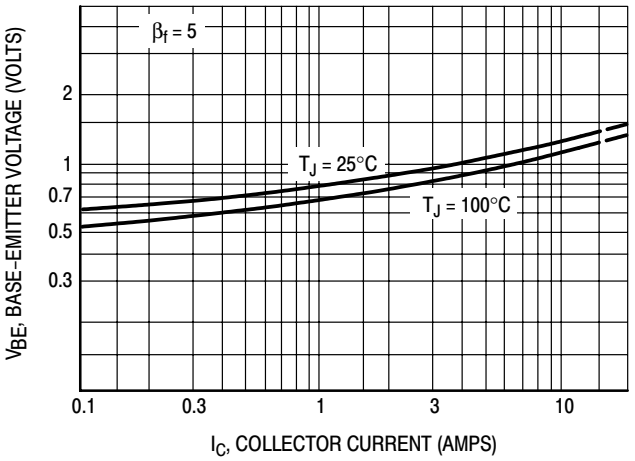


Figure 4. Base–Emitter Voltage

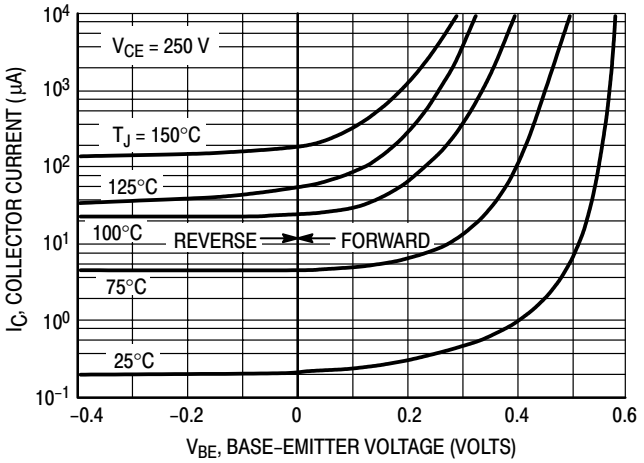


Figure 5. Collector Cutoff Region

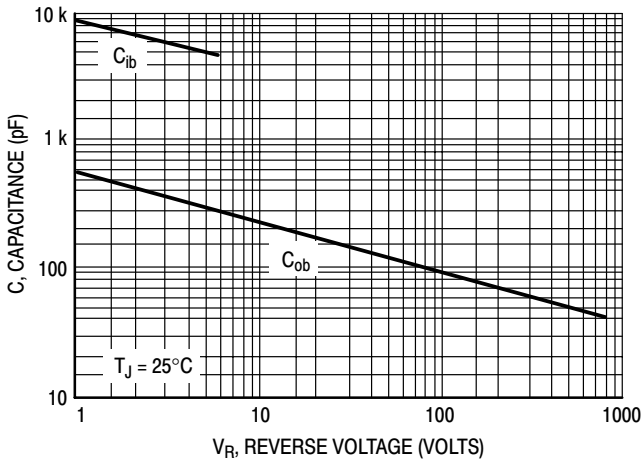
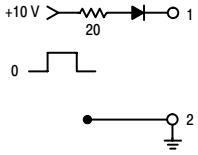
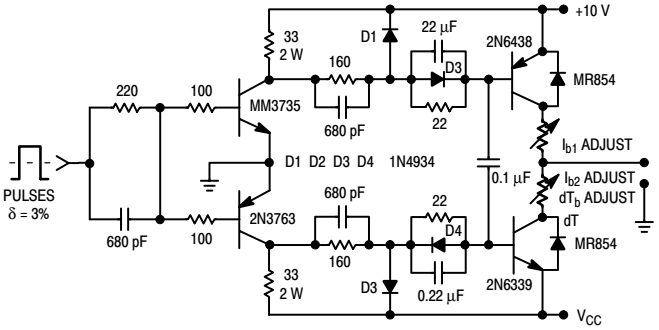
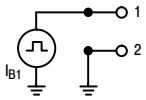
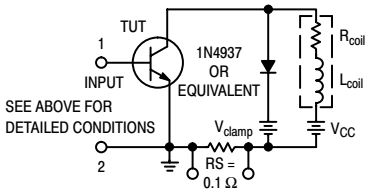
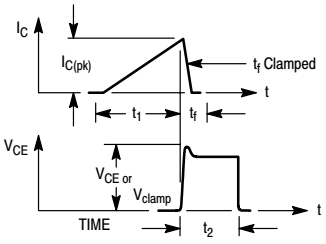
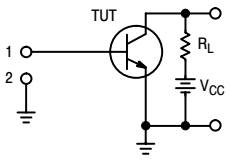


Figure 6. Capacitance

Table 1. Test Conditions for Dynamic Performance

	$V_{CEO(sus)}$	RBSOA AND INDUCTIVE SWITCHING	RESISTIVE SWITCHING
INPUT CONDITIONS	 PW Varied to Attain I_C = 200 mA		TURN–ON TIME  I_{B1} adjusted to obtain the forced h_{FE} desired TURN–OFF TIME Use inductive switching driver as the input to the resistive test circuit.
CIRCUIT VALUES	L_{coil} = 25 mH, V_{CC} = 10 V R_{coil} = 0.7 Ω	L_{coil} = 180 μH R_{coil} = 0.05 Ω V_{CC} = 20 V V_{clamp} = 300 V R_B ADJUSTED TO ATTAIN DESIRED I_{B1}	V_{CC} = 300 V R_L = 83 Ω Pulse Width = 10 μs
TEST CIRCUITS	INDUCTIVE TEST CIRCUIT 	OUTPUT WAVEFORMS  t_1 Adjusted to Obtain I_C $t_1 \approx \frac{L_{coil}(I_{C_{pk}})}{V_{CC}}$ $t_2 \approx \frac{L_{coil}(I_{C_{pk}})}{V_{Clamp}}$ Test Equipment Scope — Tektronix 475 or Equivalent	RESISTIVE TEST CIRCUIT 

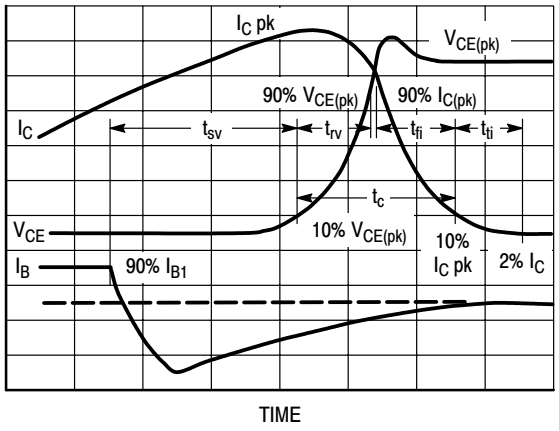


Figure 7. Inductive Switching Measurements

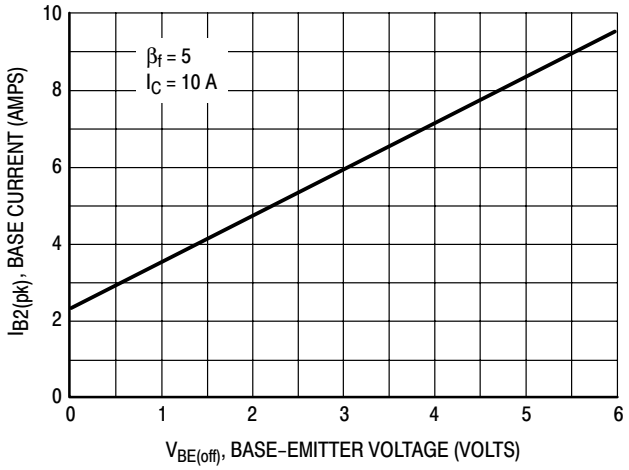


Figure 8. Peak–Reverse Current

SWITCHING TIMES NOTE

In resistive switching circuits, rise, fall, and storage times have been defined and apply to both current and voltage waveforms since they are in phase. However, for inductive loads which are common to SWITCHMODE power supplies and hammer drivers, current and voltage waveforms are not in phase. Therefore, separate measurements must be made on each waveform to determine the total switching time. For this reason, the following new terms have been defined.

t_{sv} = Voltage Storage Time, 90% I_{B1} to 10% V_{clamp}
t_{rv} = Voltage Rise Time, 10–90% V_{clamp}
t_{fi} = Current Fall Time, 90–10% I_C
t_{ti} = Current Tail, 10–2% I_C
t_c = Crossover Time, 10% V_{clamp} to 10% I_C

An enlarged portion of the inductive switching waveforms is shown in Figure 7 to aid in the visual identity of these terms.

For the designer, there is minimal switching loss during storage time and the predominant switching power losses occur during the crossover interval and can be obtained using the standard equation from AN–222:

$$P_{SWT} = 1/2\ V_{CC} I_C (t_c)\ f$$

In general, $t_{rv} + t_{fi} \simeq t_c$. However, at lower test currents this relationship may not be valid.

As is common with most switching transistors, resistive switching is specified at 25°C and has become a benchmark for designers. However, for designers of high frequency converter circuits, the user oriented specifications which make this a “SWITCHMODE” transistor are the inductive switching speeds (t_c and t_{sv}) which are guaranteed at 100°C.

INDUCTIVE SWITCHING

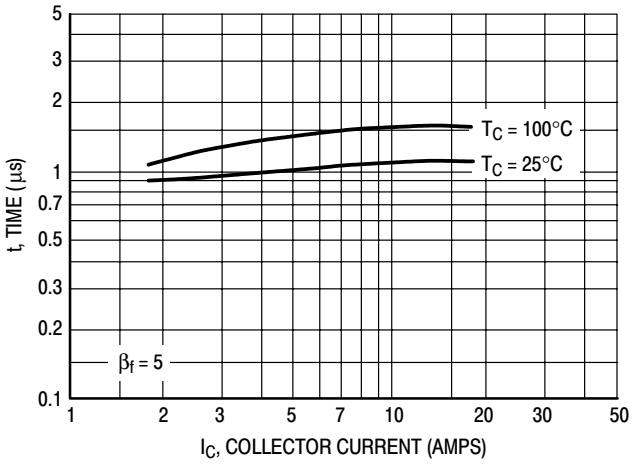


Figure 9. Storage Time, t_{sv}

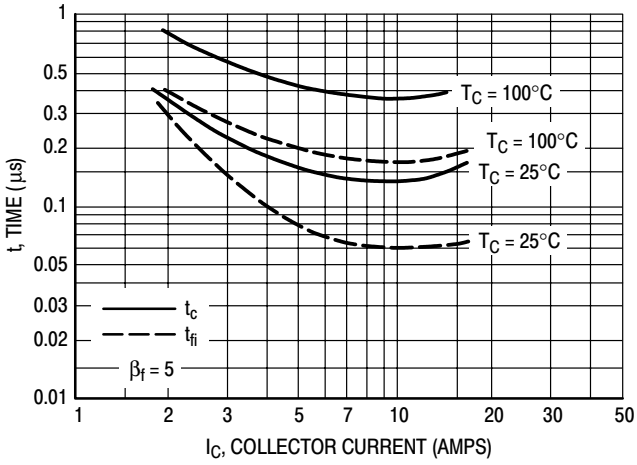


Figure 10. Crossover and Fall Times

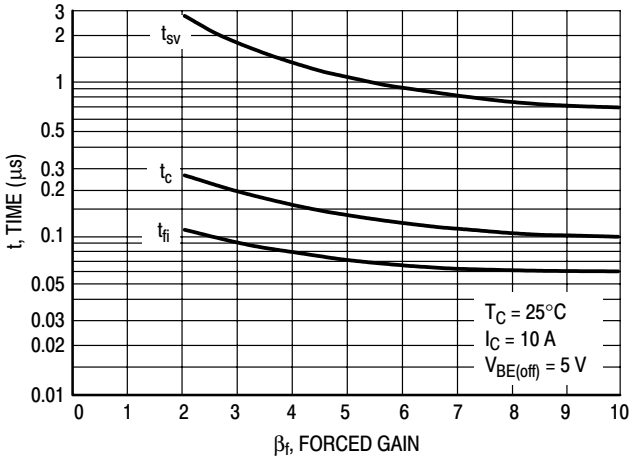


Figure 11. Turn–Off Times versus Forced Gain

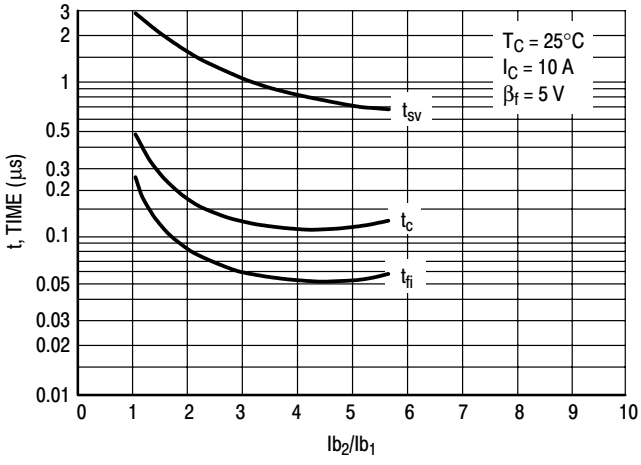


Figure 12. Turn–Off Times versus Ib_2/Ib_1

The Safe Operating Area figures shown in Figures 12 and 13 are specified for these devices under the test conditions shown.

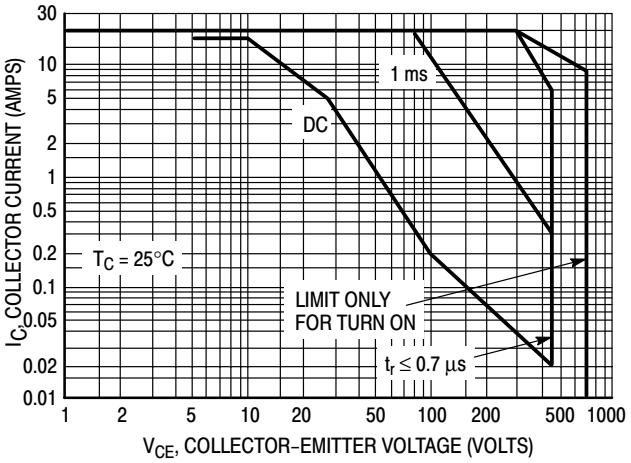


Figure 13. Forward Bias Safe Operating Area

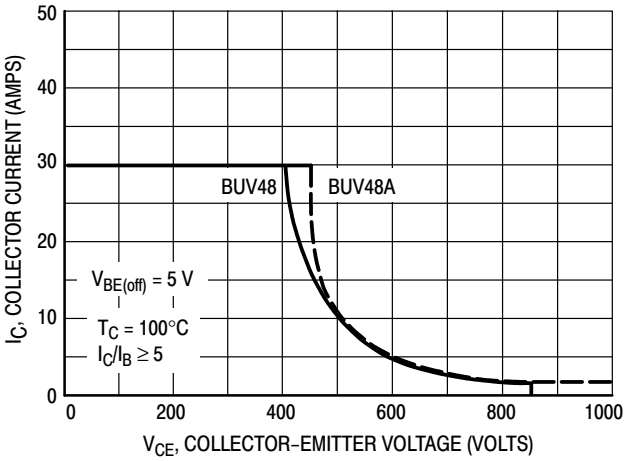


Figure 14. Reverse Bias Safe Operating Area

SAFE OPERATING AREA INFORMATION

FORWARD BIAS

There are two limitations on the power handling ability of a transistor: average junction temperature and second breakdown. Safe operating area curves indicate $I_C - V_{CE}$ limits of the transistor that must be observed for reliable operation; i.e., the transistor must not be subjected to greater dissipation than the curves indicate.

The data of Figure 13 is based on T_C = 25°C; $T_{J(pk)}$ is variable depending on power level. Second breakdown pulse limits are valid for duty cycles to 10% but must be derated when $T_C \leq$ 25°C. Second breakdown limitations do not derate the same as thermal limitations. Allowable current at the voltages shown on Figure 13 may be found at any case temperature by using the appropriate curve on Figure 15.

$T_{J(pk)}$ may be calculated from the data in Figure 11. At high case temperatures, thermal limitations will reduce the power that can be handled to values less than the limitations imposed by second breakdown.

REVERSE BIAS

For inductive loads, high voltage and high current must be sustained simultaneously during turn−off, in most cases, with the base to emitter junction reverse biased. Under these conditions the collector voltage must be held to a safe level at or below a specific value of collector current. This can be accomplished by several means such as active clamping, RC snubbing, load line shaping, etc. The safe level for these devices is specified as Reverse Bias Safe Operating Area and represents the voltage current conditions during reverse biased turn−off. This rating is verified under clamped conditions so that the device is never subjected to an avalanche mode. Figure 14 gives RBSOA characteristics.

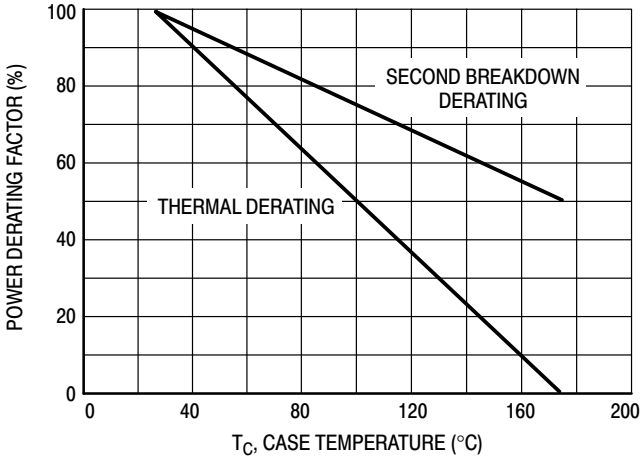


Figure 15. Power Derating

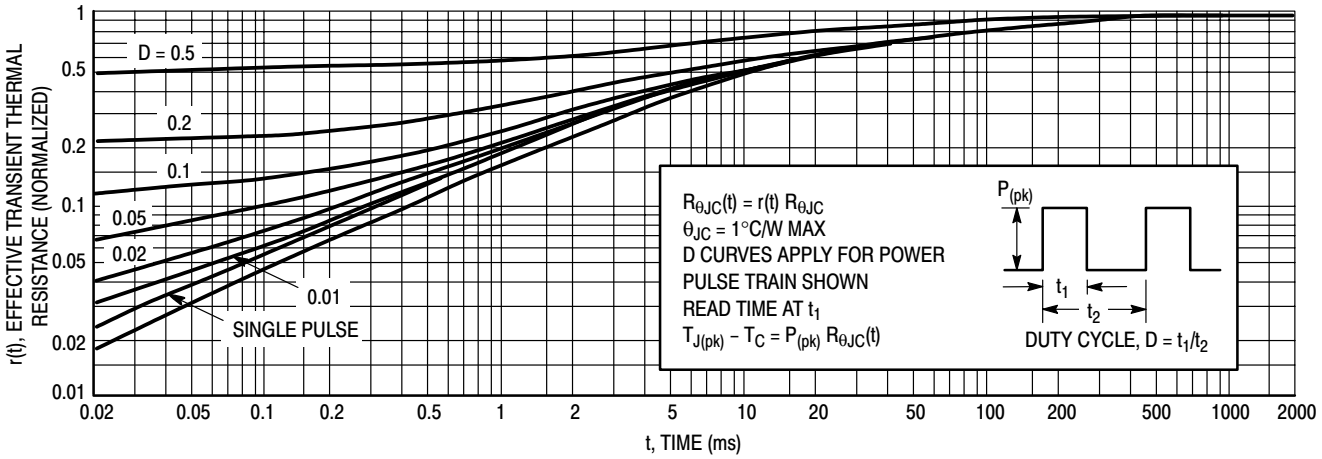


Figure 16. Thermal Response

OVERLOAD CHARACTERISTICS

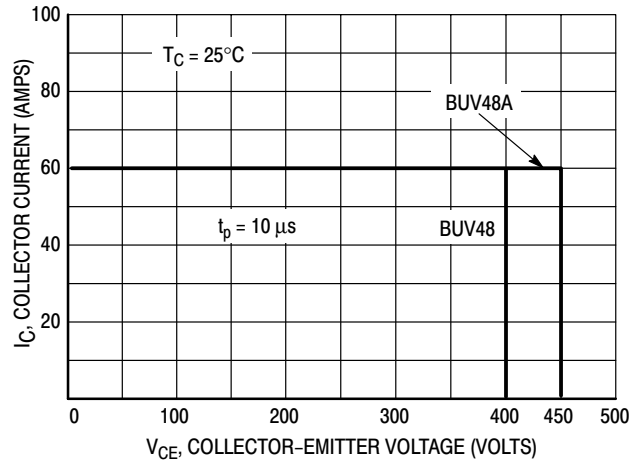


Figure 17. Rated Overload Safe Operating Area (OLSOA)

OLSOA

OLSOA applies when maximum collector current is limited and known. A good example is a circuit where an inductor is inserted between the transistor and the bus, which limits the rate of rise of collector current to a known value. If the transistor is then turned off within a specified amount of time, the magnitude of collector current is also known.

Maximum allowable collector–emitter voltage versus collector current is plotted for several pulse widths. (Pulse width is defined as the time lag between the fault condition and the removal of base drive.) Storage time of the transistor has been factored into the curve. Therefore, with bus voltage and maximum collector current known, Figure 17 defines the maximum time which can be allowed for fault detection and shutdown of base drive.

OLSOA is measured in a common–base circuit (Figure 19) which allows precise definition of collector–emitter voltage and collector current. This is the same circuit that is used to measure forward–bias safe operating area.

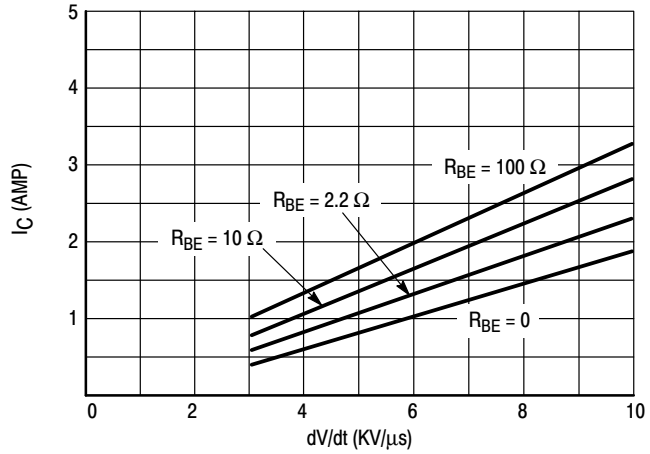


Figure 18. $I_C = f(dV/dt)$

Notes:
- $V_{CE} = V_{CC} + V_{BE}$
- Adjust pulsed current source for desired I_C, t_p

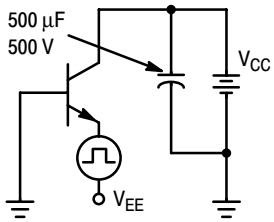
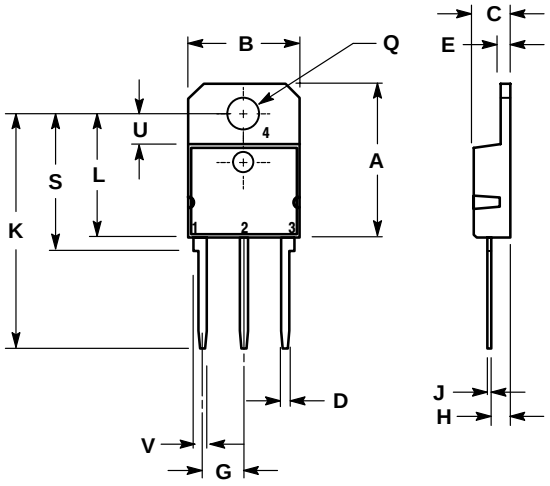


Figure 19. Overload SOA Test Circuit

PACKAGE DIMENSIONS

SOT−93 (TO−218)
CASE 340D−02
ISSUE B



NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
2. CONTROLLING DIMENSION: MILLIMETER.

	MILLIMETERS		INCHES	
DIM	MIN	MAX	MIN	MAX
A	−−−	20.35	−−−	0.801
B	14.70	15.20	0.579	0.598
C	4.70	4.90	0.185	0.193
D	1.10	1.30	0.043	0.051
E	1.17	1.37	0.046	0.054
G	5.40	5.55	0.213	0.219
H	2.00	3.00	0.079	0.118
J	0.50	0.78	0.020	0.031
K	31.00 REF		1.220 REF	
L	−−−	16.20	−−−	0.638
Q	4.00	4.10	0.158	0.161
S	17.80	18.20	0.701	0.717
U	4.00 REF		0.157 REF	
V	1.75 REF		0.069	

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Email: ONlit–asia@hibbertco.com

JAPAN: ON Semiconductor, Japan Customer Focus Center
4–32–1 Nishi–Gotanda, Shinagawa–ku, Tokyo, Japan 141–0031
Phone: 81–3–5740–2700
Email: r14525@onsemi.com

ON Semiconductor Website: http://onsemi.com

For additional information, please contact your local Sales Representative.